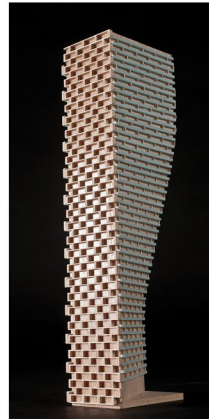


**ROADWAY TRAFFIC NOISE
ASSESSMENT**

1240 Carling Avenue
Ottawa, Ontario

GRADIENT WIND REPORT: 23-113 – Traffic Noise



May 15, 2023

PREPARED FOR

S.J. Lawrence Architect Incorporated

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PREPARED BY

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EXECUTIVE SUMMARY

This report describes a roadway traffic noise assessment undertaken in support of a Site Plan Control (SPA) application for a proposed development located at 1240 Carling Avenue in Ottawa, Ontario. The development comprises a 3-storey residential building with 18 units. The primary sources of roadway traffic noise impacting the site include Merivale Road, Carling Avenue, and Highway 417. Figure 1 illustrates a complete site plan with surrounding context.

The assessment is based on (i) theoretical noise prediction methods that conform to the Ministry of the Environment, Conservation and Parks (MECP) and City of Ottawa requirements; (ii) noise level criteria as specified by the City of Ottawa's Environmental Noise Control Guidelines (ENCG); (iii) future vehicular traffic volumes based on the City of Ottawa's Official Plan roadway classifications; and (iv) architectural drawings provided by S.J. Lawrence Architect Incorporated in April 2023.

The results of the current analysis indicate that noise levels will range between 47 and 74 dBA during the daytime period (07:00-23:00) and between 39 and 67 dBA during the nighttime period (23:00-07:00). The highest noise level (74 dBA) occurs at the northwest façade, which is nearest and most exposed to Carling Avenue. Building components with a higher Sound Transmission Class (STC) rating will be required where exterior noise levels exceed 65 dBA, as indicated in Figure 3 and Table 4. Results of the calculations also indicate that the development will require central air conditioning, which will allow occupants to keep windows closed and maintain a comfortable living environment. A Type D Warning Clause will also be required in all Lease, Purchase and Sale Agreements, as summarized in Section 6.

Noise levels at the at-grade amenity are expected to not exceed 55 dBA during the daytime period. Therefore, no acoustic mitigation is required for this space.

Stationary noise sources associated with the development are expected to comprise of direct expansion (DX) Split Air Conditioning units and internal forced air heating systems. These sources are not expected to be a concern at noise sensitive spaces and surrounding properties, provided the following are considered in the design: judicious selection of the equipment, and locating the equipment on a high roof away from nearby residential receptors. Installation of the equipment should be done in accordance with NPC-216 Residential Air Conditioning Devices.



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1. INTRODUCTION

Gradient Wind Engineering Inc. (Gradient Wind) was retained by S.J. Lawrence Architect Incorporated to undertake a roadway traffic noise assessment in support of a Site Plan Control (SPA) application for a proposed development located at 1240 Carling Avenue in Ottawa, Ontario. This report summarizes the methodology, results, and recommendations related to the assessment of exterior and interior noise levels generated by local roadway traffic.

Our work is based on theoretical noise calculation methods conforming to the City of Ottawa¹ and Ministry of the Environment, Conservation and Parks (MECP)² guidelines. Noise calculations were based on architectural drawings provided by S.J. Lawrence Architect Incorporated in April 2023, with future traffic volumes corresponding to the City of Ottawa's Official Plan (OP) roadway classifications.

2. TERMS OF REFERENCE

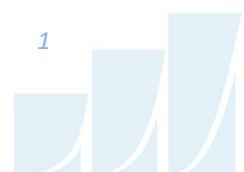
The focus of this roadway traffic noise assessment is a proposed development located at 1240 Carling Avenue in Ottawa, Ontario. The development comprises a 3-storey residential building with 18 units. The building is situated on an irregular parcel of land bound by Carling Avenue to the northwest, and low-rise residential buildings in the remaining compass directions. The building has a triangular planform with a proposed amenity area at the rear of the building to the south. The basement comprises several residential units, a storage area to the north, and a mechanical room at the center. The ground floor comprises a garbage and bicycle storage room to the northwest corner, a lobby area at the north corner, and residential units throughout. The remaining floors above are primarily designated for residential use.

The at-grade amenity space associated with the development was included in the assessment as an Outdoor Living Area (OLA). The primary sources of roadway traffic noise impacting the site include Merivale Road, Carling Avenue, and Highway 417. Figure 1 illustrates a complete site plan with surrounding context.

Stationary noise sources associated with the development are expected to comprise of direct expansion (DX) Split Air Conditioning units and internal forced air heating systems. These sources are not expected

¹ City of Ottawa Environmental Noise Control Guidelines, January 2016

² Ontario Ministry of the Environment and Climate Change – Environmental Noise Guidelines, Publication NPC-300, Queens Printer for Ontario, Toronto, 2013



to be a concern at noise sensitive spaces and surrounding properties, provided the following are considered in the design: judicious selection of the equipment, and locating the equipment on a high roof away from nearby residential receptors. Installation of the equipment should be done in accordance with NPC-216 Residential Air Conditioning Devices.

3. OBJECTIVES

The principal objectives of this study are to (i) calculate the future noise levels on the study building produced by local roadway traffic, and (ii) ensure that interior and exterior noise levels do not exceed the allowable limits specified by the City of Ottawa's Environmental Noise Control Guidelines as outlined in Section 4.2 of this report.

4. METHODOLOGY

4.1 Background

Noise can be defined as any obtrusive sound. It is created at a source, transmitted through a medium, such as air, and intercepted by a receiver. Noise may be characterized in terms of the power of the source or the sound pressure at a specific distance. While the power of a source is characteristic of that particular source, the sound pressure depends on the location of the receiver and the path that the noise takes to reach the receiver. Measurement of noise is based on the decibel unit, dBA, which is a logarithmic ratio referenced to a standard noise level (2×10^{-5} Pascals). The 'A' suffix refers to a weighting scale, which better represents how the noise is perceived by the human ear. With this scale, a doubling of power results in a 3 dBA increase in measured noise levels and is just perceptible to most people. An increase of 10 dBA is often perceived to be twice as loud.

4.2 Roadway Traffic Noise

4.2.1 Criteria for Roadway Traffic Noise

For surface roadway traffic noise, the equivalent sound energy level, L_{eq} , provides a measure of the time varying noise levels, which is well correlated with the annoyance of sound. It is defined as the continuous sound level, which has the same energy as a time varying noise level over a period of time. For roadways, the L_{eq} is commonly calculated on the basis of a 16-hour (L_{eq16}) daytime (07:00-23:00) / 8-hour (L_{eq8}) nighttime (23:00-07:00) split to assess its impact on residential buildings. The City of Ottawa's



Environmental Noise Control Guidelines (ENCG) specifies that the recommended indoor noise limit range (that is relevant to this study) is 45 and 40 dBA for living rooms and sleeping quarters respectively, as listed in Table 1. Based on Gradient Wind’s experience, more comfortable indoor noise levels should be targeted, towards 42 and 37 dBA, respectively, to control peak noise and deficiencies in building envelope construction.

TABLE 1: INDOOR SOUND LEVEL CRITERIA (ROAD) ³

Type of Space	Time Period	L _{eq} (dBA)
General offices, reception areas, retail stores, etc.	07:00 – 23:00	50
Living/dining/den areas of residences , hospitals, schools, nursing/retirement homes, day-care centres, theatres, places of worship, libraries, individual or semi-private offices, conference rooms, etc.	07:00 – 23:00	45
Sleeping quarters of hotels/motels	23:00 – 07:00	45
Sleeping quarters of residences , hospitals, nursing/retirement homes, etc.	23:00 – 07:00	40

Predicted noise levels at the plane of window (POW) dictate the action required to achieve the recommended sound levels. An open window is considered to provide a 10 dBA reduction in noise, while a standard closed window is capable of providing a minimum 20 dBA noise reduction⁴. A closed window due to a ventilation requirement will bring noise levels down to achieve an acceptable indoor environment⁵. Therefore, where noise levels exceed 55 dBA daytime and 50 dBA nighttime, the ventilation for the building should consider the need for having windows and doors closed, which triggers the need for forced air heating with provision for central air conditioning. Where noise levels exceed 65 dBA daytime and 60 dBA nighttime, air conditioning will be required and building components will require higher levels of sound attenuation⁶.

³ Adapted from ENCG 2016 – Tables 2.2b and 2.2c

⁴ Burberry, P.B. (2014). Mitchell’s Environment and Services. Routledge, Page 125

⁵ MOECP, Environmental Noise Guidelines, NPC 300 – Part C, Section 7.8

⁶ MOECP, Environmental Noise Guidelines, NPC 300 – Part C, Section 7.1.3

The sound level criterion for outdoor living areas is 55 dBA, which applies during the daytime (07:00 to 23:00). When noise levels exceed 55 dBA, mitigation must be provided to reduce noise levels where technically and administratively feasible to acceptable levels at or below the criterion.

4.2.2 Theoretical Roadway Noise Predictions

Noise predictions were performed with the aid of the MECP computerized noise assessment program, STAMSON 5.04, for road analysis. Appendix A includes the STAMSON 5.04 input and output data.

Roadway traffic noise calculations were performed by treating each roadway segment as separate line sources of noise. In addition to the traffic volumes summarized in Table 2, theoretical noise predictions were based on the following parameters:

- Truck traffic on all roadways was taken to comprise 5% heavy trucks and 7% medium trucks, as per ENCG requirements for noise level predictions.
- The day/night split for all streets was taken to be 92%/8%, respectively.
- Ground surfaces were taken to be reflective due to the presence of hard (paved) ground, or absorptive due to the presence of soft (lawn) ground.
- Topography was assumed to be a flat/gentle slope surrounding the study building. Highway 417 was modelled with an elevation of 2 m above local grade.
- For select sources where appropriate, the receptor considered the surrounding existing and proposed buildings as a barrier partially or fully obstructing exposure to the source.
- Noise receptors were strategically placed at 5 locations around the study area (see Figure 2).
- Receptor distances and exposure angles are illustrated in Figures 4 and 5.

4.2.3 Roadway Traffic Volumes

The ENCG dictates that noise calculations should consider future sound levels based on a roadway’s classification at the mature state of development. Therefore, traffic volumes are based on the roadway classifications outlined in the City of Ottawa’s Official Plan (OP) and Transportation Master Plan⁷ which provide additional details on future roadway expansions. Average Annual Daily Traffic (AADT) volumes are then based on data in Table B1 of the ENCG for each roadway classification. Table 2 (below) summarizes the AADT values used for each roadway included in this assessment.

TABLE 2: ROADWAY TRAFFIC DATA

Segment	Roadway Traffic Data	Speed Limit (km/h)	Traffic Volumes
Merivale Road	4-Lane Arterial (Undivided)	50	30,000
Carling Avenue	6-Lane Arterial (Divided)	60	50,000
Highway 417 Eastbound/Westbound	8-Lane Freeway	100	73,333

⁷ City of Ottawa Transportation Master Plan, November 2013

5. ROADWAY TRAFFIC NOISE RESULTS

5.1 Roadway Traffic Noise Levels

The results of the roadway traffic noise calculations are summarized in Table 3 below. A complete set of input and output data from all STAMSON 5.04 calculations are available in Appendix A.

TABLE 3: EXTERIOR NOISE LEVELS DUE TO ROAD TRAFFIC

Receptor Number	Receptor Height Above Grade (m)	Receptor Location	STAMSON 5.04 Noise Level (dBA)	
			Day	Night
1	7.7	POW – 3 rd Floor – Southwest Façade	70	62
2	7.7	POW – 3 rd Floor – Northwest Façade	74	67
3	7.7	POW – 3 rd Floor – Northeast Façade	70	63
4	7.7	POW – 3 rd Floor – Southeast Façade	47	39
5	1.5	OLA – At-grade amenity	53	N/a*

*Nighttime noise levels for the OLA are not considered as per ENCG

The results of the current analysis indicate that noise levels will range between 47 and 74 dBA during the daytime period (07:00-23:00) and between 39 and 67 dBA during the nighttime period (23:00-07:00). The highest noise level (74 dBA) occurs at the northwest façade, which is nearest and most exposed to Carling Avenue.

5.2 Noise Control Measures

The noise levels predicted due to roadway traffic exceed the criteria listed in Section 4.2 for building components. As discussed in Section 4.2, the anticipated STC requirements for windows have been estimated based on the overall noise reduction required for each intended use of space (STC = outdoor noise level – targeted indoor noise levels). As per ENCG requirements, detailed STC calculations will be required to be completed prior to building permit application. The STC requirements for the windows are summarized below in Table 4 and outlined in Figure 3. Where specific updated building components are not identified, bedroom/living room are to satisfy Ontario Building Code (OBC 2020) requirements.



TABLE 4: NOISE CONTROL REQUIREMENTS

Façade	Floor Number	Min. Window STC (Bedroom/Living Room)	Exterior Wall STC	Warning Clauses	A/C or FAH
Southwest, Northwest, Northeast	1-3	37/32	45	Type D	A/C

The STC requirements apply to windows, doors, spandrel panels and curtainwall elements. Exterior wall components on these façades are recommended to have a minimum STC of 45, where a window/wall system is used. A review of window supplier literature indicates that the specified STC ratings can be achieved by a variety of window systems having a combination of glass thickness and inter-pane spacing. We have specified an example window configuration, however several manufacturers and various combinations of window components, such as those proposed, will offer the necessary sound attenuation rating. The specified STC requirements also apply to swinging and/or sliding doors.

Results of the calculations also indicate that the development will require central air conditioning, which will allow occupants to keep windows closed and maintain a comfortable living environment. In addition to ventilation requirements, Warning Clauses will also be required in all Agreements of Purchase and Sale and Lease Agreements, as summarized in Section 6.

Noise levels at the at-grade amenity are expected to not exceed 55 dBA during the daytime period. Therefore, no acoustic mitigation is required for this space.

6. DISCUSSION, CONCLUSIONS AND RECOMMENDATIONS

The results of the current analysis indicate that noise levels will range between 47 and 74 dBA during the daytime period (07:00-23:00) and between 39 and 67 dBA during the nighttime period (23:00-07:00). The highest noise level (74 dBA) occurs at the northwest façade, which is nearest and most exposed to Carling Avenue. Building components with a higher Sound Transmission Class (STC) rating will be required where exterior noise levels exceed 65 dBA, as indicated in Figure 3 and Table 4.

Results of the calculations also indicate that the development will require central air conditioning, which will allow occupants to keep windows closed and maintain a comfortable living environment. A Type D Warning Clause will also be required in all Lease, Purchase and Sale Agreements, as summarized below.

Type D:

"This dwelling unit has been supplied with a central air conditioning system which will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the Municipality and the Ministry of the Environment."

Noise levels at the at-grade amenity are expected to not exceed 55 dBA during the daytime period. Therefore, no acoustic mitigation is required for this space.

Stationary noise sources associated with the development are expected to comprise of direct expansion (DX) Split Air Conditioning units and internal forced air heating systems. These sources are not expected to be a concern at noise sensitive spaces and surrounding properties, provided the following are considered in the design: judicious selection of the equipment, and locating the equipment on a high roof away from nearby residential receptors. Installation of the equipment should be done in accordance with NPC-216 Residential Air Conditioning Devices.

This concludes our roadway traffic noise assessment and report. If you have any questions or wish to discuss our findings, please advise us. In the interim, we thank you for the opportunity to be of service.

Sincerely,

Gradient Wind Engineering Inc.

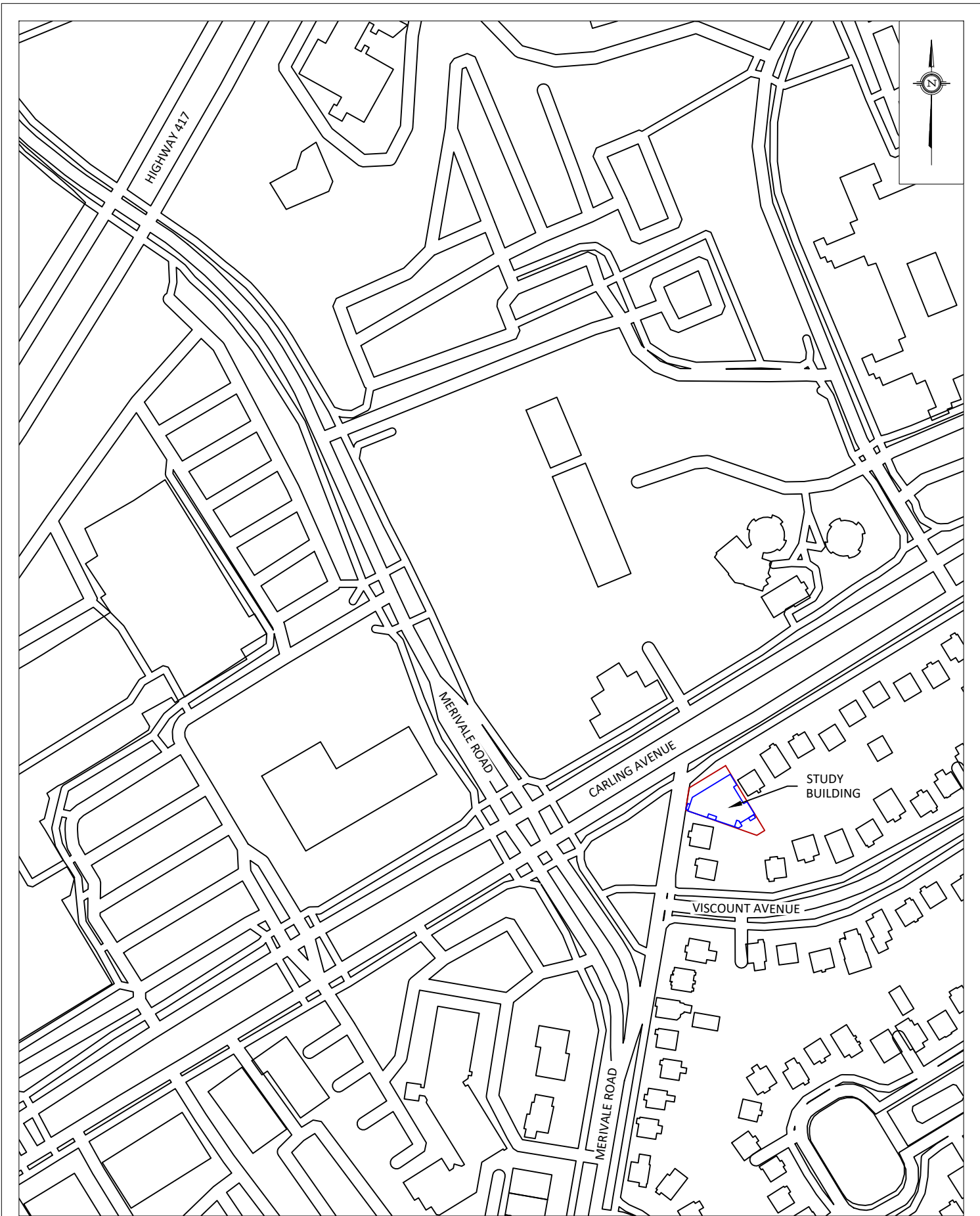


Giuseppe Garro, M.A.Sc.
Environmental Scientist

Gradient Wind Report #23-113

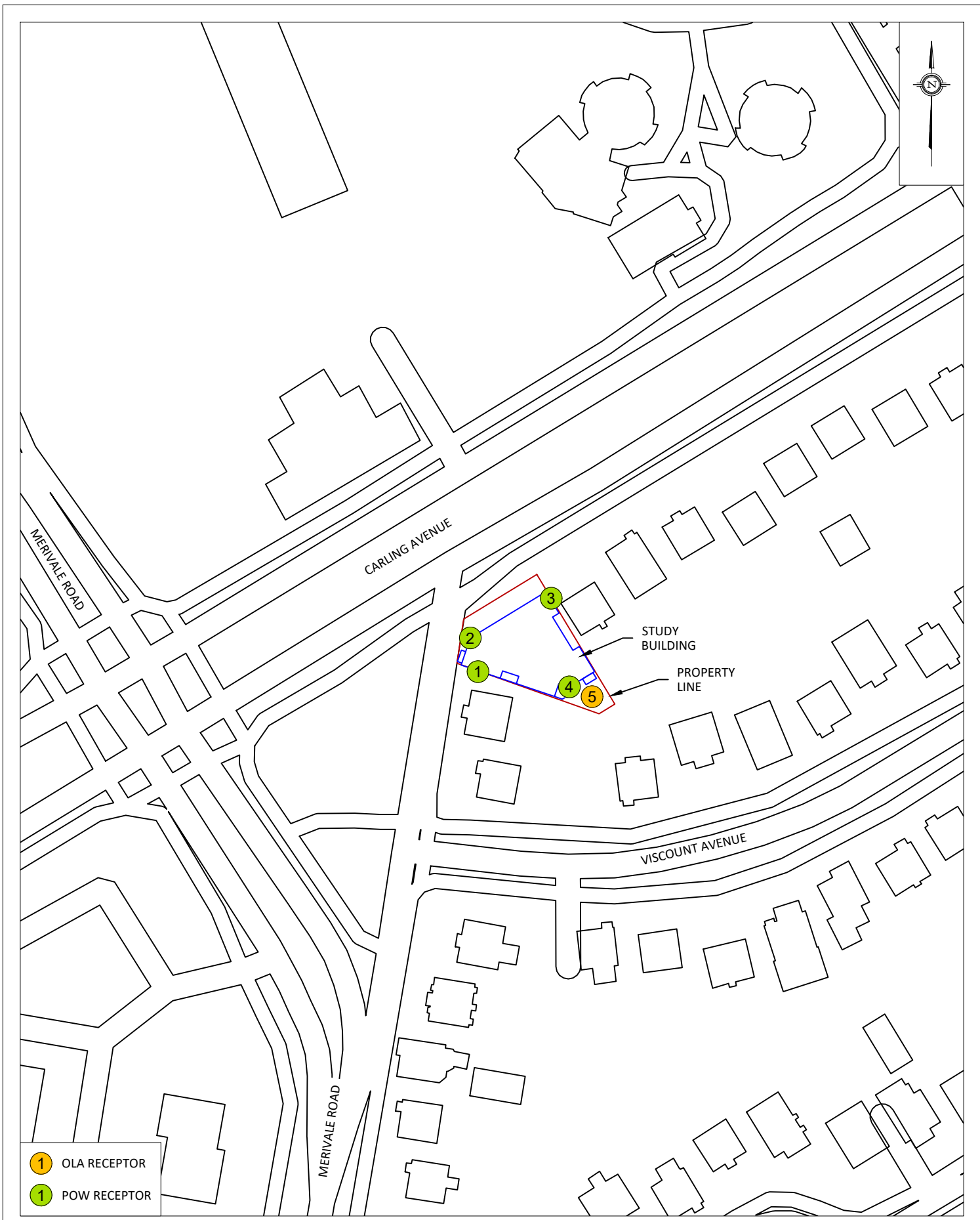


Joshua Foster, P.Eng.
Lead Engineer



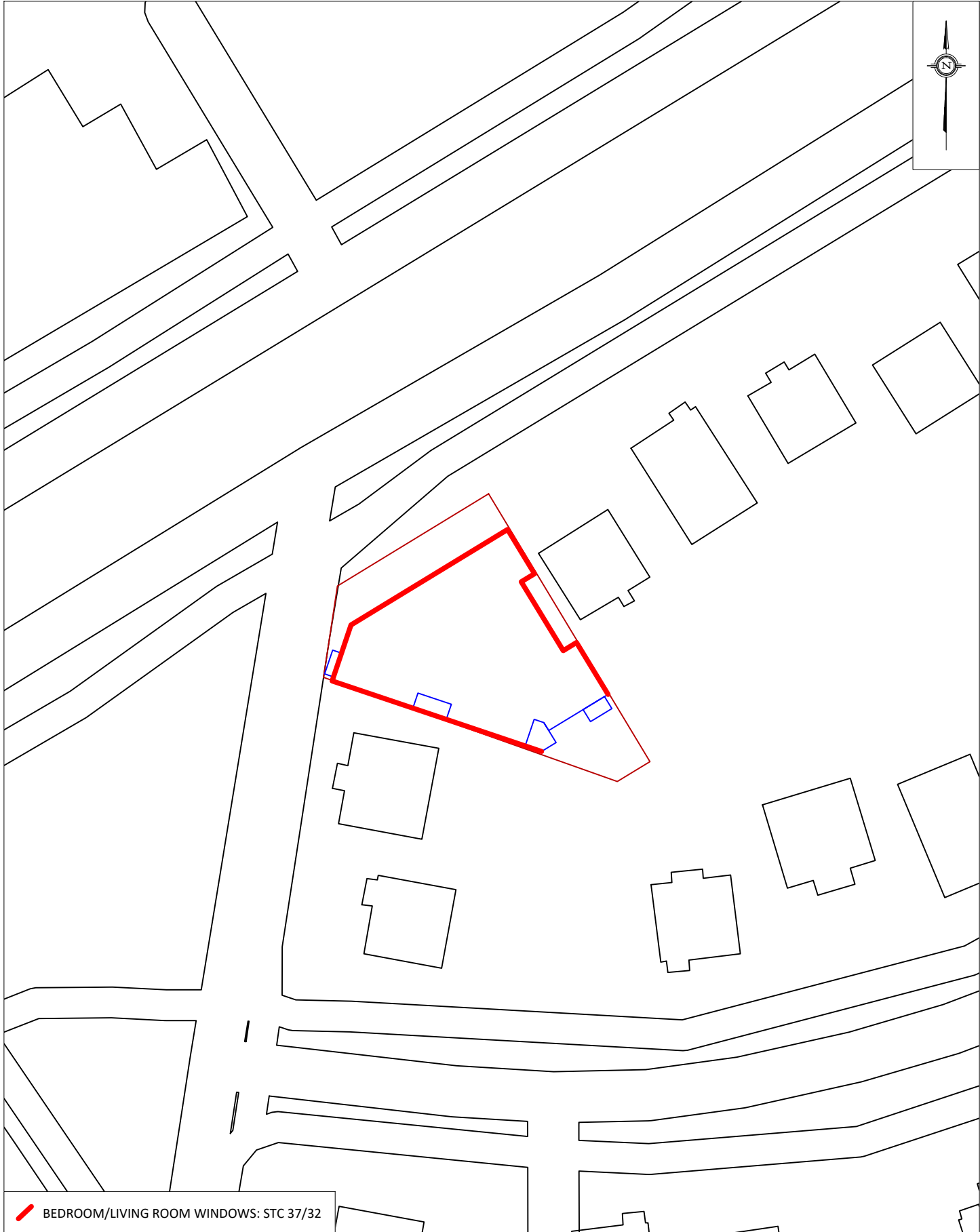
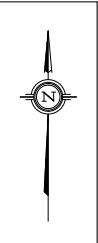
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SCALE	1:2000 (APPROX.)	DRAWING NO. GW23-113-1
DATE	MAY 4, 2023	DRAWN BY G.G.


DESCRIPTION	FIGURE 1: SITE PLAN AND SURROUNDING CONTEXT
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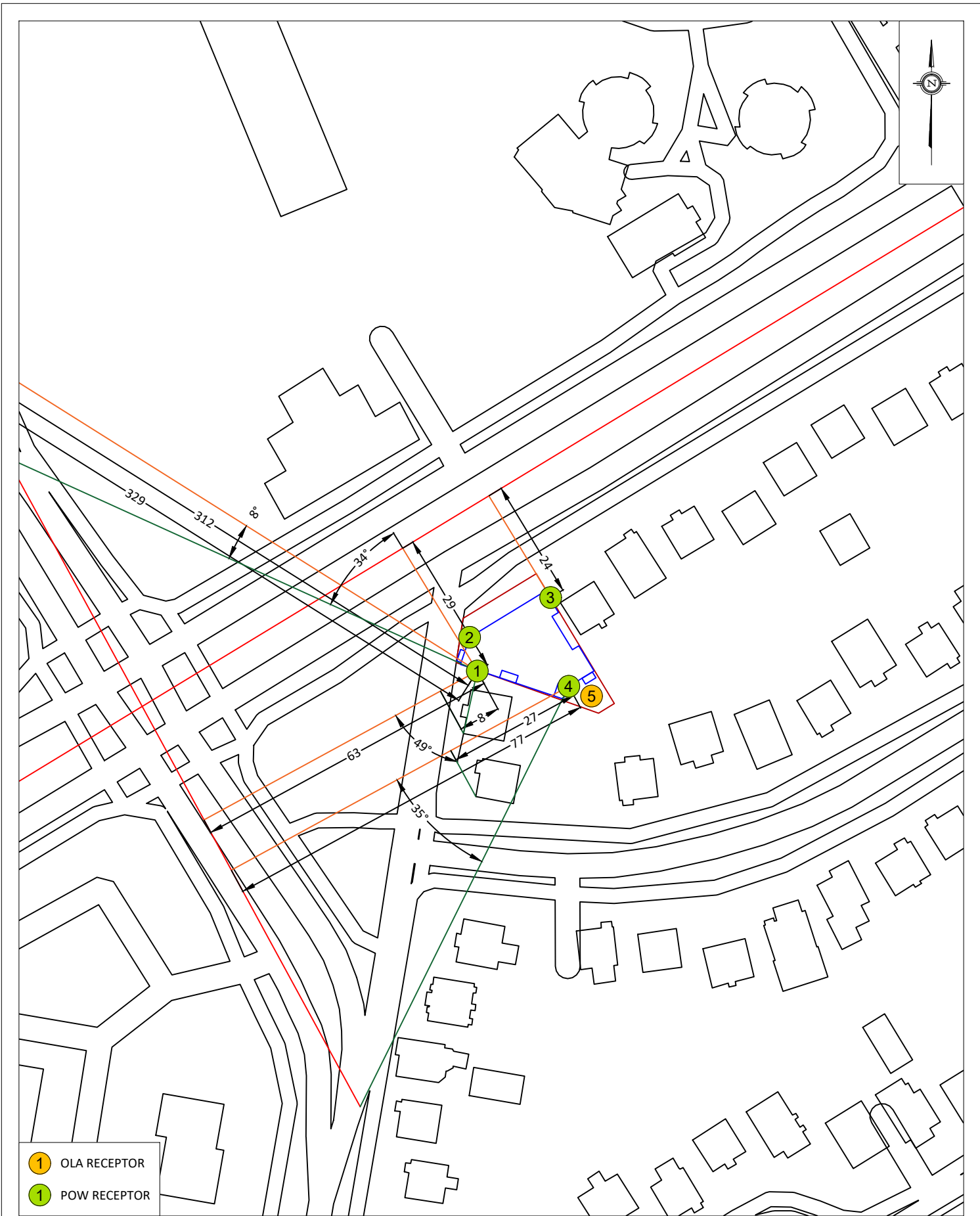
- 1 OLA RECEPTOR
- 1 POW RECEPTOR

GRADIENTWIND ENGINEERS & SCIENTISTS 127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM	PROJECT 1240 CARLING AVENUE, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT		DESCRIPTION FIGURE 2: RECEPTOR LOCATIONS
	SCALE 1:1000 (APPROX.)	DRAWING NO. GW23-113-2	
	DATE MAY 4, 2023	DRAWN BY G.G.	



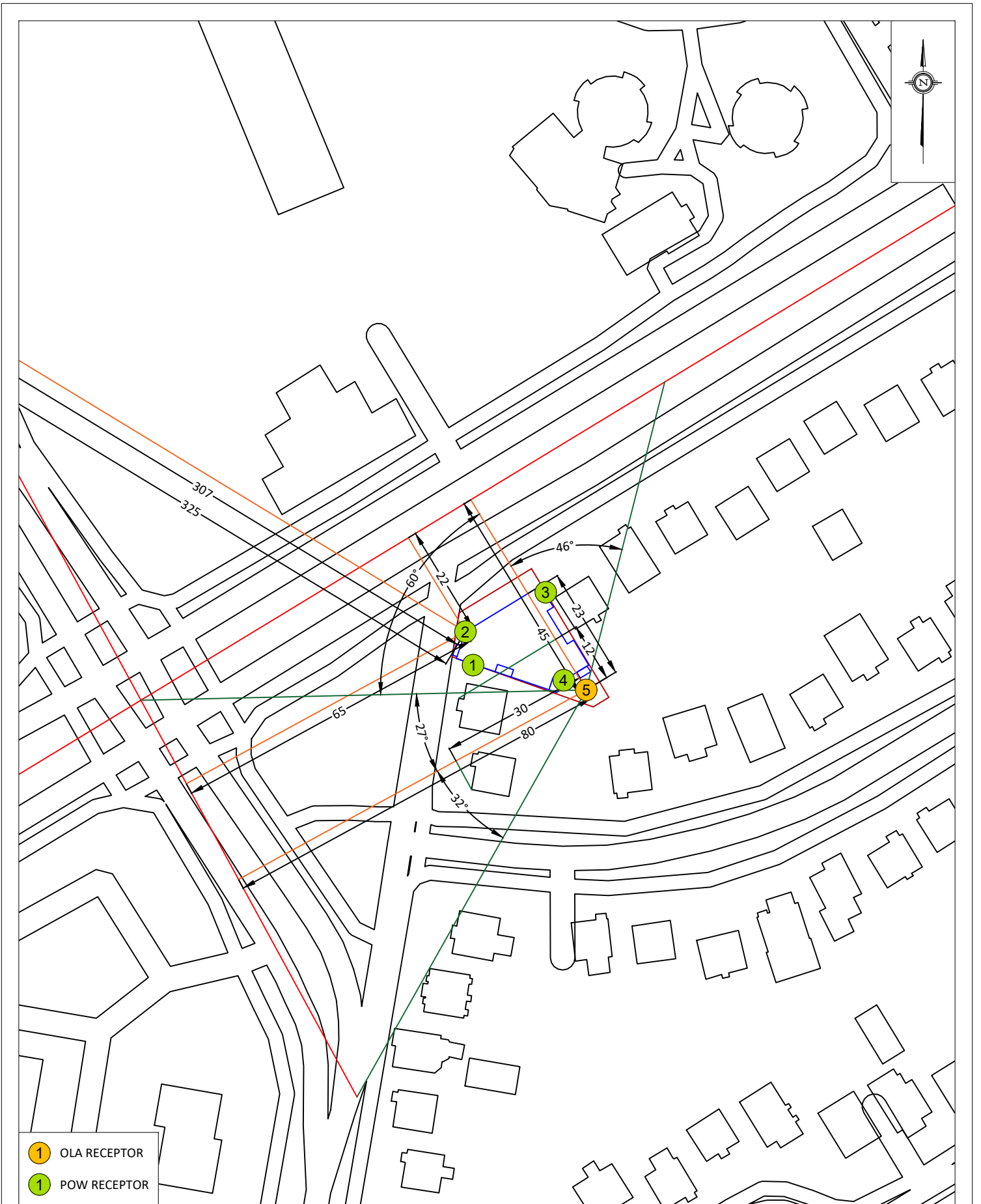
 BEDROOM/LIVING ROOM WINDOWS: STC 37/32

PROJECT	1240 CARLING AVENUE, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT	
SCALE	1:500 (APPROX.)	DRAWING NO. GW23-113-3
DATE	MAY 4, 2023	DRAWN BY G.G.



- 1 OLA RECEPTOR
- 1 POW RECEPTOR

<p>GRADIENTWIND ENGINEERS & SCIENTISTS</p> <p>127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM</p>	<p>PROJECT: 1240 CARLING AVENUE, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT</p>	<p>DESCRIPTION:</p>	
	<p>SCALE: 1:1000 (APPROX.)</p>	<p>DRAWING NO.: GW23-113-4</p>	<p>FIGURE 4: STAMSON INPUT PARAMETERS</p>
	<p>DATE: MAY 4, 2023</p>	<p>DRAWN BY: G.G.</p>	

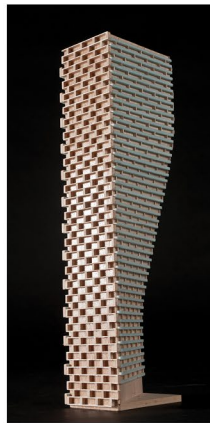


- 1 OLA RECEPTOR
- 1 POW RECEPTOR

<p>GRADIENTWIND ENGINEERS & SCIENTISTS</p> <p>127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM</p>	PROJECT	1240 CARLING AVENUE, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT	DESCRIPTION
	SCALE	1:1000 (APPROX.)	DRAWING NO.
	DATE	MAY 4, 2023	DRAWN BY
			<p>FIGURE 5: STAMSON INPUT PARAMETERS</p>
		DRAWING NO.	GW23-113-5
		DRAWN BY	G.G.

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APPENDIX A

STAMSON 5.04 – INPUT AND OUTPUT DATA

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STAMSON 5.0 NORMAL REPORT Date: 05-05-2023 11:33:27
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r1.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: MR (day/night)

Car traffic volume : 24288/2112 veh/TimePeriod *
Medium truck volume : 1932/168 veh/TimePeriod *
Heavy truck volume : 1380/120 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 30000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: MR (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 63.00 / 63.00 m
Receiver height : 7.70 / 7.70 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -90.00 deg Angle2 : -49.00 deg
Barrier height : 8.00 m
Barrier receiver distance : 8.00 / 8.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 2: CA (day/night)

Car traffic volume : 40480/3520 veh/TimePeriod *
Medium truck volume : 3220/280 veh/TimePeriod *
Heavy truck volume : 2300/200 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)



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* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 50000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: CA (day/night)

Angle1 Angle2 : -90.00 deg -34.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 29.00 / 29.00 m
Receiver height : 7.70 / 7.70 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

Road data, segment # 3: HWY 417 EB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: HWY 417 EB (day/night)

Angle1 Angle2 : -90.00 deg -8.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 312.00 / 312.00 m
Receiver height : 7.70 / 7.70 m
Topography : 3 (Elevated; no barrier)
Elevation : 2.00 m
Reference angle : 0.00



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Road data, segment # 4: HWY 417 WB (day/night)

```
-----
Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)
```

* Refers to calculated road volumes based on the following input:

```
24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00
```

Data for Segment # 4: HWY 417 WB (day/night)

```
-----
Angle1 Angle2 : -90.00 deg -8.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 329.00 / 329.00 m
Receiver height : 7.70 / 7.70 m
Topography : 3 (Elevated; no barrier)
Elevation : 2.00 m
Reference angle : 0.00
```

Results segment # 1: MR (day)

Source height = 1.50 m

Barrier height for grazing incidence

```
-----
Source ! Receiver ! Barrier ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
1.50 ! 7.70 ! 6.91 ! 6.91
```

ROAD (0.00 + 52.56 + 64.14) = 64.43 dBA

```
Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj
SubLeq
```

```
-----
--
-90 -49 0.00 71.49 0.00 -6.23 -6.42 0.00 0.00 -6.27
52.56
```



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```

-----
--
-49      90      0.00  71.49   0.00  -6.23  -1.12   0.00   0.00   0.00
64.14
-----

```

Segment Leq : 64.43 dBA

Results segment # 2: CA (day)

Source height = 1.50 m

ROAD (0.00 + 67.29 + 0.00) = 67.29 dBA

```

Angle1 Angle2  Alpha RefLeq  P.Adj  D.Adj  F.Adj  W.Adj  H.Adj  B.Adj
SubLeq
-----

```

```

--
-90     -34     0.00  75.22   0.00  -2.86  -5.07   0.00   0.00   0.00
67.29
-----

```

Segment Leq : 67.29 dBA

Results segment # 3: HWY 417 EB (day)

Source height = 1.50 m

ROAD (0.00 + 58.22 + 0.00) = 58.22 dBA

```

Angle1 Angle2  Alpha RefLeq  P.Adj  D.Adj  F.Adj  W.Adj  H.Adj  B.Adj
SubLeq
-----

```

```

--
-90     -8      0.41  81.40   0.00 -18.64  -4.54   0.00   0.00   0.00
58.22
-----

```

Segment Leq : 58.22 dBA



Results segment # 4: HWY 417 WB (day)

Source height = 1.50 m

ROAD (0.00 + 57.90 + 0.00) = 57.90 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--									
-90	-8	0.41	81.40	0.00	-18.97	-4.54	0.00	0.00	0.00
57.90									

Segment Leq : 57.90 dBA

Total Leq All Segments: 69.74 dBA

Results segment # 1: MR (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	7.70	6.91	6.91

ROAD (0.00 + 44.97 + 56.54) = 56.83 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--									
-90	-49	0.00	63.89	0.00	-6.23	-6.42	0.00	0.00	-6.27
44.97									

--									
-49	90	0.00	63.89	0.00	-6.23	-1.12	0.00	0.00	0.00
56.54									

Segment Leq : 56.83 dBA



Results segment # 2: CA (night)

Source height = 1.50 m

ROAD (0.00 + 59.69 + 0.00) = 59.69 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--									
-90	-34	0.00	67.63	0.00	-2.86	-5.07	0.00	0.00	0.00
59.69									

Segment Leq : 59.69 dBA

Results segment # 3: HWY 417 EB (night)

Source height = 1.49 m

ROAD (0.00 + 50.62 + 0.00) = 50.62 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--									
-90	-8	0.41	73.80	0.00	-18.64	-4.54	0.00	0.00	0.00
50.62									

Segment Leq : 50.62 dBA

Results segment # 4: HWY 417 WB (night)

Source height = 1.49 m

ROAD (0.00 + 50.30 + 0.00) = 50.30 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--									
-90	-8	0.41	73.80	0.00	-18.97	-4.54	0.00	0.00	0.00
50.30									

Segment Leq : 50.30 dBA

Total Leq All Segments: 62.14 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 69.74
(NIGHT): 62.14



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STAMSON 5.0 NORMAL REPORT Date: 05-05-2023 11:33:35
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r2.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: MR (day/night)

Car traffic volume : 24288/2112 veh/TimePeriod *
Medium truck volume : 1932/168 veh/TimePeriod *
Heavy truck volume : 1380/120 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 30000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: MR (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 65.00 / 65.00 m
Receiver height : 7.70 / 7.70 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

Road data, segment # 2: CA (day/night)

Car traffic volume : 40480/3520 veh/TimePeriod *
Medium truck volume : 3220/280 veh/TimePeriod *
Heavy truck volume : 2300/200 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 50000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00



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Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: CA (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 22.00 / 22.00 m
Receiver height : 7.70 / 7.70 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

Road data, segment # 3: HWY 417 EB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: HWY 417 EB (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 307.00 / 307.00 m
Receiver height : 7.70 / 7.70 m
Topography : 3 (Elevated; no barrier)
Elevation : 2.00 m
Reference angle : 0.00

Road data, segment # 4: HWY 417 WB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *



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Heavy truck volume : 3373/293 veh/TimePeriod *
 Posted speed limit : 100 km/h
 Road gradient : 0 %
 Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
 Percentage of Annual Growth : 0.00
 Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 4: HWY 417 WB (day/night)

 Angle1 Angle2 : -90.00 deg 90.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 325.00 / 325.00 m
 Receiver height : 7.70 / 7.70 m
 Topography : 3 (Elevated; no barrier)
 Elevation : 2.00 m
 Reference angle : 0.00

Results segment # 1: MR (day)

 Source height = 1.50 m

ROAD (0.00 + 62.11 + 0.00) = 62.11 dBA

SubLeq	Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

62.11	0	90	0.00	71.49	0.00	-6.37	-3.01	0.00	0.00	0.00
-------	---	----	------	-------	------	-------	-------	------	------	------

 Segment Leq : 62.11 dBA

Results segment # 2: CA (day)

 Source height = 1.50 m

ROAD (0.00 + 73.56 + 0.00) = 73.56 dBA



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Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	90	0.00	75.22	0.00	-1.66	0.00	0.00	0.00	0.00

SubLeq
73.56

Segment Leq : 73.56 dBA

Results segment # 3: HWY 417 EB (day)

Source height = 1.50 m

ROAD (0.00 + 61.85 + 0.00) = 61.85 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	90	0.41	81.40	0.00	-18.54	-1.01	0.00	0.00	0.00

SubLeq
61.85

Segment Leq : 61.85 dBA

Results segment # 4: HWY 417 WB (day)

Source height = 1.50 m

ROAD (0.00 + 61.50 + 0.00) = 61.50 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	90	0.41	81.40	0.00	-18.89	-1.01	0.00	0.00	0.00

SubLeq
61.50

Segment Leq : 61.50 dBA

Total Leq All Segments: 74.36 dBA



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Results segment # 1: MR (night)

Source height = 1.50 m

ROAD (0.00 + 54.52 + 0.00) = 54.52 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

0	90	0.00	63.89	0.00	-6.37	-3.01	0.00	0.00	0.00
54.52									

Segment Leq : 54.52 dBA

Results segment # 2: CA (night)

Source height = 1.50 m

ROAD (0.00 + 65.97 + 0.00) = 65.97 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

-90	90	0.00	67.63	0.00	-1.66	0.00	0.00	0.00	0.00
65.97									

Segment Leq : 65.97 dBA

Results segment # 3: HWY 417 EB (night)

Source height = 1.49 m

ROAD (0.00 + 54.25 + 0.00) = 54.25 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

-90	90	0.41	73.80	0.00	-18.54	-1.01	0.00	0.00	0.00
54.25									



Segment Leq : 54.25 dBA

Results segment # 4: HWY 417 WB (night)

Source height = 1.49 m

ROAD (0.00 + 53.90 + 0.00) = 53.90 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq

--
-90 90 0.41 73.80 0.00 -18.89 -1.01 0.00 0.00 0.00
53.90

--

Segment Leq : 53.90 dBA

Total Leq All Segments: 66.77 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 74.36
(NIGHT): 66.77



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STAMSON 5.0 NORMAL REPORT Date: 05-05-2023 11:33:42
 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r3.te Time Period: Day/Night 16/8 hours
 Description:

Road data, segment # 1: CA (day/night)

```
-----
Car traffic volume   : 40480/3520   veh/TimePeriod  *
Medium truck volume : 3220/280    veh/TimePeriod  *
Heavy truck volume  : 2300/200    veh/TimePeriod  *
Posted speed limit  : 60 km/h
Road gradient       : 0 %
Road pavement      : 1 (Typical asphalt or concrete)
```

* Refers to calculated road volumes based on the following input:

```
24 hr Traffic Volume (AADT or SADT): 50000
Percentage of Annual Growth         : 0.00
Number of Years of Growth           : 0.00
Medium Truck % of Total Volume      : 7.00
Heavy Truck % of Total Volume       : 5.00
Day (16 hrs) % of Total Volume      : 92.00
```

Data for Segment # 1: CA (day/night)

```
-----
Angle1  Angle2      : 0.00 deg   90.00 deg
Wood depth          : 0           (No woods.)
No of house rows   : 0 / 0
Surface            : 2           (Reflective ground surface)
Receiver source distance : 24.00 / 24.00 m
Receiver height     : 7.70 / 7.70 m
Topography          : 1           (Flat/gentle slope; no barrier)
Reference angle     : 0.00
```

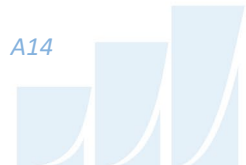
Results segment # 1: CA (day)

Source height = 1.50 m

ROAD (0.00 + 70.17 + 0.00) = 70.17 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq	-----									
70.17	0	90	0.00	75.22	0.00	-2.04	-3.01	0.00	0.00	0.00



Segment Leq : 70.17 dBA

Total Leq All Segments: 70.17 dBA

Results segment # 1: CA (night)

Source height = 1.50 m

ROAD (0.00 + 62.58 + 0.00) = 62.58 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq

--
 0 90 0.00 67.63 0.00 -2.04 -3.01 0.00 0.00 0.00
62.58

--

Segment Leq : 62.58 dBA

Total Leq All Segments: 62.58 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 70.17
 (NIGHT): 62.58



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STAMSON 5.0 NORMAL REPORT Date: 05-05-2023 11:33:47
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r4.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: MR (day/night)

Car traffic volume : 24288/2112 veh/TimePeriod *
Medium truck volume : 1932/168 veh/TimePeriod *
Heavy truck volume : 1380/120 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 30000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: MR (day/night)

Angle1 Angle2 : -35.00 deg 0.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 77.00 / 77.00 m
Receiver height : 7.70 / 7.70 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -35.00 deg Angle2 : 0.00 deg
Barrier height : 8.00 m
Barrier receiver distance : 27.00 / 27.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Results segment # 1: MR (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source ! Receiver ! Barrier ! Elevation of



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Height (m)	!	Height (m)	!	Height (m)	!	Barrier Top (m)
1.50	!	7.70	!	5.52	!	5.52

ROAD (0.00 + 46.99 + 0.00) = 46.99 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--	-35	0	0.00	71.49	0.00	-7.10	-7.11	0.00	0.00	-10.29
46.99										

Segment Leq : 46.99 dBA

Total Leq All Segments: 46.99 dBA

Results segment # 1: MR (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	!	Receiver Height (m)	!	Barrier Height (m)	!	Elevation of Barrier Top (m)
1.50	!	7.70	!	5.52	!	5.52

ROAD (0.00 + 39.39 + 0.00) = 39.39 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--	-35	0	0.00	63.89	0.00	-7.10	-7.11	0.00	0.00	-10.29
39.39										

Segment Leq : 39.39 dBA

Total Leq All Segments: 39.39 dBA

TOTAL Leq FROM ALL SOURCES (DAY) : 46.99
(NIGHT) : 39.39



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STAMSON 5.0 NORMAL REPORT Date: 05-05-2023 11:33:53
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r5.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: MR (day/night)

Car traffic volume : 24288/2112 veh/TimePeriod *
Medium truck volume : 1932/168 veh/TimePeriod *
Heavy truck volume : 1380/120 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 30000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: MR (day/night)

Angle1 Angle2 : -32.00 deg 27.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 80.00 / 80.00 m
Receiver height : 1.50 / 1.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -32.00 deg Angle2 : 27.00 deg
Barrier height : 8.00 m
Barrier receiver distance : 30.00 / 30.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 2: CA1 (day/night)

Car traffic volume : 40480/3520 veh/TimePeriod *
Medium truck volume : 3220/280 veh/TimePeriod *
Heavy truck volume : 2300/200 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)



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* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 50000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: CA1 (day/night)

Angle1 Angle2 : -90.00 deg -60.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 45.00 / 45.00 m
Receiver height : 1.50 / 1.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -90.00 deg Angle2 : -60.00 deg
Barrier height : 8.00 m
Barrier receiver distance : 12.00 / 12.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 3: CA2 (day/night)

Car traffic volume : 40480/3520 veh/TimePeriod *
Medium truck volume : 3220/280 veh/TimePeriod *
Heavy truck volume : 2300/200 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 50000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: CA2 (day/night)

Angle1 Angle2 : -60.00 deg 46.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0



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Surface : 1 (Absorptive ground surface)
Receiver source distance : 45.00 / 45.00 m
Receiver height : 1.50 / 1.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -60.00 deg Angle2 : 46.00 deg
Barrier height : 10.33 m
Barrier receiver distance : 23.00 / 23.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 4: CA3 (day/night)

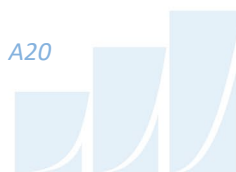
Car traffic volume : 40480/3520 veh/TimePeriod *
Medium truck volume : 3220/280 veh/TimePeriod *
Heavy truck volume : 2300/200 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 50000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 4: CA3 (day/night)

Angle1 Angle2 : 46.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 45.00 / 45.00 m
Receiver height : 1.50 / 1.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : 46.00 deg Angle2 : 90.00 deg
Barrier height : 8.00 m
Barrier receiver distance : 23.00 / 23.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00



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Results segment # 1: MR (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	1.50	1.50	1.50

ROAD (0.00 + 40.12 + 0.00) = 40.12 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

-32	27	0.18	71.49	0.00	-8.58	-4.88	0.00	0.00	-17.91
40.12									

Segment Leq : 40.12 dBA

Results segment # 2: CA1 (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	1.50	1.50	1.50

ROAD (0.00 + 47.65 + 0.00) = 47.65 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

-90	-60	0.18	75.22	0.00	-5.63	-9.02	0.00	0.00	-12.93
47.65									

Segment Leq : 47.65 dBA



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Results segment # 3: CA2 (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	1.50	1.50	1.50

ROAD (0.00 + 47.93 + 0.00) = 47.93 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

-60	46	0.04	75.22	0.00	-4.96	-2.33	0.00	0.00	-20.00
47.93									

Segment Leq : 47.93 dBA

Results segment # 4: CA3 (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	1.50	1.50	1.50

ROAD (0.00 + 49.09 + 0.00) = 49.09 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

46	90	0.18	75.22	0.00	-5.63	-7.07	0.00	0.00	-13.43
49.09									

Segment Leq : 49.09 dBA

Total Leq All Segments: 53.26 dBA



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Results segment # 1: MR (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	1.50	1.50	1.50

ROAD (0.00 + 32.53 + 0.00) = 32.53 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

-32	27	0.18	63.89	0.00	-8.58	-4.88	0.00	0.00	-17.91
32.53									

Segment Leq : 32.53 dBA

Results segment # 2: CA1 (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	1.50	1.50	1.50

ROAD (0.00 + 40.05 + 0.00) = 40.05 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

-90	-60	0.18	67.63	0.00	-5.63	-9.02	0.00	0.00	-12.93
40.05									

Segment Leq : 40.05 dBA

GRADIENTWIND

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Results segment # 3: CA2 (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	1.50	1.50	1.50

ROAD (0.00 + 40.34 + 0.00) = 40.34 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-60	46	0.04	67.63	0.00	-4.96	-2.33	0.00	0.00	-20.00

SubLeq
40.34

Segment Leq : 40.34 dBA

Results segment # 4: CA3 (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	1.50	1.50	1.50

ROAD (0.00 + 41.50 + 0.00) = 41.50 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
46	90	0.18	67.63	0.00	-5.63	-7.07	0.00	0.00	-13.43

SubLeq
41.50

Segment Leq : 41.50 dBA

Total Leq All Segments: 45.66 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 53.26
(NIGHT): 45.66

