

Geotechnical Investigation

Proposed Commercial Development

375 Didsbury Road
Ottawa, Ontario

Prepared for First Capital Realty Inc.

Report PG7751-1 Revision 3 dated June 22, 2026

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1.0 Introduction

Paterson Group (Paterson) was commissioned by First Capital Realty Inc. to conduct a geotechnical investigation at 375 Didsbury Road in the City of Ottawa (reference should be made to Figure 1 - Key Plan in Appendix 2 of this report for the general site location).

The objectives of the geotechnical investigation were to:

- ☐ Determine the subsoil and groundwater conditions at this site by means of test holes.
- ☐ Provide geotechnical recommendations pertaining to design of potential structures, including construction considerations which may affect the design.

This report has been prepared specifically and solely for the aforementioned project which is described herein. It contains our findings and includes geotechnical recommendations pertaining to the design and construction of the subject development as they are understood at the time of writing this report.

2.0 Proposed Development

The application is to amend the current zoning on the subject site from *Development Reserve – DR* to a *Neighbourhood Mixed-Use Zone*. There is no development or site plan for the site at this time.

The zoning is required to amend the zoning to be consistent with the surrounding land uses and implement the Official Plan designation for the lands. It is envisioned that the subject site could consist of several commercial buildings grouped on the site and connected by internal access lanes and parking areas.

It is anticipated that the Gross Floor Area of the combined uses may be in the order of 18,615 sq.metres and will be primarily slab-on-grade and single story. The application would seek an exception to also permit a gas bar, day care, residential and hotel as permitted uses.

The future commercial development would be municipally serviced.

3.0 Method of Investigation

3.1 Field Investigation

Field Program

Recent geotechnical investigations were conducted in fall 2025 and winter 2026 and consisted of advancing 38 boreholes (BH 1-25 to BH 38-25), 9 test pits (TP 1-25 to TP 9-25), and 5 cone penetration tests (CPTs) to maximum depths of 15.7 m, 3.2 m, and 35 m, respectively, below the existing ground surface.

A previous geotechnical investigation was carried out by this firm in 2004 and consisted of advancing a total of 15 boreholes (BH 1 to BH 15) to a maximum depth of 14.9 m below the existing ground surface.

The test hole locations were distributed in a manner to provide general coverage of the subject site, taking into consideration underground utilities and site features. The test hole locations are shown on Drawing PG7751-1 - Test Hole Location Plan in Appendix 2.

The boreholes were drilled and the CPTs were advanced using a track-mounted drill rig operated by a two-person crew. The test pits were completed using a hydraulic shovel and backfilled with the excavated soil upon completion. All fieldwork was conducted under the full-time supervision of Paterson personnel under the direction of a senior engineer.

Sampling and In Situ Testing

Soil samples were collected from the auger flights (AU), using a 50 mm diameter split-spoon sampler (SS), or using 73 mm diameter thin walled Shelby tubes in conjunction with a piston sampler (TW). Soil samples were also recovered from the sidewalls of the test pits (G). The bedrock was cored to assess the bedrock type and quality. All samples were visually inspected and initially classified on site. The auger, split-spoon, and grab samples were placed in sealed plastic bags, the Shelby tubes were sealed at both ends on site, and rock cores (RC) were placed in cardboard boxes. The samples were then transported to our laboratory for further examination and classification.

The depths at which the auger, split-spoon, Shelby tube, rock cores and grab samples were recovered from the test holes are shown as AU, SS, TW, RC and G respectively, on the Soil Profile and Test Data sheets presented in Appendix 1.

A Standard Penetration Test (SPT) was conducted in conjunction with the recovery of the split spoon samples. The SPT results are recorded as "N" values on the Soil Profile and Test Data sheets. The "N" value is the number of blows required to drive the split spoon sampler 300 mm into the soil after a 150 mm initial penetration using a 63.5 kg hammer falling from a height of 760 mm.

Diamond drilling was completed at borehole BH 22-25 to confirm the bedrock type and quality. A recovery value and a Rock Quality Designation (RQD) value were calculated for each drilled section of bedrock and are presented as RC on the Soil Profile and Test Data sheets in Appendix 1. The recovery value is the ratio of the bedrock sample length recovered over the drilled section length, in percentage.

The RQD value is the total length ratio of intact rock core length more than 100 mm in one drilled section over the length of the drilled section, in percentage. These values are indicative of the quality of the bedrock.

Undrained shear strength testing, using a vane apparatus, was carried out at regular intervals of depth in cohesive soils.

The overburden thickness was evaluated using a dynamic cone penetration test (DCPT) at boreholes BH 20-25, BH 21-25, BH 25-25, BH 37-25, BH 38-25, BH 1, BH 2, BH 3, BH 4, BH 5, BH 6, BH 7 and BH 9. The DCPT consists of driving a steel drill rod, equipped with a 50 mm diameter cone at the tip, using a 63.5 kg hammer falling from a height of 760 mm. The number of blows required to drive the cone into the soil is recorded for each 300 mm increment.

The CPTs were advanced using the direct push method, and measured the tip resistance, sleeve friction, and pore water pressure of the soils during penetration with the cone. Several dissipation tests were also conducted at each CPT location.

Seismic cone penetration testing (sCPT) was also completed within the central portion of the proposed building footprint (CPT D-26) to evaluate the shear wave velocity profile at the subject site. The sCPT consists of pushing the seismic probe in depth increments of 1 m and recording the velocity of a shear wave traveling through the overburden soils. The shear wave is generated by a hammer striking a shear plate seating on the ground surface.

The CPT logs and associated seismic records are presented on the Cone Penetration Testing Sheets in Appendix 1.

The subsurface conditions observed in the test holes were recorded in detail in the field. The soil profiles are logged on the Soil Profile and Test Data sheets in Appendix 1 of this report.

Groundwater

Groundwater monitoring wells were installed in boreholes BH 15-25, BH 28-25, and BH 32-25, while the remaining boreholes were fitted with flexible polyethylene standpipes, in order to permit monitoring of the groundwater levels subsequent to the completion of the sampling program. Open hole groundwater levels were recorded in the test pits.

3.2 Field Survey

The recent test hole locations, and ground surface elevation at each test hole location, were surveyed by Paterson using a handheld GPS and referenced to a geodetic datum. The locations of the test holes, and ground surface elevation at each test hole location, are presented on Drawing PG7751-1 - Test Hole Location Plan in Appendix 2.

3.3 Laboratory Review

The soil samples recovered from the subject site were examined in our laboratory to review the results of the field logging.

A total of 9 Shelby tube samples from the recent investigation and 6 Shelby tube samples from the previous investigation were submitted for unidimensional consolidation testing.

Atterberg limits testing was also conducted on 4 select soil samples, grain size distribution testing on 2 select soil samples, and shrinkage testing on 1 select soil samples.

The results of the laboratory testing are provided in Appendix 1 and discussed in Section 4.0.

3.4 Analytical Testing

Soil samples and water samples were submitted for analytical testing as per the project specifications. A total of 9 topsoil samples were submitted to determine their acidity, corrosivity, salinity, sodium absorption ratio, organic content, and their chloride, boron, aluminium, calcium carbonate, phosphorus, potassium, iron, manganese, zinc, copper, mercury, nickel, selenium, silver, and vanadium concentrations.

One water sample was also submitted for analytical testing to determine the pH, alkalinity, hardness, total dissolved solids, sulphate, fluoride, iron, copper,

aluminium, manganese, silver, zinc, chloride, nitrate, sodium, calcium and silica concentrations.

The results of the analytical testing for the topsoil samples and the water sample performed by Bureau Veritas labs are presented in Appendix 1.

4.0 Observations

4.1 Surface Conditions

The subject site is currently undeveloped with a mostly grassed surface. The site is bordered by a stormwater management pond to the north, Didsbury Road to the east, Campeau Drive to the south, and the Carp River to the west. The ground surface across the site is relatively level at approximate geodetic elevations 93 to 94 m.

4.2 Subsurface Profile

Overburden

Generally, the soil profile at the test hole locations consists of topsoil which is underlain by silty sand and/or a deep silty clay deposit.

A loose to compact, brown silty sand was observed underlying the topsoil in localized areas across the site, primarily along Campeau Drive and the western portion of the site along the Carp River. Where encountered, the silty sand was observed to extend to approximate depths of 0.7 to 3.7 m below the existing ground surface.

A silty clay deposit was encountered underlying the topsoil and/or silty sand, and was observed to consist of a stiff, brown silty clay crust, becoming a firm to soft, grey silty clay below approximate depths of 2 to 2.5 m below the existing ground surface.

Bedrock

Practical refusal to the auger or DCPT was encountered at depths ranging from 35 m near the southeast corner of the site, to 44.3 m in the central portion of the site, to 6.4 m near the northwest corner of the site. Bedrock was cored at borehole BH 22-25, where it was observed to consist of a fair to good quality sandstone.

Reference should be made to the Soil Profile and Test Data sheets in Appendix 1 for specific details of the soil profiles encountered at each test hole location.

Laboratory Testing Results

The results of the Atterberg limits testing is presented in Table 1, on the next page, and on the Atterberg Limits Testing Results sheets in Appendix 1.

Table 1 - Atterberg Limits Results						
Sample	Depth (m)	LL (%)	PL (%)	PI (%)	w (%)	Classification
BH 1-25 SS5	3.0 – 3.7	25	15	10	38.62	CL
BH 2-25 SS3	1.5 – 2.1	38	17	21	30.46	CL
BH 11-25 G4	4.5 – 4.9	36	19	17	43.68	CL
BH 15-25 SS6	3.8 – 4.4	27	16	11	38.18	CL
Notes: LL: Liquid Limit; PL: Plastic Limit; PI: Plasticity Index; w: water content; CL: Inorganic Clays of Low Plasticity						

Grain size distribution (sieve and hydrometer analysis) was also completed on 2 selected soil samples. The results of the grain size analysis are summarized in Table 2 and are presented on the Grain Size Distribution and Hydrometer Testing Results sheet in Appendix 1.

Table 2 - Summary of Grain Size Distribution Analysis					
Test Hole	Sample	Gravel (%)	Sand (%)	Silt (%)	Clay (%)
BH 13-25	SS4	0.0	8.9	56.1	35.0
BH 18-25	SS3	0.0	15.2	53.3	31.5

Linear shrinkage testing was completed on a sample recovered from a depth of 3.0 to 3.6 m below ground surface from borehole BH 8-25, and yielded a shrinkage limit of 15.08 and a shrinkage ratio of 1.98.

One-dimensional consolidation testing was conducted on 9 samples from the recent geotechnical investigation, and 6 samples from the previous geotechnical investigation. The results are summarized in Table 3 on the next page, and are presented in Appendix 2.

Table 3 – Summary of Consolidation Testing Results

Test Hole	Sample	Depth (m)	p'_c	p'_o	C_{cr}	C_c	OCR
BH 21-25*	TW5	4.57	76.40	49.90	0.013	0.329	1.5
BH 23-25	TW7	5.33	96.67	54.19	0.014	1.867	1.8
BH 25-25	TW4	6.86	105.02	63.29	0.015	0.940	1.7
BH 31-25	TW4	3.81	90.00	41.77	0.015	0.816	2.2
BH 32-25	TW5	4.57	53.12	75.91	0.018	0.470	1.4
BH 33-25*	TW8	7.62	100.00	67.28	0.015	0.526	1.5
BH 34-25	TW4	6.10	110.37	58.89	0.016	1.015	1.9
BH 35-25*	TW4	3.05	61.27	31.83	0.025	0.351	1.9
BH 38-25	TW7	4.57	64.14	62.95	0.014	0.470	1.0
Previous Investigations							
Test Hole	Sample	Depth (m)	p'_c	p'_o	C_{cr}	C_c	OCR
BH 1	TW 1	2.7	73	36	0.020	0.64	2.0
BH 1	TW 3	12.5	126	112	0.031	1.60	1.1
BH 2	TW 1	5.0	122	54	0.014	1.80	2.3
BH 5	TW 1	6.4	69	64	0.016	0.63	1.1
BH 9	TW 1	7.2	190	73	0.013	2.46	2.6
BH 9	TW 2	9.5	174	91	0.018	1.68	1.9
* - Likely Disturbed Sample							

4.3 Groundwater

The measured groundwater levels at the test hole locations are presented on Table 4 on the next page. However, it should be noted that groundwater levels are subject to seasonal fluctuations. Therefore, the groundwater levels could vary at the time of construction.

Table 4 - Summary of Groundwater Levels
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Test Hole Number	Ground Surface Elevation (m)	Measured Groundwater Level		Dated Recorded
		Depth (m)	Elevation (m)	
BH 1-25	94.64	6.85	87.79	December 5, 2025
BH 2-25	94.31	5.76	88.55	December 5, 2025
BH 3-25	94.17	4.45	89.72	December 5, 2025
BH 4-25	93.76	5.85	87.91	December 5, 2025
BH 5-25	93.24	1.40	91.84	December 5, 2025
BH 6-25	93.79	6.17	87.62	December 5, 2025
BH 7-25	93.36	2.89	90.47	December 5, 2025
BH 8-25	93.01	1.10	91.91	December 5, 2025
BH 9-25	92.95	0.65	92.3	December 5, 2025
BH10-25	93.27	Dry/Blocked		December 5, 2025
BH11-25	93.50	Dry/Blocked		December 5, 2025
BH12-25	93.62	Dry/Blocked		December 5, 2025
BH13-25	93.81	5.70	88.11	December 5, 2025
BH14-25	93.75	5.08	88.67	December 5, 2025
BH15-25*	94.20	3.50	90.7	December 5, 2025
BH16-25	93.76	3.10	90.66	December 5, 2025
BH17-25	93.60	3.30	90.3	December 5, 2025
BH18-25	93.25	3.17	90.08	December 5, 2025
BH19-25	93.34	2.20	91.14	December 5, 2025
BH20-25	94.16	8.06	86.1	December 5, 2025
BH21-25	93.33	2.50	90.83	December 5, 2025
BH22-25	93.38	4.90	88.48	December 5, 2025
BH23-25	93.30	1.24	92.06	December 5, 2025
BH24-25	93.75	3.20	90.55	December 5, 2025
BH25-25*	93.47	7.40	86.07	December 5, 2025
BH26-25	93.64	7.75	85.89	December 5, 2025
BH27-25	93.63	Dry/Blocked		December 5, 2025
BH28-25	93.78	2.75	91.03	December 5, 2025
BH29-25	93.02	1.10	91.92	December 5, 2025
BH30-25	92.92	1.10	91.82	December 5, 2025
BH31-25	93.58	8.04	85.54	December 5, 2025
BH32-25	93.89	Dry/Blocked		December 5, 2025
BH33-25	93.54	2.80	90.74	December 5, 2025
BH34-25	92.87	1.15	91.92	December 5, 2025
BH35-25	92.87	0.42	92.45	December 5, 2025

BH36-25	93.49	1.46	92.03	December 5, 2025
BH37-25	93.18	Dry/Blocked		December 5, 2025
BH38-25	94.29	3.64	90.65	December 5, 2025
Previous Investigations				
Test Hole Number	Ground Surface Elevation (m)	Measured Groundwater Level		Date Recorded
		Depth (m)	Elevation (m)	
TP 15-21	67.52	3.00	64.52	November 16, 2021
BH 3*	71.57	3.87	67.70	September 18, 2019
BH 4	67.49	Inaccessible	-	September 27, 2019
BH 5	68.91	Inaccessible	-	September 27, 2019
BH 6*	70.60	1.01	69.59	September 18, 2019
BH 7	71.39	2.19	69.20	September 27, 2019
BH 8	68.59	3.76	64.83	September 27, 2019
BH 9*	70.95	1.17	69.78	September 18, 2019
BH 10	70.69	Blocked	-	September 27, 2019
BH 11	66.78	Blocked	-	September 27, 2019
Note: The ground surface elevation at each test hole location was surveyed using a handheld GPS using a geodetic datum. *Denotes Groundwater Monitoring Well				

All test pits, with the exception of TP 15-21, were observed to be dry upon completion.

The recorded groundwater levels are also provided on the applicable Soil Profile and Test Data sheet presented in Appendix 1.

Dissipation testing was also conducted at each CPT location to measure the T_{50} dissipation period. These results are attached in Appendix 1.

5.0 Discussion

5.1 Geotechnical Assessment

The subject site is considered suitable for the proposed commercial development and zoning application from a geotechnical perspective. Due to the presence of a deep clay deposit throughout the subject site, the proposed development will be subject to grade raise restrictions that would also influence the type of foundations a structure could be supported by.

While details are not currently known, it is expected common low-rise slab-on-grade commercial plaza structures would be able to be supported by conventional spread footings foundations founded upon the undisturbed, compact silty sand or undisturbed, stiff silty clay bearing mediums. Commercial structures that have heavier loading requirements, such as those with high racking loads, storage live loads and other types of similar uses, may be supported by either deep foundation or conventional spread footings in conjunction with lightweight fill or be supported by a preloading/surcharging program. This is discussed further in Section 5.3 of this report.

Due to limited information known at the time of preparing this report, all recommendations provided herein are only considered preliminary and subject to further review and refinement once design details for contemplated development concepts are available for geotechnical input. These recommendations are considered suitable to support the current zoning application from a geotechnical perspective and would be assessed at a later stage of design once design concepts are available for geotechnical review and input. At this time, the recommendations are considered suitable for discussion and preliminary planning purposes only.

The above and other considerations are further discussed in detail in the following sections.

5.2 Site Grading and Preparation

Stripping Depth

Topsoil and deleterious fill, such as those containing organic materials, should be stripped from under any buildings, paved areas, pipe bedding and other settlement sensitive structures.

Subgrade Preparation

If a silty sand subgrade is encountered at the underside of slab or footing elevation and observed to be in a loose state of compactness, the material should be proof rolled using suitable vibratory equipment making several passes under dry conditions and above freezing temperatures, and approved by Paterson at the time of construction.

Fill Placement

Fill placed for grading beneath the proposed buildings should consist, unless otherwise specified, of clean imported granular fill, such as Ontario Provincial Standard Specifications (OPSS) Granular A or Granular B Type II. The imported fill material should be tested and approved prior to delivery. The fill should be placed in maximum 300 mm thick loose lifts and compacted using suitable compaction equipment. Fill placed beneath the building should be compacted to a minimum of 98% of the standard Proctor maximum dry density (SPMDD).

Site-excavated silty sand could be placed as general landscaping fill and beneath exterior parking where settlement of the ground surface is of minor concern. These materials should be spread in lifts with a maximum thickness of 300 mm and compacted by the tracks of the spreading equipment to minimize voids. If this material is to be used to build up the subgrade level for areas to be paved, it should be compacted in thin lifts to at least 95% of the material's SPMDD.

Preload/Surcharge Program with Wick Drains

As discussed above, if a scenario arises where the combined loads from the grade raise fill and structural loading would lead to settlements that would exceed typical settlement criteria surcharging would be advisable. If lightweight fill is either too costly or insufficient to resolve loading constraints, surcharging would be recommended to be undertaken. Depending on the magnitude of surcharge that would be undertaken, the time to complete the surcharge program may be significantly reduced by the implementation of wick drains.

Wick drains consist of pre-fabricated, corrugated plastic drainage channels which are covered in geotextile. They are installed using a steel mandrel attached to an excavator, which advances the pre-fabricated wick drain to the required depth on a pre-determined grid pattern. The purpose of the wick drains is to accelerate the consolidation settlement of the silty clay deposit under a preload/surcharge pile.

Wick drains are typically designed and installed by a specialty ground improvement contractor. The wick drain design should be provided as a submittal in advance of construction, for review and approval by Paterson.

All of these design recommendations may be determined once concept plans and associated grading and building footprint and loading configurations are available to review from a geotechnical perspective.

Granular fill material could potentially be used to build the preload/surcharge pile and then re-used later on-site for the pavement base and sub-base in paved areas. The final height and dimensions of the preload/surcharge pile, if deemed appropriate and suitable for a future development, will be determined by Paterson once the proposed building details become finalized.

5.3 Foundation Design

Strip footings, up to 2 m wide, and pad footings, up to 4 m wide, placed on an undisturbed, compact silty sand or undisturbed, stiff silty clay bearing surface, **at or above geodetic elevation 93.0 m**, can be designed using a bearing resistance value at serviceability limit states (SLS) of **80 kPa** and a factored bearing resistance value at ultimate limit states (ULS) of **120 kPa**. All footings shall have a minimum dimension of 0.5 m.

These values are dependent on review of future grading plans and other loading proposed structures will contribute to stressing the underlying subsoils and are considered suitable for preliminary discussion purposes but are not considered applicable to detailed design at this time.

An undisturbed soil bearing surface consists of one from which all topsoil and deleterious materials, such as loose, frozen or disturbed soil, whether in situ or not, have been removed, in the dry, prior to placement of concrete for footings. The undisturbed, compact silty sand or undisturbed, stiff silty clay bearing surfaces should be inspected by qualified geotechnical personnel from Paterson prior to foundation construction.

The bearing resistance value at SLS for footings bearing on the above-noted soils, in conjunction with the completion of a successful preload/surcharge program for the proposed commercial building, will be subjected to potential post-construction total and differential settlements of 25 and 20 mm, respectively.

Lateral Support

The bearing medium under footing-supported structures is required to be provided with adequate lateral support with respect to excavations and different foundation levels.

Adequate lateral support is provided to a stiff silty clay, compact silty sand, or engineered fill above the groundwater table when a plane extending down and out from the bottom edge of the footing at a minimum of 1.5H:1V passes only through in situ soil of the same or higher capacity as the bearing medium soil.

Permissible Grade Raise Recommendation

For asphalt-paved access lanes and parking areas beyond the limits of the proposed commercial building, permissible grade raise restrictions are required in order to mitigate excessive post-construction settlements.

At this time, the permissible grade raise restriction varies and may range between approximately **0.5** and **1.2 m** for building footprints across the subject site. The areas of each grade raise restriction magnitude would be delineated on a plan at a later stage of conceptual design and once grading concepts can be assessed such that these values are provided for discussion and preliminary discussion purposes only.

It should be noted that the permissible grade raise values provided are based on typical fill materials with a unit weight of 18 kN/m^3 below the pavement structure, and a unit weight of 22 kN/m^3 for the pavement structure. If heavier fill materials, such as blast rock, are used to raise the grade below the pavement structure, then the permissible grade raise restriction would need to be reduced.

It should also be noted that the permissible grade raise restriction within the building footprint accounts for the loads on the slab-on-grade, therefore, if the building locations shift, the permissible grade raise restrictions would need to be adjusted.

If higher than permissible grade raises are required for asphalt-paved access lanes and parking areas located beyond the buildings, then preloading with or without a surcharge, lightweight fill, and/or other measures should be investigated to reduce the risks of unacceptable long-term, post construction total and differential settlements.

5.4 Design for Earthquakes

The sCPT was completed at the subject site to accurately determine the applicable seismic site classification for proposed structures in accordance with Table 4.1.8.4.A of the Ontario Building Code (OBC) 2024. The sCPT equipment consisted of a 2-component geophone mounted behind the CPT cone.

The geophone is also connected to the GP Seismic System which records the velocity of the shear waves as they propagate down through the overburden. Recordings for the testing were completed at 1 m intervals.

The GP Seismic System is also connected to a computer laptop and the trigger system. The trigger system consists of a trigger attached to a hammer, and a shear plate which is weighted down by the drill rig used to push the cone. The hammer is used to strike the shear plate creating a shear wave that travels to the geophone. The hammer shots are repeated between 4 to 8 times at each shot location to improve the signal to noise ratio.

Interpretation of sCPT was completed by Paterson personnel using DI Viewer Software package (Geoprobe Systems). The processing sequence consisted of data quality control followed by interpretation of arrival points and calculation of the corresponding shear wave velocity profile.

The average shear wave velocity in the upper 30 m of the soil profile (V_{s30}) was calculated considering the standard equation for average shear wave velocity provided in OBC 2024 and as presented below:

$$V_{s30} = \frac{Depth_{of\ interest}(m)}{\left(\sum_{i=1}^N \frac{H_i}{V_{s_i}}\right)}$$
$$Depth_{of\ interest}(m) = \sum_{i=1}^N H_i$$

Where N is the number of layers, H_i represents the thickness of layer i , and V_{s_i} is the shear wave velocity for layer i . Based on the above,

$$V_{s30} = 155\ m/s$$

The site class for seismic site designation can therefore be taken as **Class X₁₅₅**. Soils underlying the subject site are not susceptible to liquefaction or cyclic softening. Reference should be made to the latest version of the OBC 2024 for a full discussion of the earthquake design requirements.

5.5 Slab on Grade Construction

With the removal of all topsoil and deleterious materials within the footprints of buildings, the silty sand or silty clay subgrade will be considered an acceptable subgrade surface on which to commence backfilling for floor slab construction. The upper 200 mm of sub-slab fill should consist of an OPSS Granular A crushed stone. All backfill material within the footprint of a proposed building should be placed in maximum 300 mm thick loose lifts and compacted to at least 98% of its SPMDD.

Any soft areas should be removed and backfilled with appropriate backfill material. OPSS Granular B Type II, with a maximum particle size of 50 mm, are recommended for backfilling below the floor slab.

5.6 Pavement Design

Car only parking areas, access lanes and heavy truck parking areas are anticipated at this site. The proposed pavement structures are shown in Tables 5 and 6.

Table 5 - Recommended Pavement Structure Car Only Parking Areas	
Thickness (mm)	Material Description
50	Wear Course - HL-3 or Superpave 12.5 Asphaltic Concrete
150	BASE - OPSS Granular A Crushed Stone
300	SUBBASE - OPSS Granular B Type II
SUBGRADE - Either fill, in situ soil, or OPSS Granular B Type I or II material placed over in situ soil or fill	

Table 6 - Recommended Pavement Structure Access Lanes and Heavy Truck Parking Areas	
Thickness (mm)	Material Description
40	Wear Course - Superpave 12.5 Asphaltic Concrete
50	Binder Course - Superpave 19.0 Asphaltic Concrete
150	BASE - OPSS Granular A Crushed Stone
450	SUBBASE - OPSS Granular B Type II
SUBGRADE - Either fill, in situ soil, or OPSS Granular B Type I or II material placed over in situ soil or fill	

Minimum Performance Graded (PG) 58-34 asphalt cement should be used for this project. The pavement granular base and subbase should be placed in maximum 300 mm thick lifts and compacted to a minimum of 99% of the material's SPMDD using suitable vibratory equipment, noting that excessive compaction can result in subgrade softening.

If soft spots develop in the subgrade during compaction or due to construction traffic, the affected areas should be excavated and replaced with OPSS Granular B Type I or II material.

Pavement Structure Drainage

Satisfactory performance of the pavement structure is largely dependent on the contact zone between the subgrade material and the base stone in a dry condition. Failure to provide adequate drainage under conditions of heavy wheel loading can result in the fine subgrade soil being pumped into the voids in the stone subbase, thereby reducing load carrying capacity.

Where silty clay is anticipated at subgrade level, consideration should be given to installing subdrains during the pavement construction as per City of Ottawa standards. The subdrain inverts should be approximately 300 mm below subgrade level, and the subgrade surface should be crowned to promote water flow to drainage lines.

6.0 Design and Construction Precautions

6.1 Foundation Drainage and Backfill

A perimeter foundation drainage system is considered optional for slab-on-grade structures at the subject site, as it would help minimize frost heave of paved and landscaped areas in the vicinity of proposed buildings. Where utilized, the system should consist of a 150 mm diameter perforated corrugated plastic pipe, surrounded on all sides by 150 mm of 19 mm clear crushed stone which is placed at the footing level around the exterior perimeter of the structures. The pipe should have a positive outlet, such as a gravity connection to the storm sewer.

Backfill against the exterior sides of the foundation walls should consist of free-draining non frost susceptible granular materials, such as clean sand or OPSS Granular B Type I granular material. The greater part of the site excavated materials will be frost susceptible and, as such, are not recommended for re-use as backfill against the foundation walls. A geocomposite drainage board, such as Miradrain G100N or Delta Drain 6000, connected to the perimeter foundation drainage system is recommended.

6.2 Protection of Footings Against Frost Action

Perimeter foundations of heated structures are required to be insulated against the deleterious effects of frost action. A minimum of 1.5 m of soil cover, or an equivalent combination of soil cover and foundation insulation, should be provided for adequate frost protection of heated structures.

Exterior unheated footings, such as those for isolated exterior piers or loading docks, are more prone to deleterious movement associated with frost action than the exterior walls of the heated structure and require additional protection, such as soil cover of 2.1 m or an equivalent combination of soil cover and foundation insulation.

6.3 Excavation Side Slopes

The side slopes of excavations in the soil and fill overburden materials should either be cut back at acceptable slopes or should be retained by shoring systems from the start of the excavation until the structure is backfilled. It is expected that sufficient room will be available for the greater part of the excavation to be undertaken by open-cut methods (i.e., unsupported excavations).

The excavation side slopes above the groundwater level extending to a maximum depth of 3 m should be cut back at 1H:1V or flatter. The flatter slope is required for excavation below groundwater level. Excavations below the groundwater level should be cut back at a maximum slope of 1.5H:1V. The subsoil at this site is considered to be mainly a Type 2 and 3 soil according to the Occupational Health and Safety Act and Regulations for Construction Projects.

Excavated soil should not be stockpiled directly at the top of excavations and heavy equipment should be kept away from the excavation sides.

Slopes in excess of 3 m in height should be periodically inspected by the geotechnical consultant in order to detect if the slopes are exhibiting signs of distress.

It is recommended that a trench box be used at all times to protect personnel working in trenches with steep or vertical sides. It is expected that services will be installed by “cut and cover” methods and excavations will not be left open for extended periods of time.

Excavation Base Stability

The base of supported excavations can fail by 3 general modes:

- ❑ Shear failure within the ground caused by inadequate resistance to loads imposed by grade difference inside and outside of the excavation,
- ❑ Piping from water seepage through granular soils, and
- ❑ Heave of layered soils due to water pressures confined by intervening low permeability soils.

The potential for base heave in cohesive soils should be determined for stability of flexible retaining systems. The factor of safety with respect to basal heave, FS_b , is:

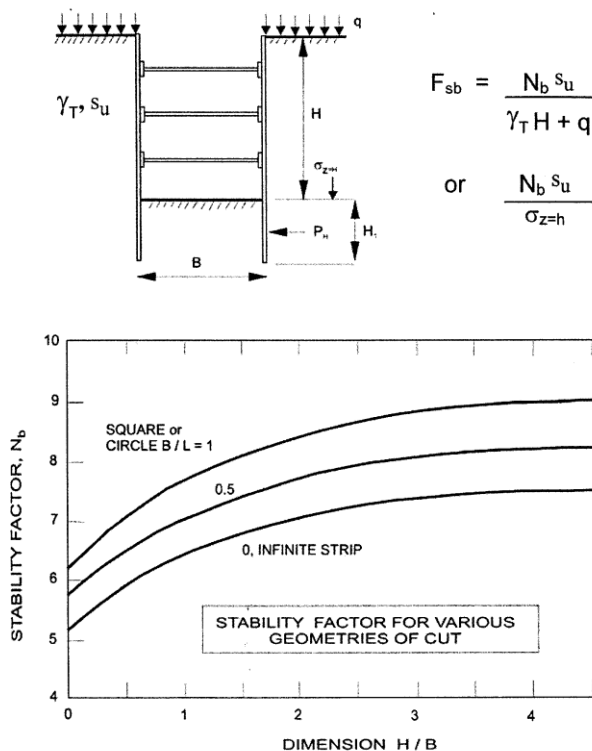
$$FS_b = \frac{N_b s_u}{\sigma_z}$$

where:

N_b - stability factor dependent upon the geometry of the excavation and given in Figure 1 on the following page.

s_u - undrained shear strength of the soil below the base level

σ_z - total overburden and surcharge pressures at the bottom of the excavation



In the case of stiff clays or compact to dense sands, a factor of safety of 2 is recommended for base stability.

6.4 Pipe Bedding and Backfill

Bedding and backfill materials should be in accordance with the most recent Material Specifications and Standard Detail Drawings from the Department of Public Works and Services, Infrastructure Services Branch of the City of Ottawa.

The pipe bedding for sewer and water pipes should consist of at least 150 mm of OPSS Granular A material. Where the bedding is located within the firm grey silty clay, the thickness of the bedding material should be increased to a minimum of 300 mm as directed by the geotechnical consultant at the time of construction. The material should be placed in maximum 300 mm thick lifts and compacted to a minimum of 99% of its SPMDD. The bedding material should extend at least to the spring line of the pipe.

The cover material, which should consist of OPSS Granular A, should extend from the spring line of the pipe to at least 300 mm above the obvert of the pipe. The material should be placed in maximum 300 mm thick lifts and compacted to a minimum of 95% of its SPMDD.

It should generally be possible to re-use the moist (not wet) brown silty clay above the cover material if the excavation and filling operations are carried out in dry weather conditions. Wet silty clay materials will be difficult to re-use, as the high-water contents make compacting impractical without an extensive drying period. Where hard surface areas are considered above the trench backfill, the trench backfill material within the frost zone (about 1.8 m below finished grade) should match the soils exposed at the trench walls to reduce potential differential frost heaving. The trench backfill should be placed in maximum 300 mm thick loose lifts and compacted to a minimum of 95% of the material's SPMDD.

To reduce long-term lowering of the groundwater at this site, clay seals should be provided within the service trenches excavated through the silty clay deposit. The seals should be at least 1.5 m long (in the trench direction) and should extend from trench wall to trench wall. The seals should extend from the frost line and fully penetrate the bedding, subbedding and cover material. The barriers should consist of relatively dry and compactable brown silty clay placed in maximum 300 mm thick loose layers and compacted to a minimum of 95% of the SPMDD. The clay seals should be placed at the site boundaries and at strategic locations at no more than 60 m intervals in the service trenches excavated through the silty clay deposit.

6.5 Groundwater Control

Groundwater Control for Building Construction

It is anticipated that groundwater infiltration into excavations should be controllable using open sumps. The contractor should be prepared to direct water away from all bearing surfaces and subgrades, regardless of the source, to prevent disturbance to the founding medium.

Dewatering Permit

Under the current regulations enacted by the Ministry of Environment, Conservation and Parks (MECP), any dewatering in excess of 50,000 L/day requires a registration on the Environmental Activity and Sector Registry (EASR), provided that dewatering is related to construction. If the dewatering is not related to construction, a Permit to Take Water obtained from the MECP will be required.

In the event that an EASR is required to facilitate dewatering of the proposed development, a minimum of 3 to 4 weeks should be allotted for completion of the EASR registration and the Water Taking and Discharge Plan, to be prepared by a Qualified Person as stipulated under O.Reg. 63/16. Should a Permit to Take Water be required, a minimum of five to six months should be allotted for completion of the permit, due to the minimum review period imposed by the MECP.

Impacts on Neighbouring Properties

As the proposed buildings are anticipated to be slab-on-grade structures, it is not anticipated that they would be founded below the long-term groundwater level. As a result, long-term groundwater lowering is not anticipated, and therefore no adverse effects are expected to neighboring properties.

6.6 Winter Construction

Precautions must be taken if winter construction is considered for this project. The subsoil conditions at this site consist of frost susceptible materials. In the presence of water and freezing conditions, ice could form within the soil mass. Heaving and settlement upon thawing could occur.

In the event of construction during below zero temperatures, the founding stratum should be protected from freezing temperatures using straw, propane heaters and tarpaulins or other suitable means. In this regard, the base of the excavations should be insulated from sub-zero temperatures immediately upon exposure and until such time as heat is adequately supplied to the building and the footings are protected with sufficient soil cover to prevent freezing at founding level.

Trench excavations and pavement construction are also difficult activities to complete during freezing conditions without introducing frost into the subgrade or in the excavation walls and bottoms. Precautions should be taken if such activities are to be carried out during freezing conditions. Additional information could be provided, if required.

6.7 Tree Planting Setbacks

Paterson completed a soils review of the site to determine the applicable tree planting setbacks, in accordance with the City of Ottawa's Tree Planting in Sensitive Marine Clay Soils (2017 Guidelines). Atterberg limits testing was completed for selected silty clay samples. Sieve analysis testing was also completed on selected soil samples. The results of the testing are presented in Tables 1 and 2 in Section 4.2 and in Appendix 1.

Based on the results of our review, the plasticity index of the silty clay deposit at the subject site does not exceed 40%. Therefore, the following tree planting setbacks are recommended for the silty clay deposit. Large trees (mature height over 14 m) can be planted within the silty clay areas provided a tree to foundation setback equal to the full mature height of the tree can be provided (e.g., in a park or other green space).

Tree planting setback limits may be reduced to **4.5 m** for small (mature height up to 7.5 m) and medium size trees (mature tree height 7.5 to 14 m), provided that the conditions noted below are met.

- ☐ The underside of footing (USF) is 2.1 m or greater below the lowest finished grade must be satisfied for footings within 10 m from the tree, as measured from the centre of the tree trunk and verified by means of the Grading Plan as indicated procedural changes below.
- ☐ A small tree must be provided with a minimum 25 m³ of available soil volume while a medium tree must be provided with a minimum of 30 m³ of available soil volume, as determined by the Landscape Architect. The developer is to ensure that the soil is generally un-compacted when backfilling in street tree planting locations.
- ☐ The tree species must be small (mature tree height up to 7.5 m) to medium size (mature tree height 7.5 m to 14 m) as confirmed by the Landscape Architect.
- ☐ The foundation walls are to be reinforced at least nominally (minimum of two upper and two lower 15M bars in the foundation wall).
- ☐ Grading surrounding the tree must promote drainage to the tree root zone (in such a manner as not to be detrimental to the tree).

It is well documented in the literature, and is our experience, that fast-growing trees located near buildings founded on cohesive soils that shrink on drying can result in long-term differential settlements of the structures. Tree varieties that have the most pronounced effect on foundations are seen to consist of poplars, willows, and some maples (i.e., Manitoba Maples) and, as such, they should not be considered in the landscaping design.

7.0 Recommendations

It is recommended that the following be carried out by Paterson once details of the proposed development are available:

- ☐ Review of conceptual, detailed grading, servicing, landscaping and structural plan(s), from a geotechnical perspective.

It is a requirement for the foundation design data provided herein to be applicable that a material testing and observation program be performed by the geotechnical consultant. The following aspects of the program should be performed by Paterson:

- ☐ Observation of all bearing surfaces prior to the placement of concrete.
- ☐ Sampling and testing of the concrete and fill materials used.
- ☐ Periodic observation of the condition of unsupported excavation side slopes in excess of 3 m in height, if applicable.
- ☐ Observation of all subgrades prior to backfilling.
- ☐ Field density tests to determine the level of compaction achieved.
- ☐ Sampling and testing of the bituminous concrete, including mix design reviews.

A report confirming that these works have been conducted in general accordance with our recommendations could be issued upon the completion of a satisfactory inspection program by the geotechnical consultant.

All excess soils generated by construction activities that will be transported on-site or off-site should be handled as per *Ontario Regulation 406/19: On-Site and Excess Soil Management*.

8.0 Statement of Limitations

The recommendations provided are in accordance with the present understanding of the project. Paterson requests permission to review the recommendations when the drawings and specifications are completed.

A soils investigation is a limited sampling of a site. Should any conditions at the site be encountered which differ from those at the test locations, Paterson requests immediate notification to permit reassessment of our recommendations.

The recommendations provided herein should only be used by the design professionals associated with this project. They are not intended for contractors bidding on or undertaking the work. The latter should evaluate the factual information provided in this report and determine the suitability and completeness for their intended construction schedule and methods. Additional testing may be required for their purposes.

The present report applies only to the project described in this document. Use of this report for purposes other than those described herein or by person(s) other than First Capital Realty Inc., or its agents, is not authorized without review by Paterson for the applicability of our recommendations to the alternative use of the report.

Paterson Group Inc.



Nicholas F. R. Versolato, P.Eng., ing.



Drew Petahtegoose, P.Eng.



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- ☐ Paterson Group (1 copy)

APPENDIX 1

SOIL PROFILE AND TEST DATA SHEETS

SYMBOLS AND TERMS

CONE PENETRATION TESTING LOGS

DISSIPATION TESTING RESULTS

GRAIN SIZE DISTRIBUTION AND HYDROMETER TESTING RESULTS

ATTERBERG LIMITS TESTING RESULTS

SHRINKAGE TESTING RESULTS

CONSOLIDATION TESTING RESULTS

ANALYTICAL TESTING RESULTS

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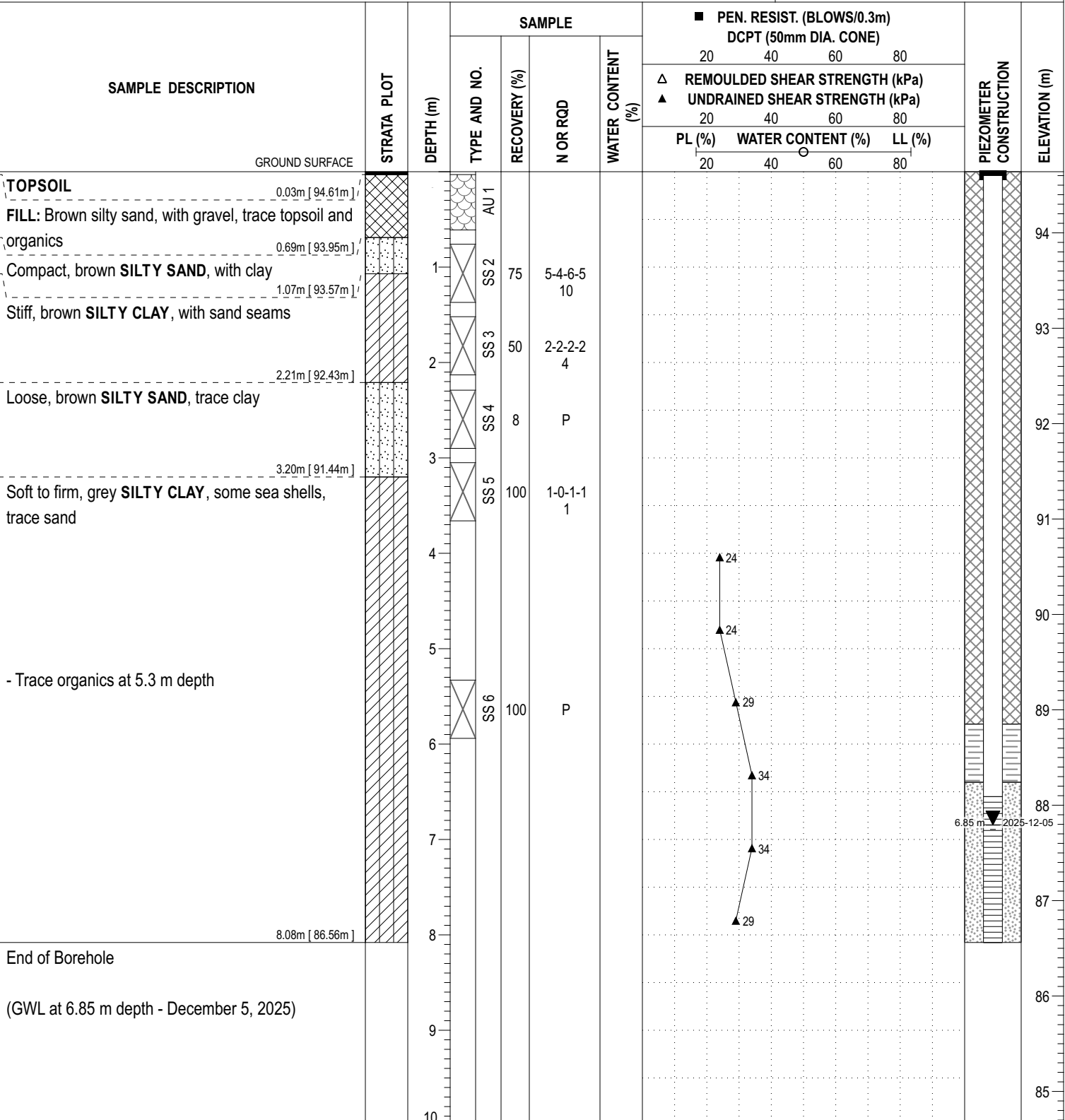
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PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: October 29, 2025

HOLE NO. : BH 1-25


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NORTHING: 5018753.24

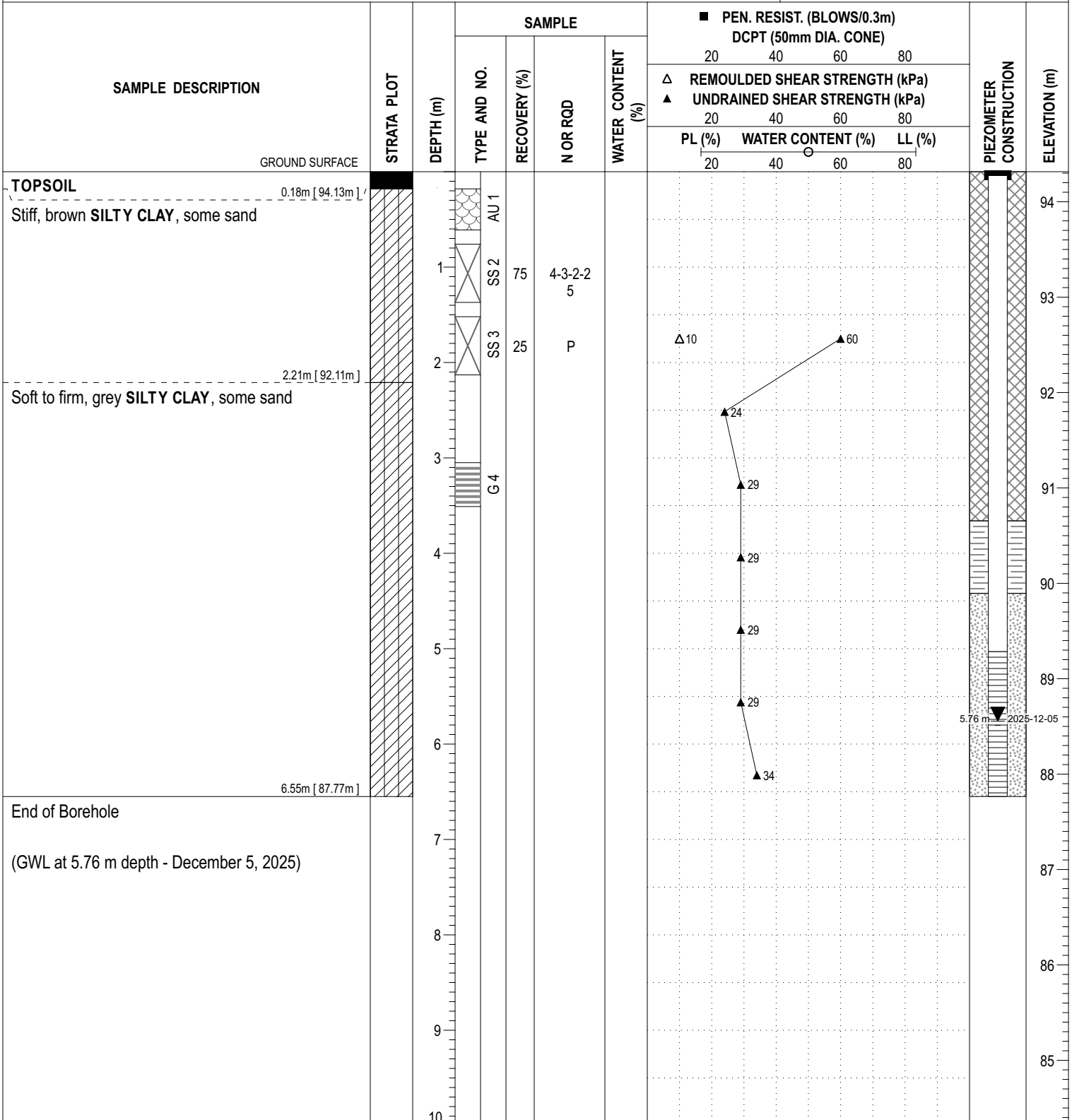
ELEVATION: 94.31

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: October 29, 2025

HOLE NO. : BH 2-25


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COORD. SYS.: MTM ZONE 9

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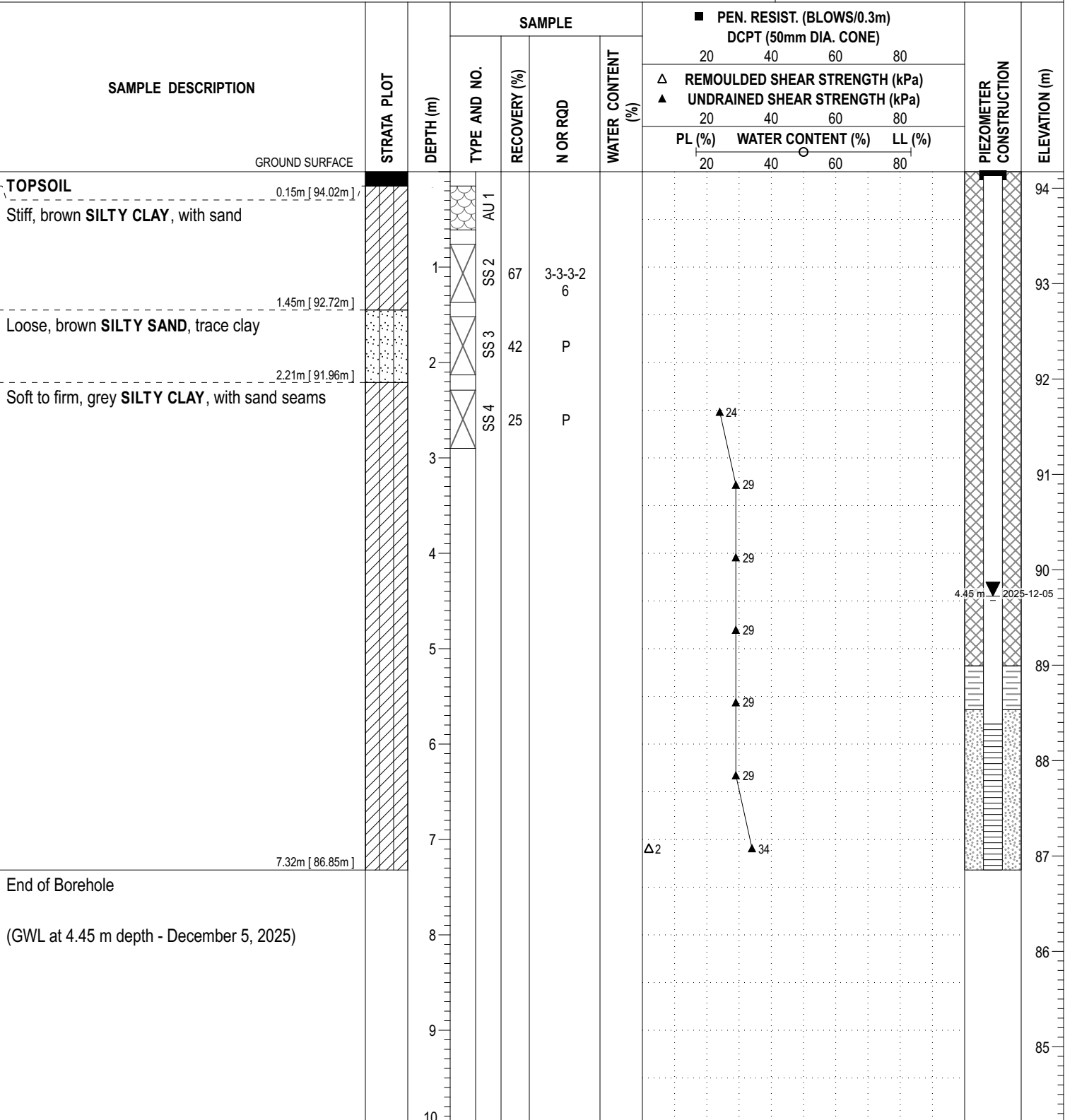
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PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: October 29, 2025

HOLE NO. : BH 3-25


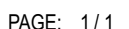
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ELEVATION: 93.76

FILE NO. : PG7751

HOLE NO. : BH 4-25

DATE: October 29, 2025



ELEVATION: 93.24

FILE NO. : PG7751

HOLE NO.: BH 5-25

DATE: October 30, 2025

PAGE: 1 / 1

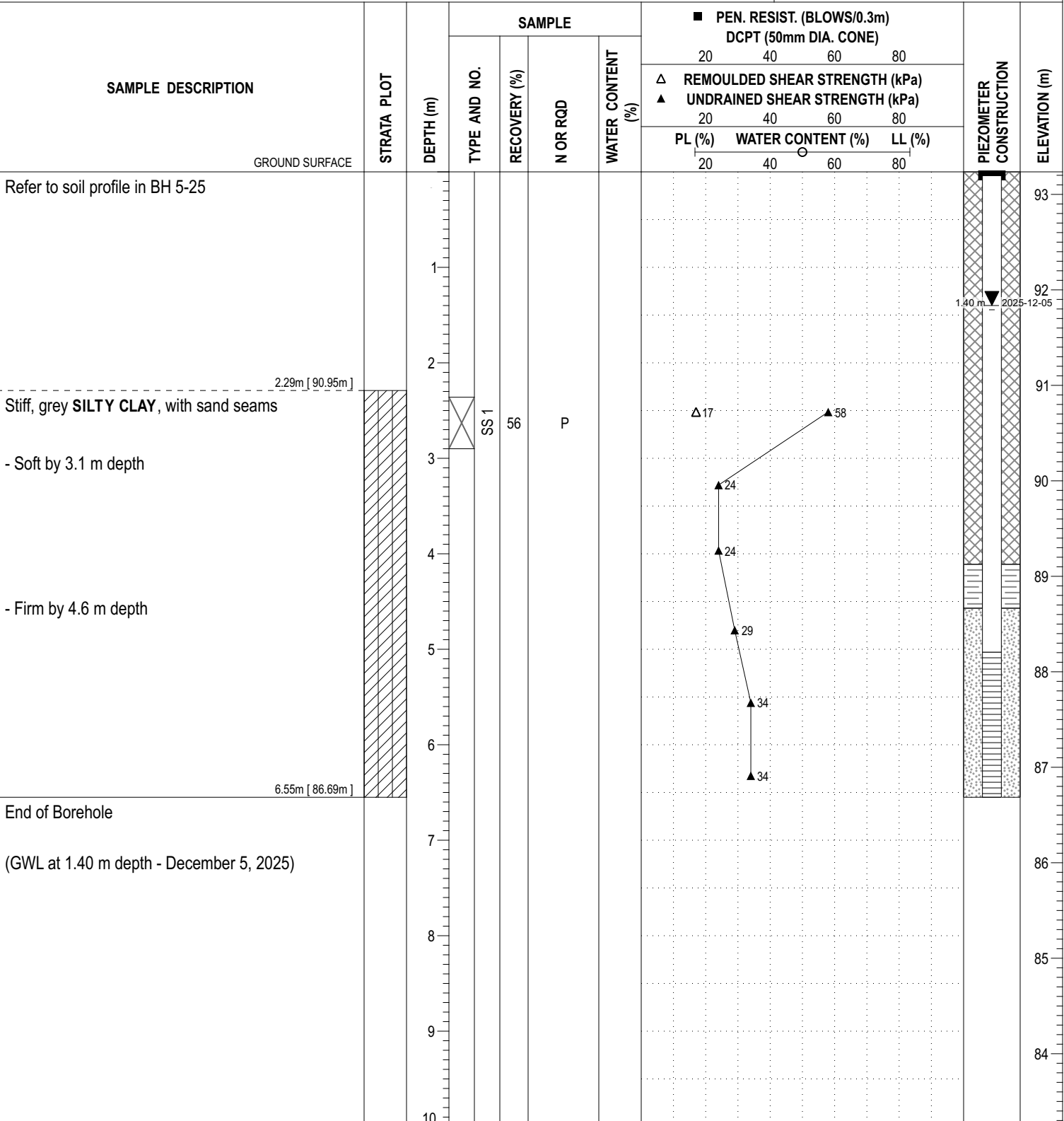
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PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: October 30, 2025

HOLE NO. : BH 5A-25


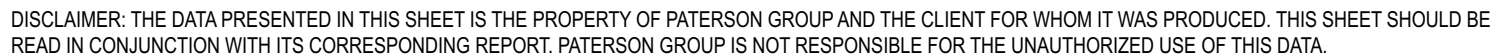
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ELEVATION: 93.79

FILE NO. : PG7751

HOLE NO. : BH 6-25

DATE: October 30, 2025



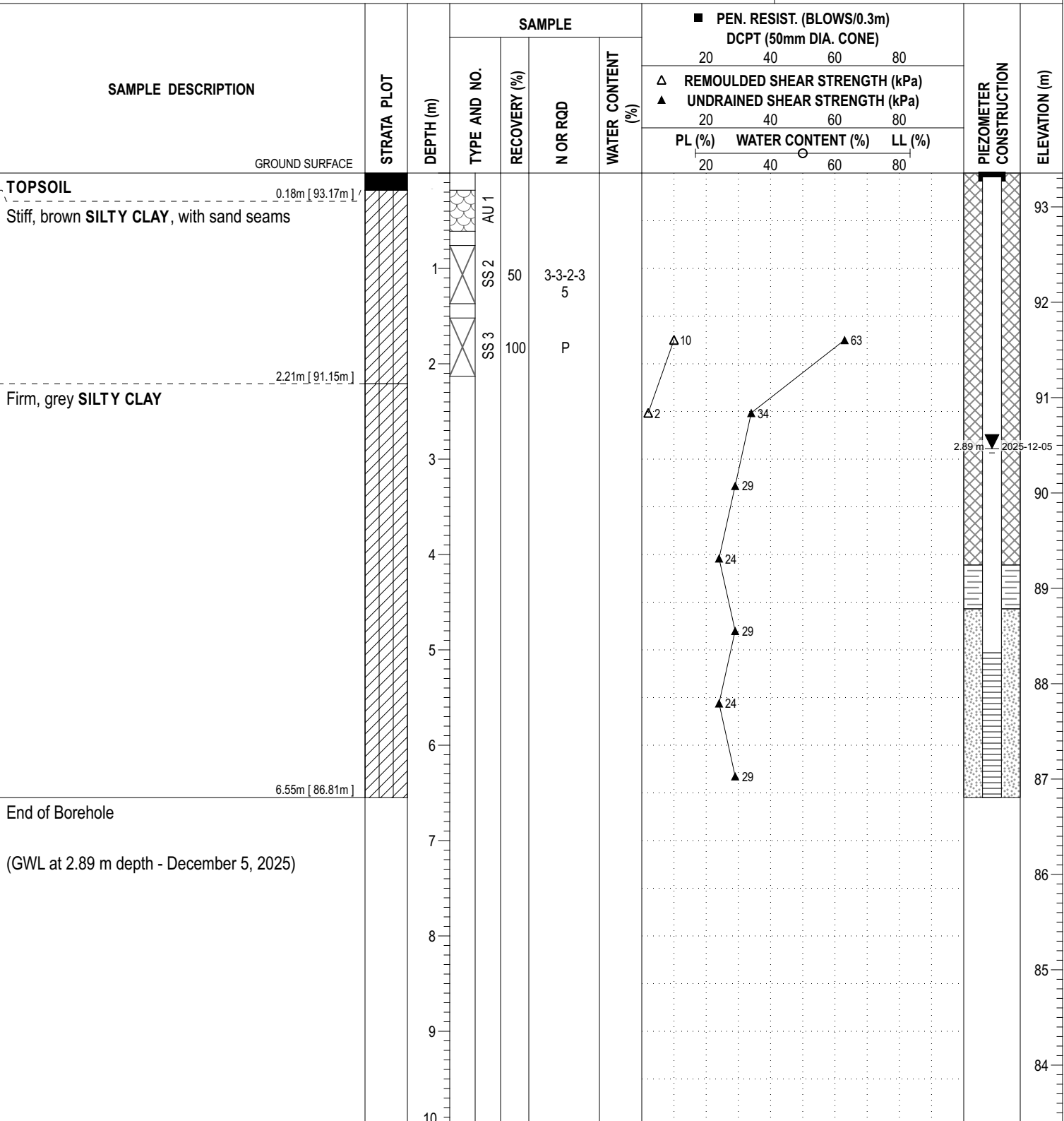


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PROJECT: Proposed Commercial Development **FILE NO. :** PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS: **DATE:** October 30, 2025 **HOLE NO. :** BH 7-25



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ELEVATION: 93.01

FILE NO. : PG7751

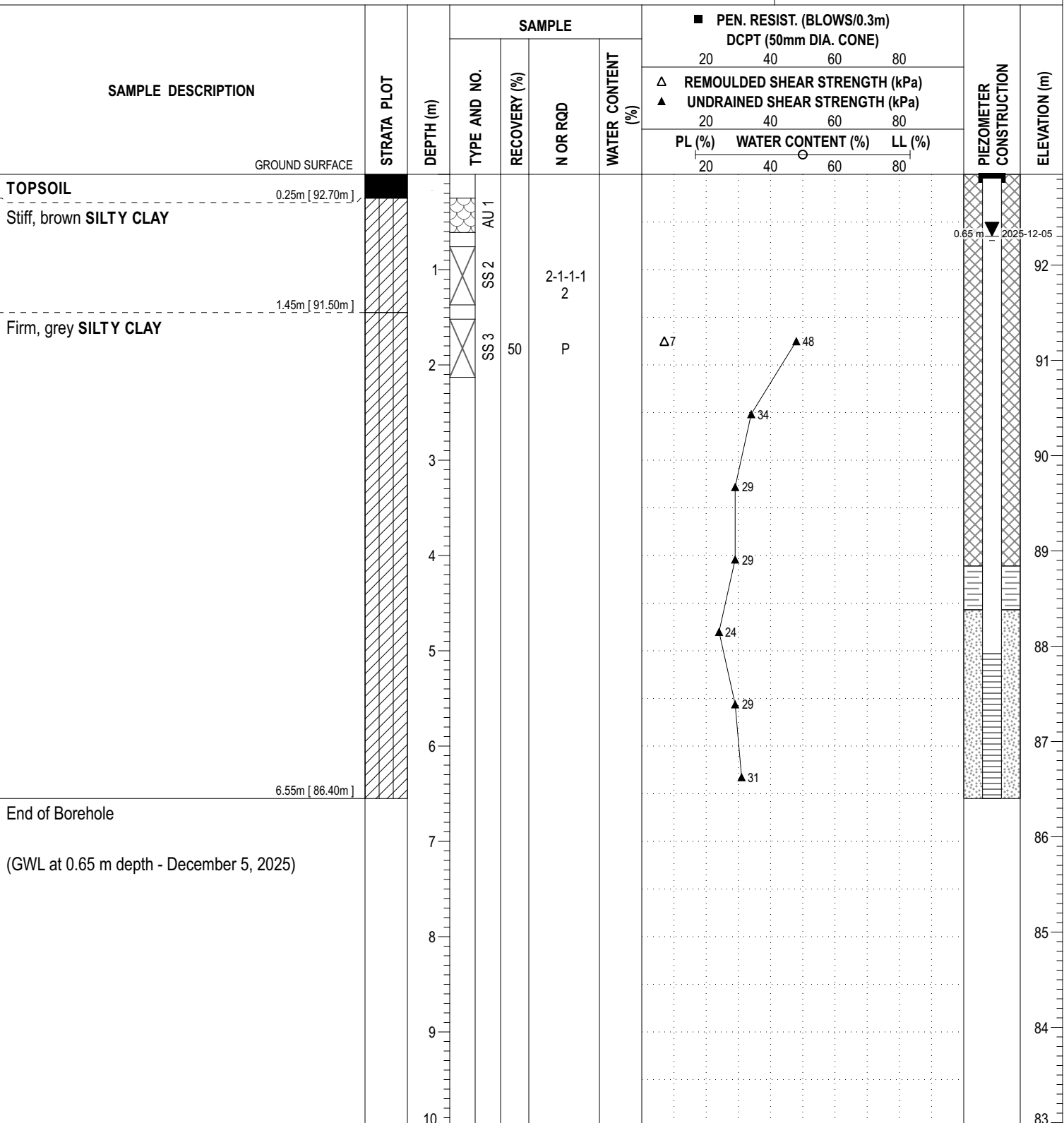
HOLE NO. : BH 8-25

DATE: November 3, 2025



PAGE: 1 / 1

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PROJECT: Proposed Commercial Development			FILE NO. : PG7751
ADVANCED BY: CME-55 Low Clearance Drill			HOLE NO. : BH 9-25
REMARKS:			DATE: November 3, 2025



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ELEVATION: 93.27

FILE NO. : PG7751

REMARKS:

DATE: November 3, 2025

HOLE NO. : BH10-25



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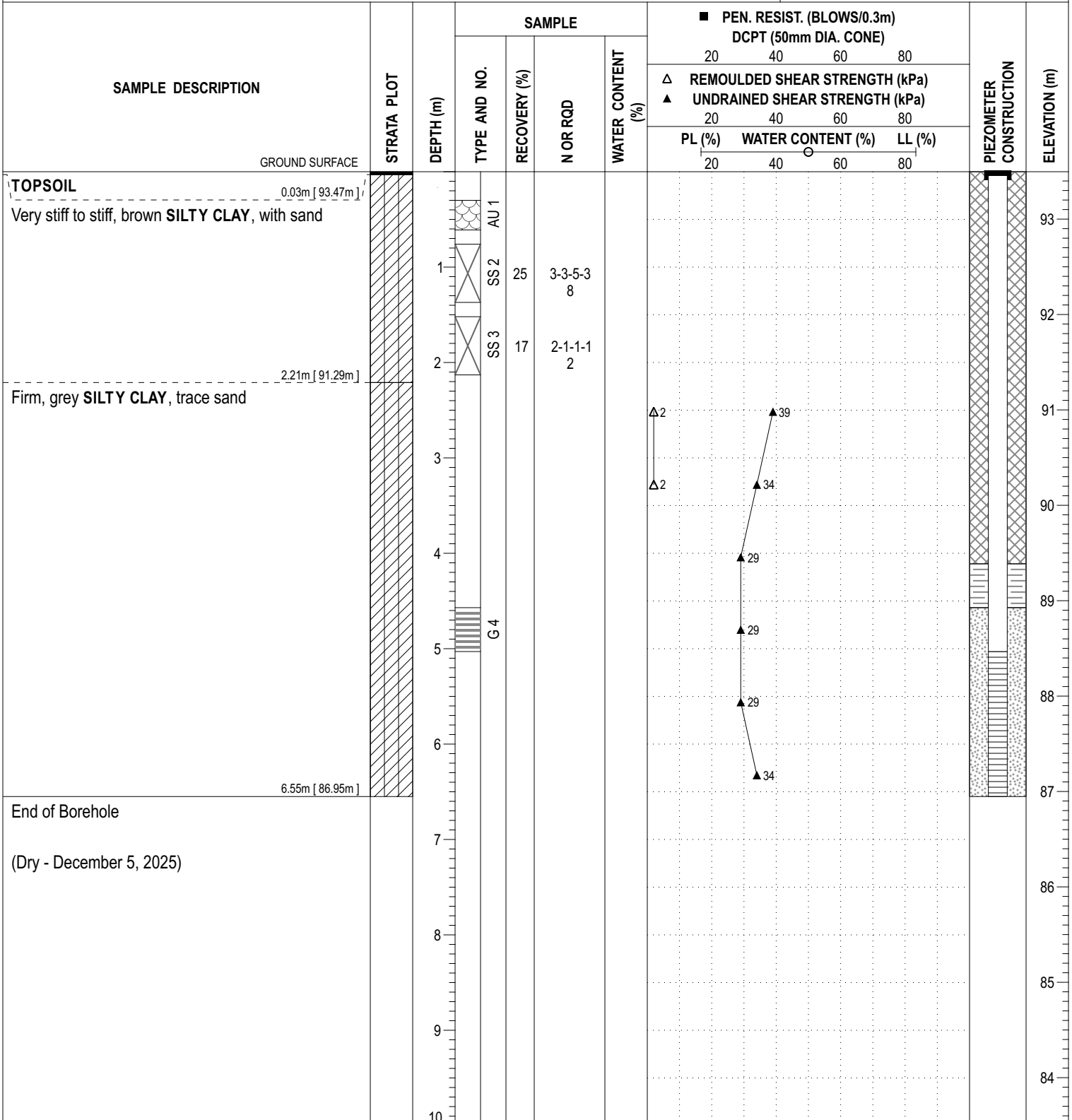
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PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 3, 2025

HOLE NO. : BH11-25


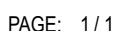
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ELEVATION: 93.62

FILE NO. : PG7751

HOLE NO. : BH12-25

DATE: November 3, 2025



ELEVATION: 93.81

FILE NO. : PG7751

REMARKS:

DATE: November 4, 2025

HOLE NO. : BH13-25



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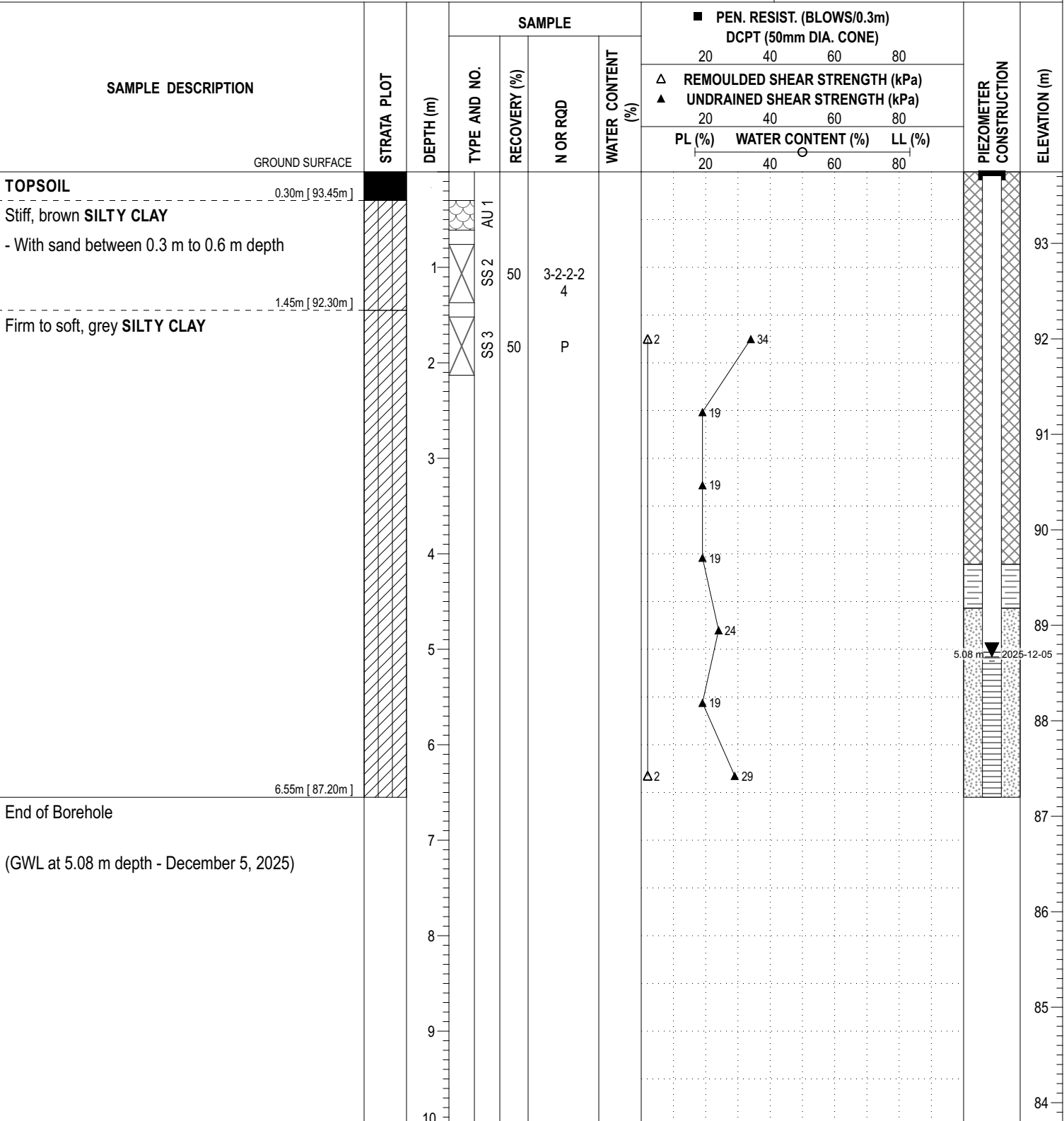
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PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 4, 2025

HOLE NO. : BH14-25


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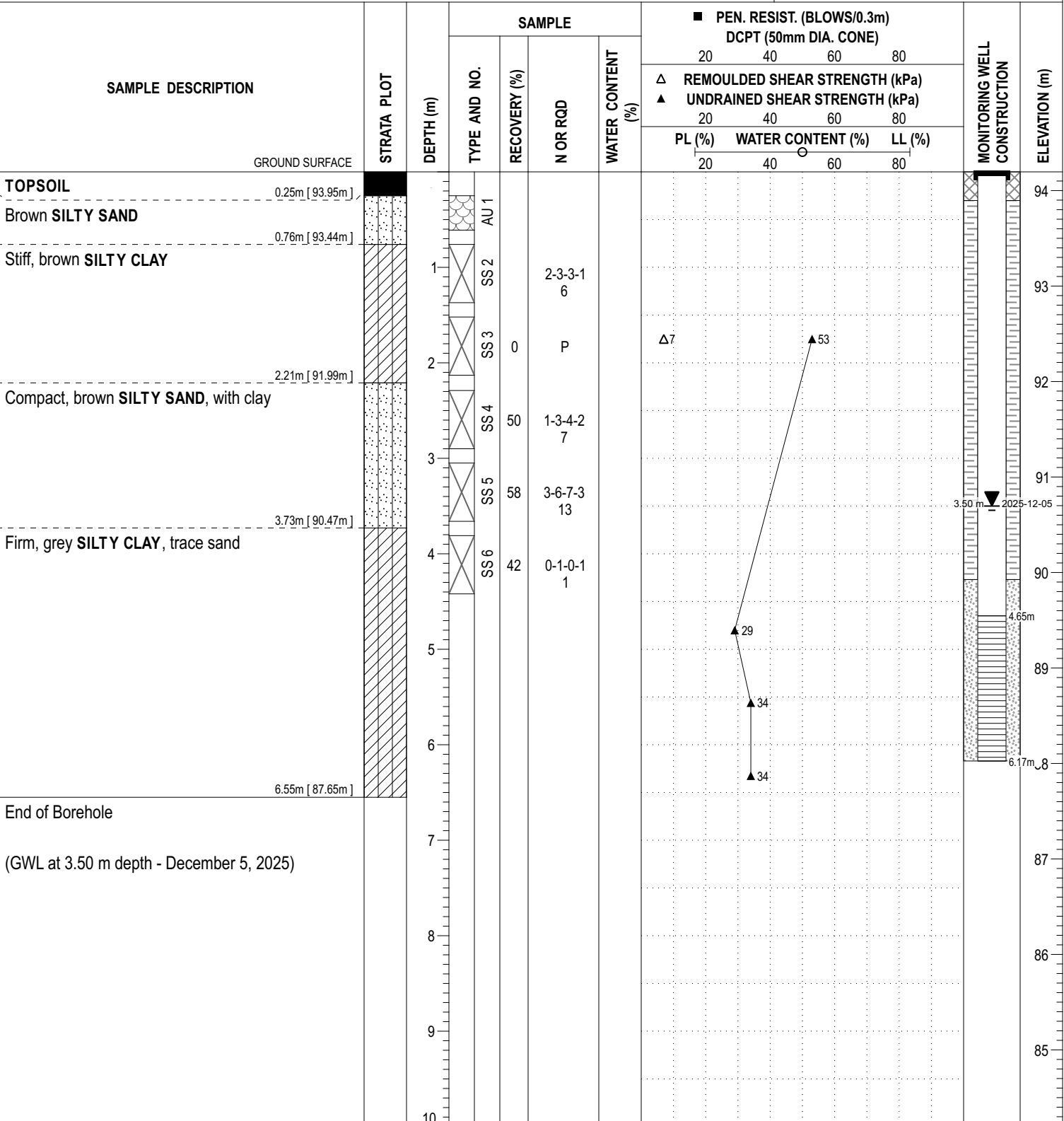
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PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 4, 2025

HOLE NO. : BH15-25


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PROJECT: Proposed Commercial Development

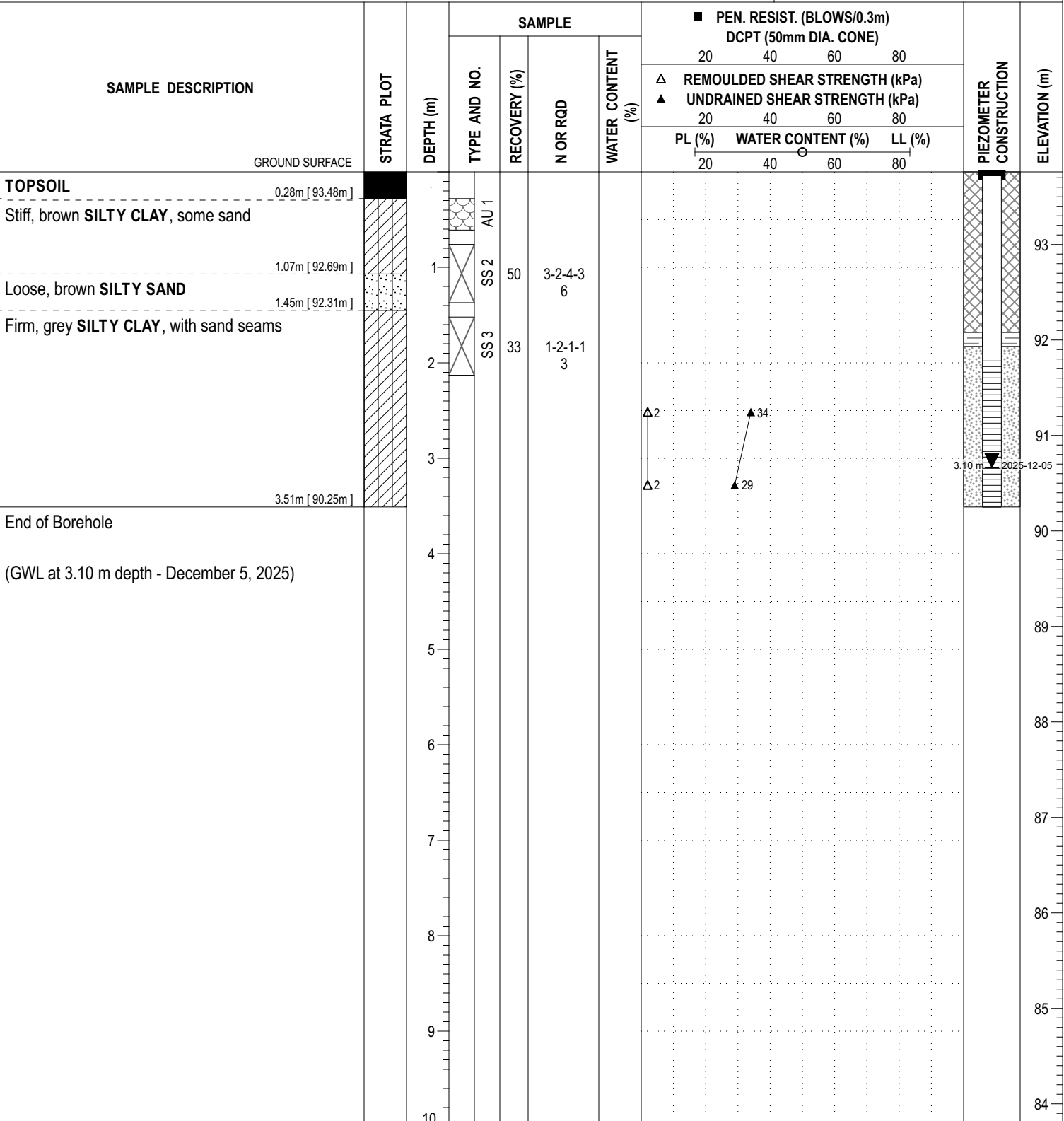
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FILE NO. : PG7751

REMARKS:

DATE: November 4, 2025

HOLE NO. : BH16-25



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HOLE NO. : BH17-25

PAGE: 1 / 1



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NORTHING: 5018779.00

ELEVATION: 93.25

PROJECT: Proposed Commercial Development

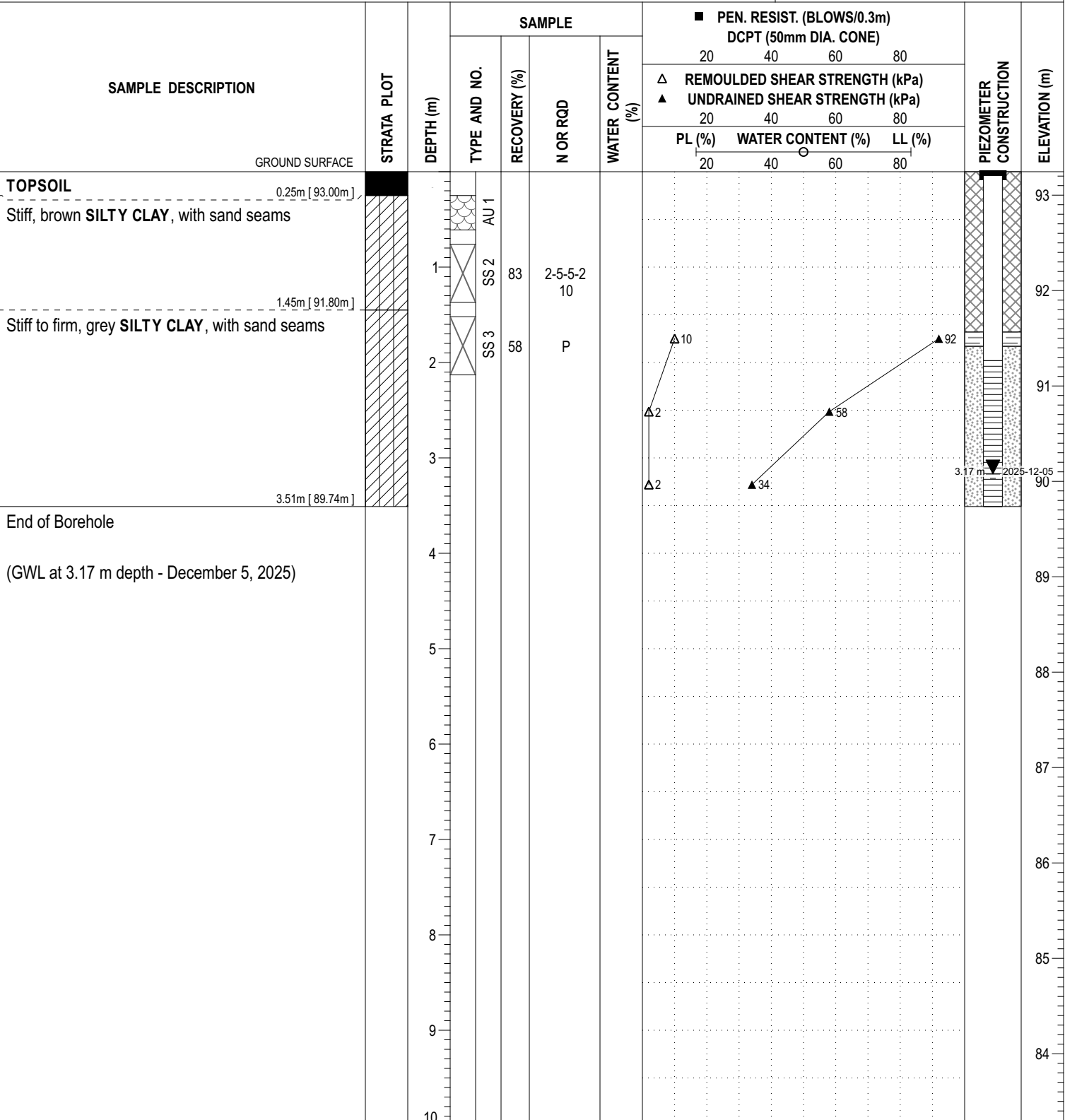
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ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:

DATE: November 4, 2025

HOLE NO. : BH18-25



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ELEVATION: 93.34

FILE NO. : PG7751

REMARKS:

DATE: November 4, 2025

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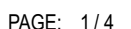


ELEVATION: 94.16

FILE NO. : PG7751

HOLE NO. : BH20-25

DATE: November 5, 2025



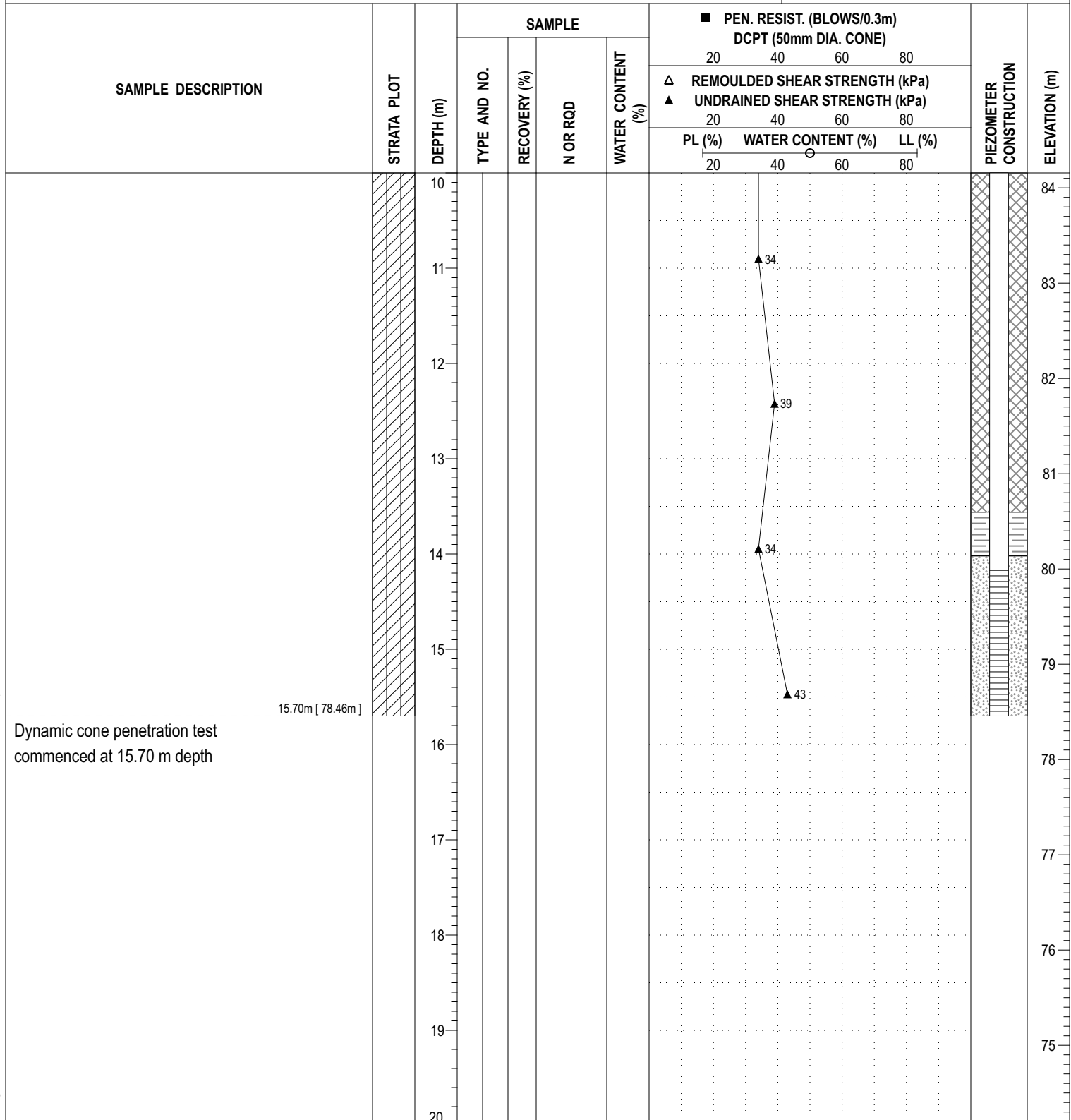
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PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 5, 2025

HOLE NO. : BH20-25


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COORD. SYS.: MTM ZONE 9 **EASTING:** 350165.98 **NORTHING:** 5018707.17 **ELEVATION:** 94.16

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 5, 2025

HOLE NO. : BH20-25

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)				PIEZOMETER CONSTRUCTION	ELEVATION (m)
			TYPE AND NO.	RECOVERY (%)	N OR RQD	WATER CONTENT (%)	20	40	60	80		
							△ REMOULDED SHEAR STRENGTH (kPa)					
							▲ UNDRAINED SHEAR STRENGTH (kPa)					
							20	40	60	80		
PL (%)	WATER CONTENT (%)		LL (%)									
20	40	60	80									
		20										74
		21										73
		22										72
		23										71
		24										70
		25										69
		26										68
		27										67
		28										66
		29										65
		30										

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COORD. SYS.: MTM ZONE 9 **EASTING:** 350165.98 **NORTHING:** 5018707.17 **ELEVATION:** 94.16

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 5, 2025

HOLE NO. : BH20-25

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)				PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N OR RQD	WATER CONTENT (%)	20	40	60	80			
							△ REMOULDED SHEAR STRENGTH (kPa)						
							▲ UNDRAINED SHEAR STRENGTH (kPa)						
							PL (%)	WATER CONTENT (%)		LL (%)			
					20	40	60	80					
End of Borehole DCPT pushed from 15.70 m to 32.00 m depth (GWL at 8.06 m depth - December 5, 2025)		30										64	
		31											63
		32											62
		33											61
		34											60
		35											59
		36											58
		37											57
		38											56
39											55		
40													

DISCLAIMER: THE DATA PRESENTED IN THIS SHEET IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHOM IT WAS PRODUCED. THIS SHEET SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

ELEVATION: 93.33

FILE NO. : PG7751

HOLE NO. : BH21-25

DATE: November 5, 2025



COORD. SYS.: MTM ZONE 9 EASTING: 350168.86 NORTHING: 5018799.43 ELEVATION: 93.33

PROJECT: Proposed Commercial Development

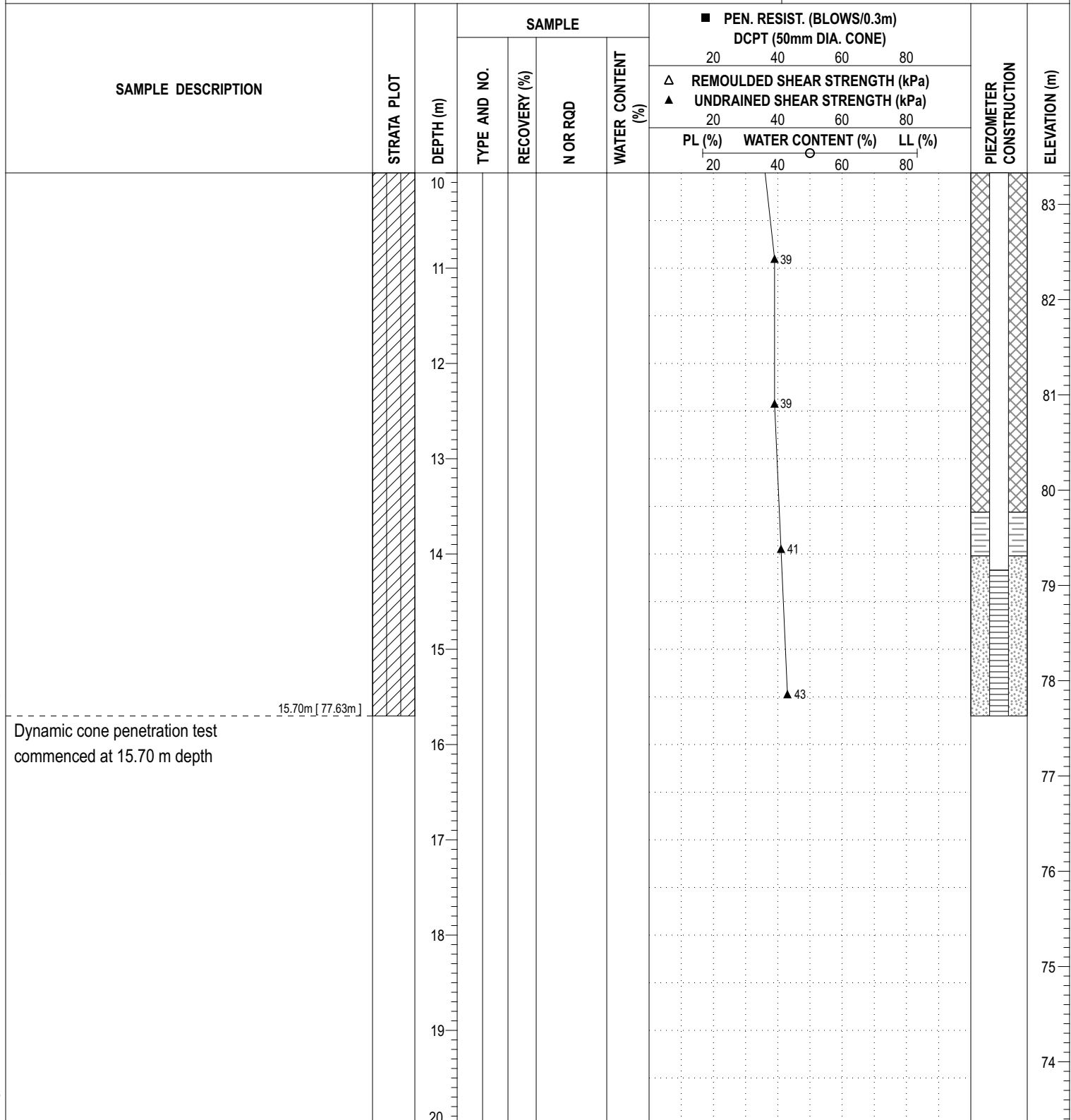
ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:

DATE: November 5, 2025

FILE NO. : PG7751

HOLE NO. : BH21-25



DISCLAIMER: THE DATA PRESENTED IN THIS SHEET IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHOM IT WAS PRODUCED. THIS SHEET SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

COORD. SYS.: MTM ZONE 9 **EASTING:** 350168.86 **NORTHING:** 5018799.43 **ELEVATION:** 93.33

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 5, 2025

HOLE NO. : BH21-25

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)				PIEZOMETER CONSTRUCTION	ELEVATION (m)
			TYPE AND NO.	RECOVERY (%)	N OR RQD	WATER CONTENT (%)	20	40	60	80		
							△ REMOULDED SHEAR STRENGTH (kPa)					
							▲ UNDRAINED SHEAR STRENGTH (kPa)					
							PL (%)	WATER CONTENT (%)		LL (%)		
		20										73
		21										72
		22										71
		23										70
		24										69
		25										68
		26										67
		27										66
		28										65
29										64		
30												

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COORD. SYS.: MTM ZONE 9	EASTING: 350168.86	NORTHING: 5018799.43	ELEVATION: 93.33
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PROJECT: Proposed Commercial Development	FILE NO. : PG7751
ADVANCED BY: CME-55 Low Clearance Drill	
REMARKS:	HOLE NO. : BH21-25
DATE: November 5, 2025	

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)				PIEZOMETER CONSTRUCTION	ELEVATION (m)
			TYPE AND NO.	RECOVERY (%)	N OR RQD	WATER CONTENT (%)	20	40	60	80		
							△ REMOULDED SHEAR STRENGTH (kPa)					
							▲ UNDRAINED SHEAR STRENGTH (kPa)					
							20	40	60	80		
PL (%)		WATER CONTENT (%)		LL (%)								
20		40		60		80						
		30										63
		31										62
		32										61
		33										60
		34										59
		35										58
		36									57	
		37									56	
		38									55	
38.71m [54.62m]												
End of Borehole		39									54	
DCPT pushed from 15.70 m to 38.71 m depth												
(GWL at 2.50 m depth - December 5, 2025)		40										

38.71m [54.62m]

End of Borehole
DCPT pushed from 15.70 m to 38.71 m depth
(GWL at 2.50 m depth - December 5, 2025)

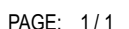
DISCLAIMER: THE DATA PRESENTED IN THIS SHEET IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHOM IT WAS PRODUCED. THIS SHEET SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

ELEVATION: 93.38

FILE NO. : PG7751

HOLE NO. : BH22-25

DATE: November 6, 2025

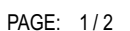


ELEVATION: 93.30

FILE NO. : PG7751

HOLE NO. : BH23-25

DATE: November 6, 2025



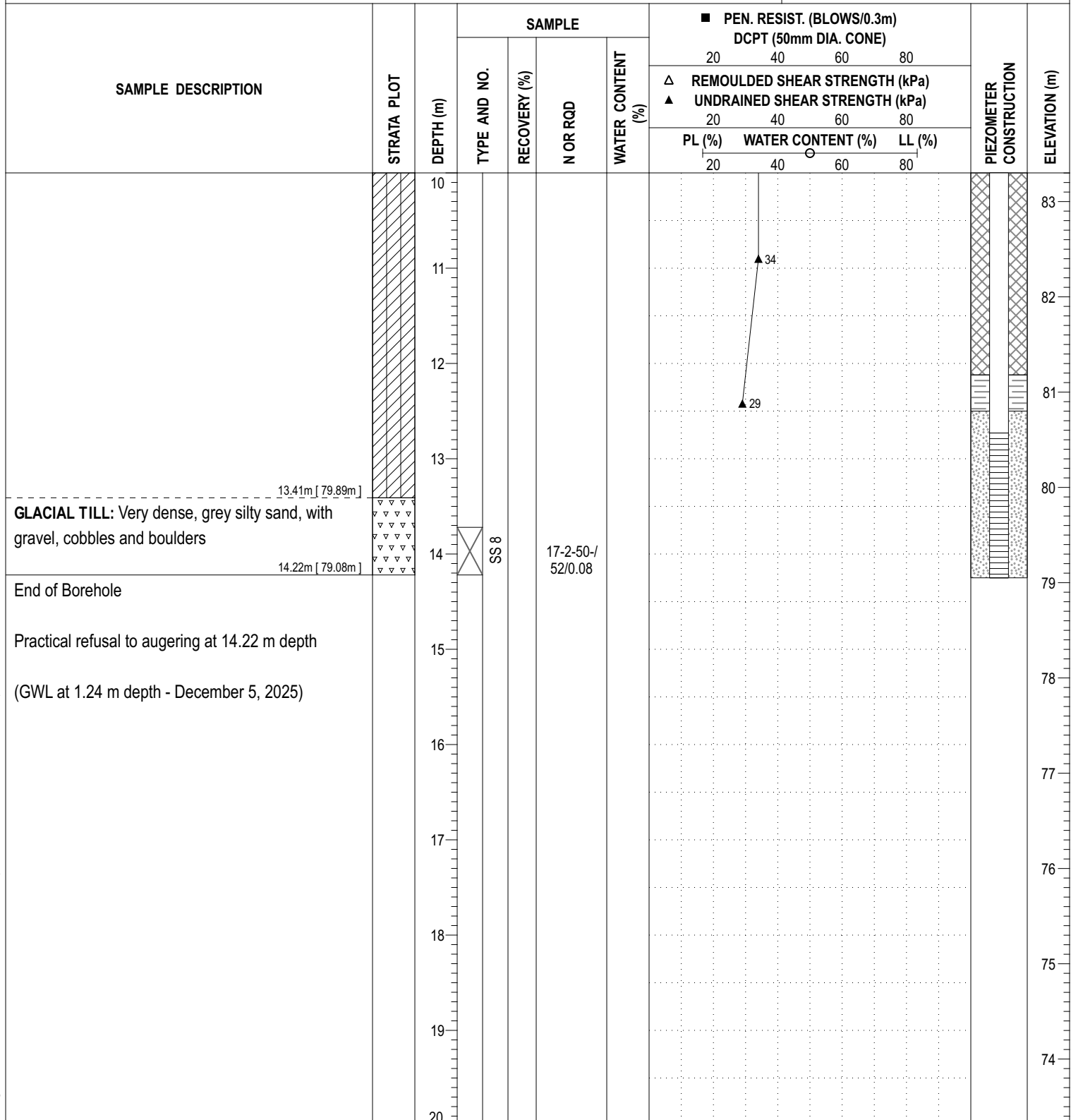
COORD. SYS.: MTM ZONE 9 **EASTING:** 349916.34 **NORTHING:** 5018815.58 **ELEVATION:** 93.30

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 6, 2025

HOLE NO. : BH23-25


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COORD. SYS.: MTM ZONE 9 **EASTING:** 349899.82 **NORTHING:** 5018779.07 **ELEVATION:** 93.75

PROJECT: Proposed Commercial Development

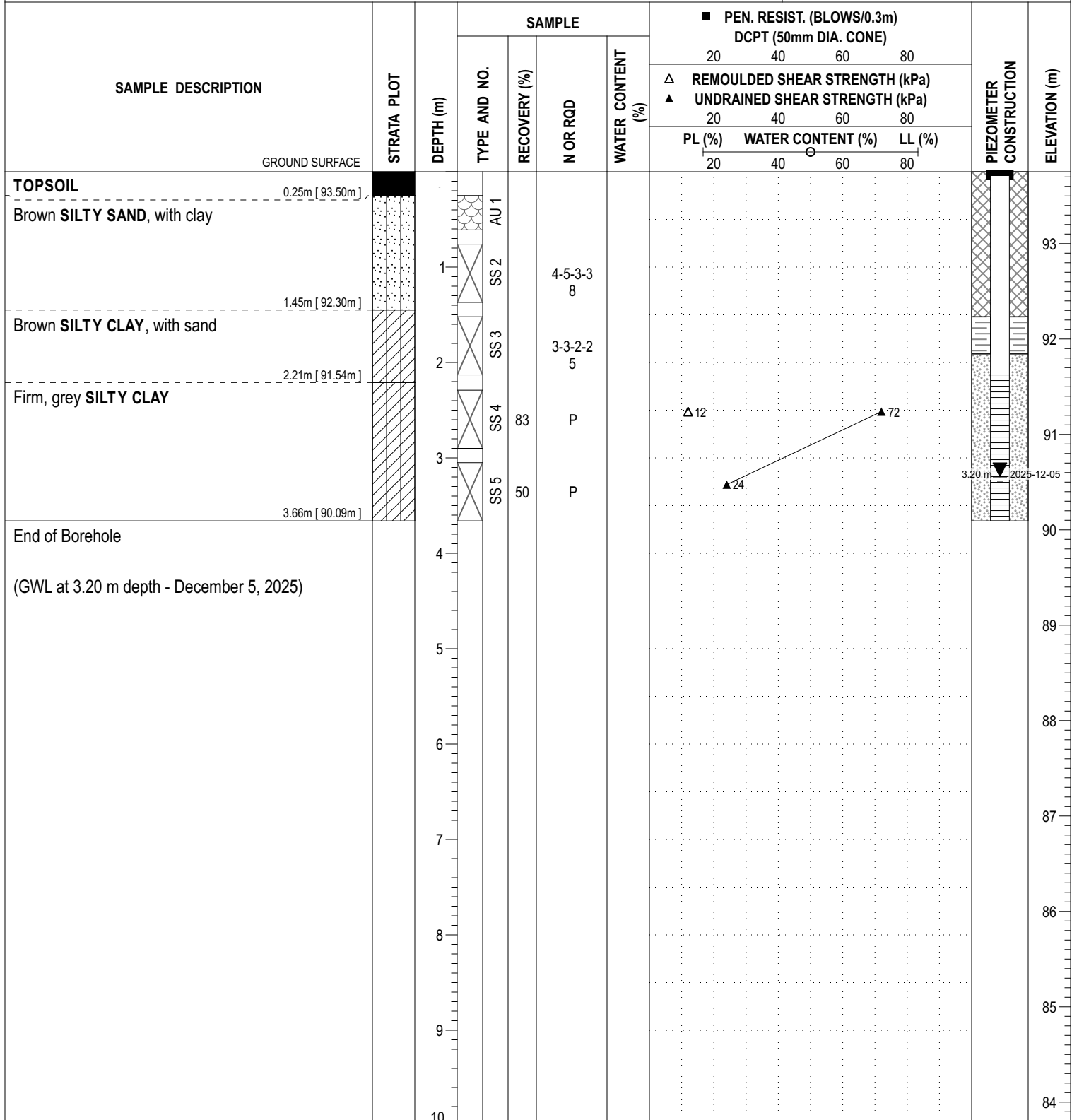
ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:

DATE: November 6, 2025

FILE NO. : PG7751

HOLE NO. : BH24-25



DISCLAIMER: THE DATA PRESENTED IN THIS SHEET IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHOM IT WAS PRODUCED. THIS SHEET SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

COORD. SYS.: MTM ZONE 9

EASTING: 350064.62

NORTHING: 5018747.86

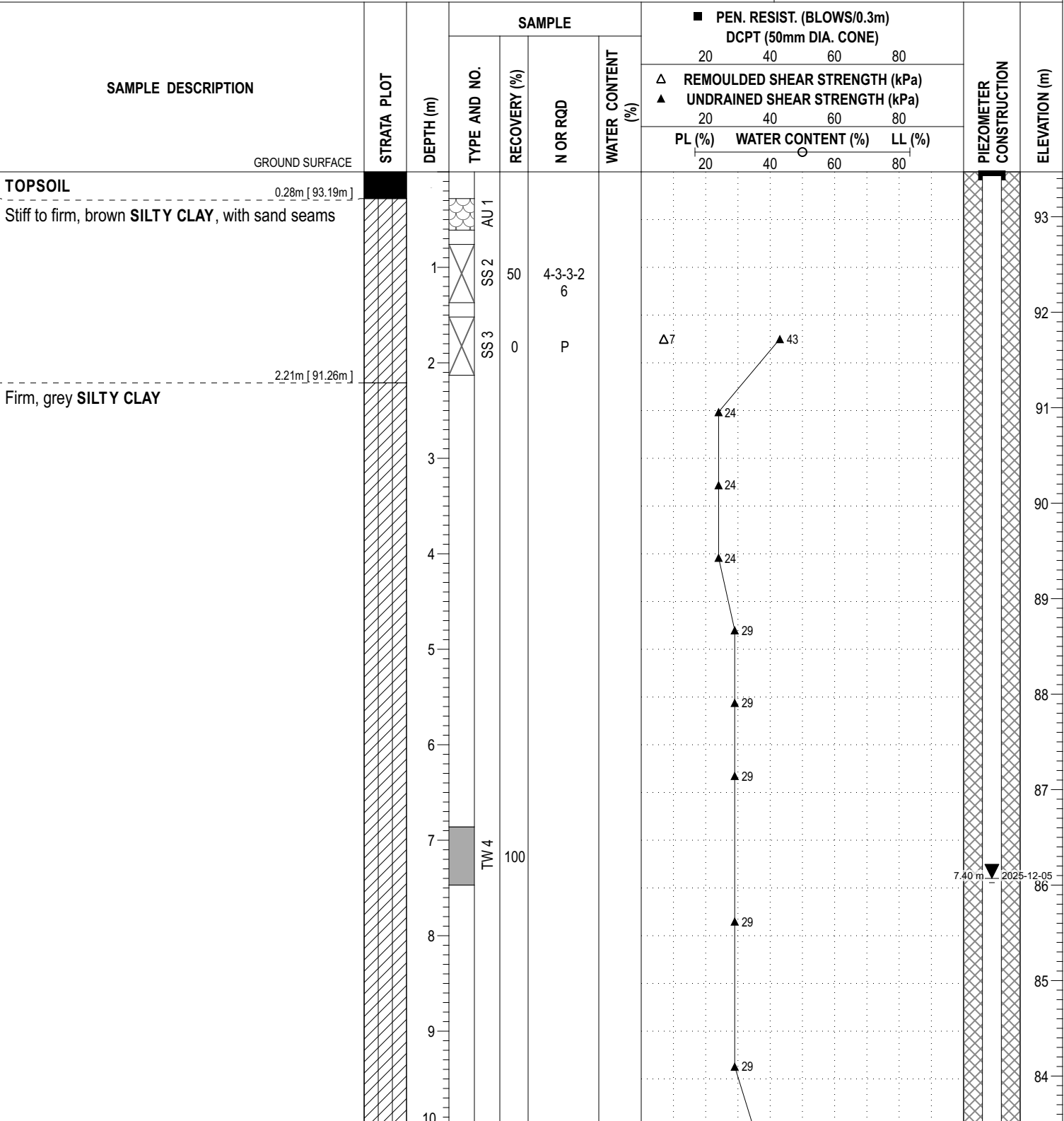
ELEVATION: 93.47

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 7, 2025

HOLE NO. : BH25-25


DISCLAIMER: THE DATA PRESENTED IN THIS SHEET IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHOM IT WAS PRODUCED. THIS SHEET SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

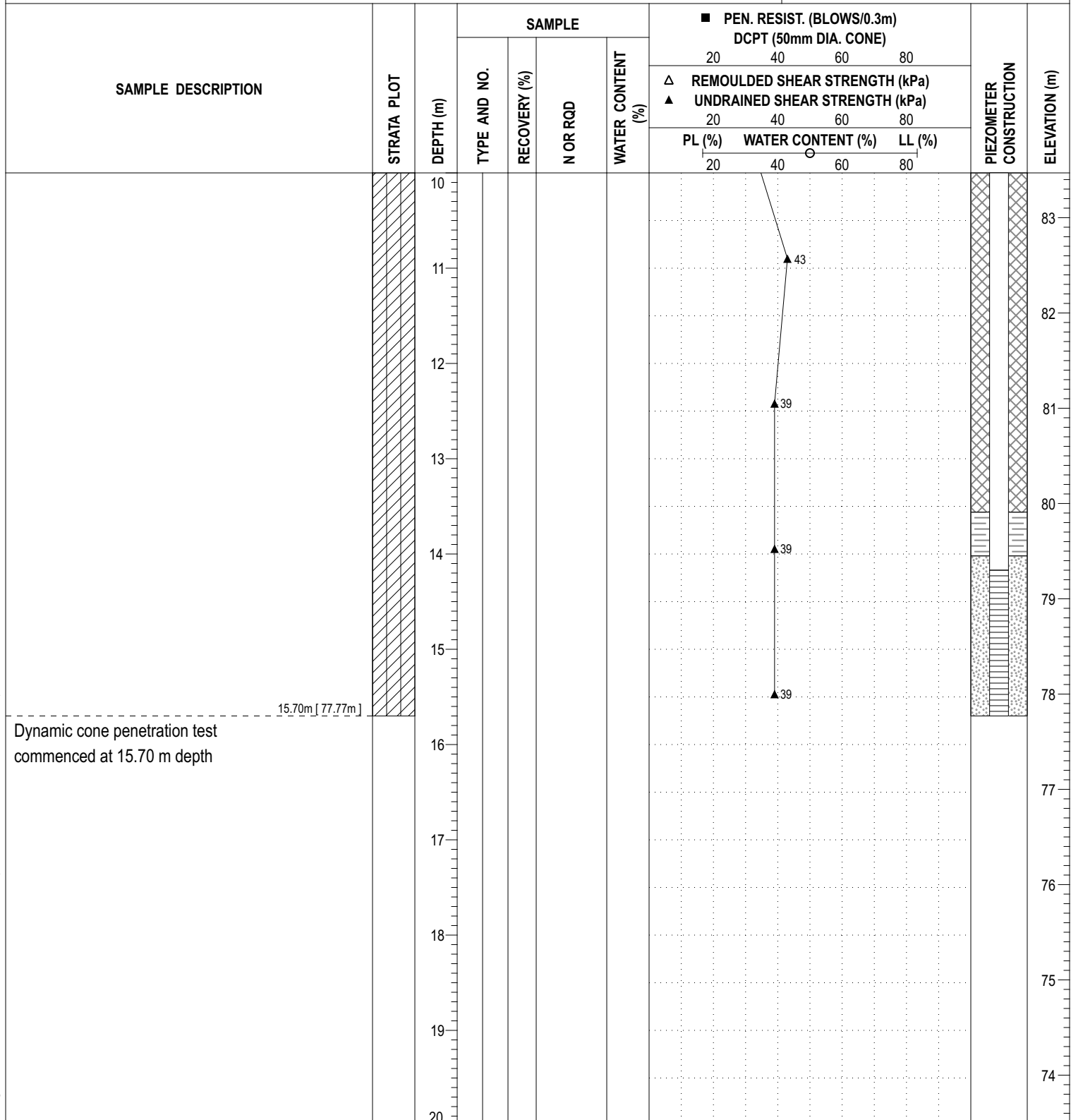
COORD. SYS.: MTM ZONE 9 **EASTING:** 350064.62 **NORTHING:** 5018747.86 **ELEVATION:** 93.47

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 7, 2025

HOLE NO. : BH25-25


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ELEVATION: 93.47

FILE NO. : PG7751

HOLE NO. : **BH25-25**

DATE: November 7, 2025

(GWL at 7.40 m depth - December 5, 2025)

PAGE: 3 / 3



COORD. SYS.: MTM ZONE 9

EASTING: 350003.84

NORTHING: 5018710.01

ELEVATION: 93.64

PROJECT: Proposed Commercial Development

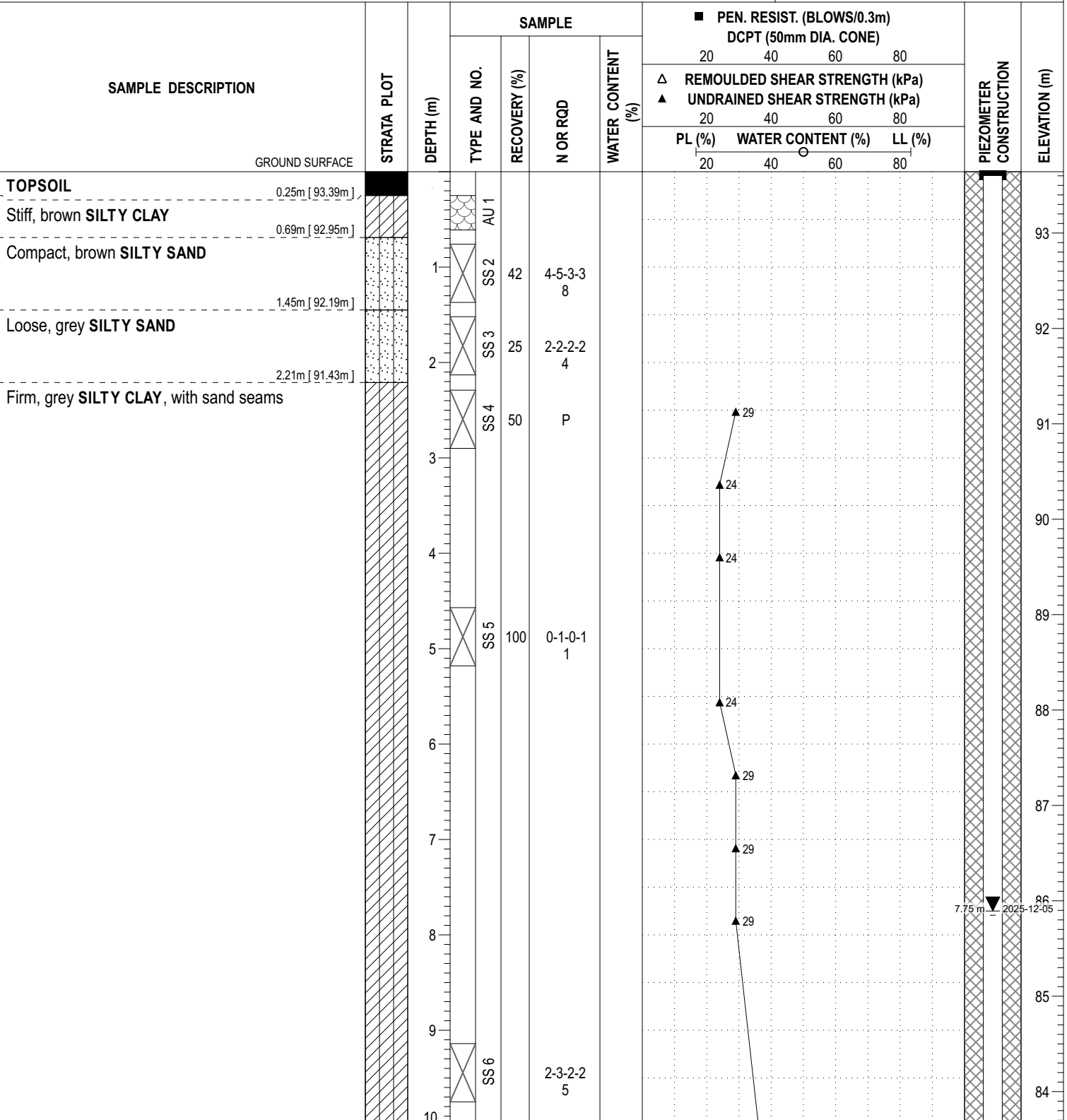
ADVANCED BY: CME-55 Low Clearance Drill

FILE NO. : PG7751

REMARKS:

DATE: November 7, 2025

HOLE NO. : BH26-25



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COORD. SYS.: MTM ZONE 9 **EASTING:** 350003.84 **NORTHING:** 5018710.01 **ELEVATION:** 93.64

PROJECT: Proposed Commercial Development

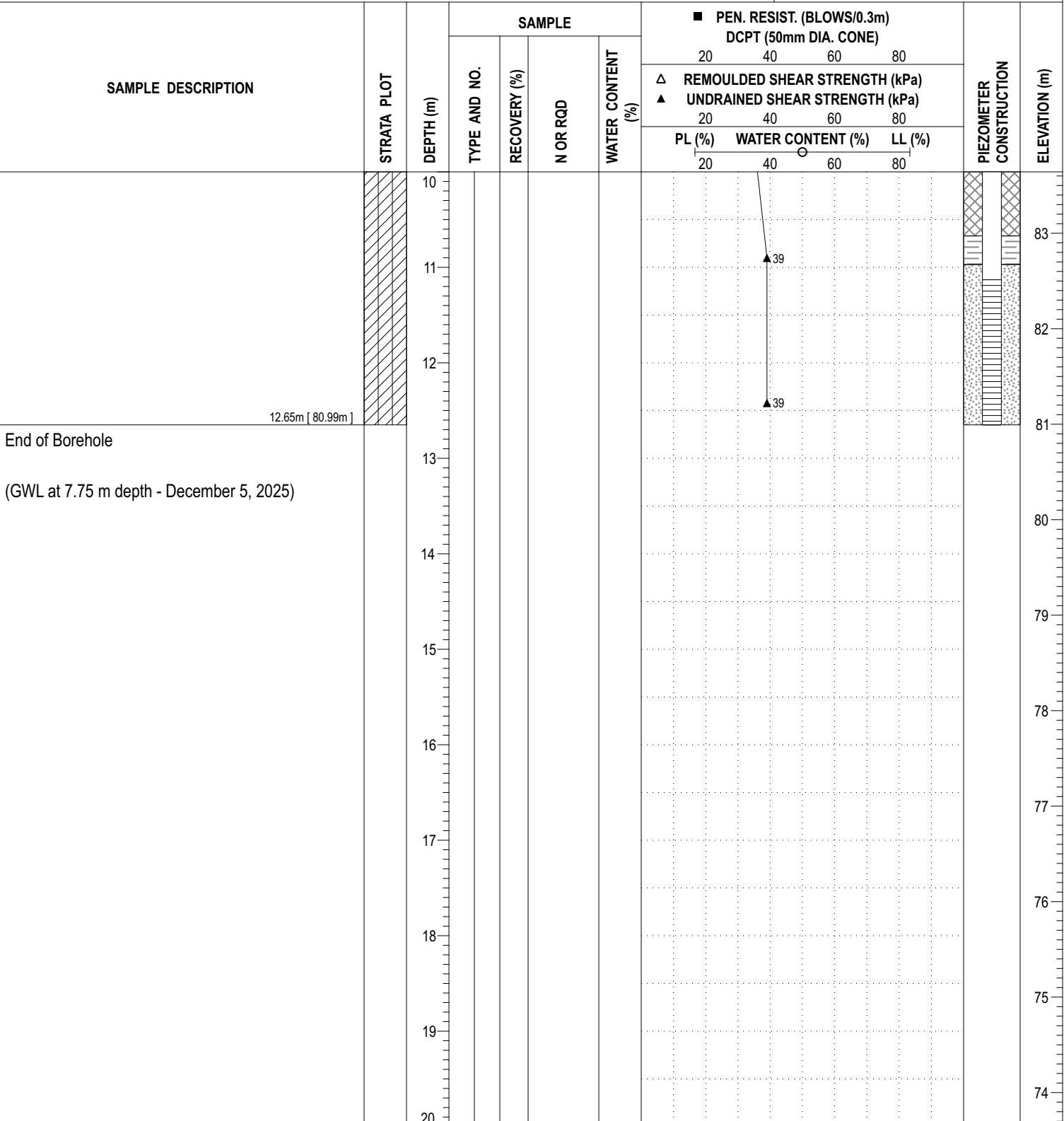
ADVANCED BY: CME-55 Low Clearance Drill

FILE NO. : PG7751

REMARKS:

DATE: November 7, 2025

HOLE NO. : BH26-25



DISCLAIMER: THE DATA PRESENTED IN THIS SHEET IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHOM IT WAS PRODUCED. THIS SHEET SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

COORD. SYS.: MTM ZONE 9 **EASTING:** 349943.30 **NORTHING:** 5018674.83 **ELEVATION:** 93.63

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 7, 2025

HOLE NO. : BH27-25

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)				PIEZOMETER CONSTRUCTION	ELEVATION (m)
			TYPE AND NO.	RECOVERY (%)	N OR RQD	WATER CONTENT (%)	20	40	60	80		
							△ REMOULDED SHEAR STRENGTH (kPa)					
							▲ UNDRAINED SHEAR STRENGTH (kPa)					
						PL (%)	WATER CONTENT (%)	LL (%)				
							20	40	60	80		
GROUND SURFACE												
TOPSOIL												
Stiff, brown SILTY CLAY, with organics			AU 1								93	
0.69m [92.94m]												
Compact, brown SILTY SAND		1	SS 2	50	3-6-5-3 11							
1.45m [92.18m]												
Loose, grey SILTY SAND, with clay		2	SS 3	75	2-2-2-1 4						92	
2.13m [91.50m]												
Firm, grey SILTY CLAY, with sand seams		3	SS 4		1-2-0-1 2						91	
3.66m [89.97m]												
End of Borehole			SS 5	42	P						90	
		4										
		5									89	
		6									88	
		7									87	
		8									86	
		9									85	
		10									84	

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COORD. SYS.: MTM ZONE 9

EASTING: 350209.04

NORTHING: 5018802.05

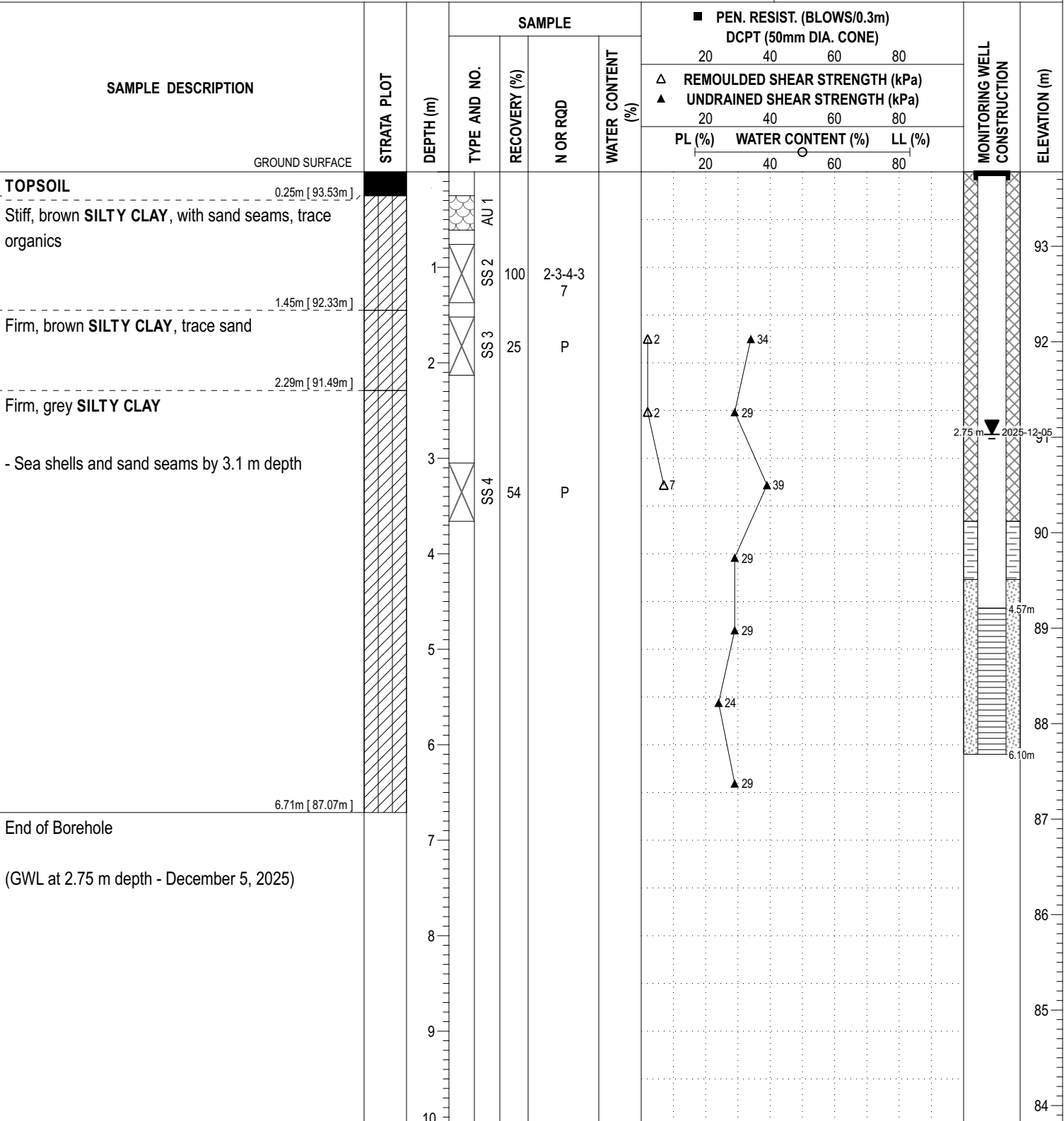
ELEVATION: 93.78

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 13, 2025

HOLE NO. : BH28-25


DISCLAIMER: THE DATA PRESENTED IN THIS SHEET IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHOM IT WAS PRODUCED. THIS SHEET SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

ELEVATION: 93.02

FILE NO. : PG7751

HOLE NO. : BH29-25

DATE: November 13, 2025



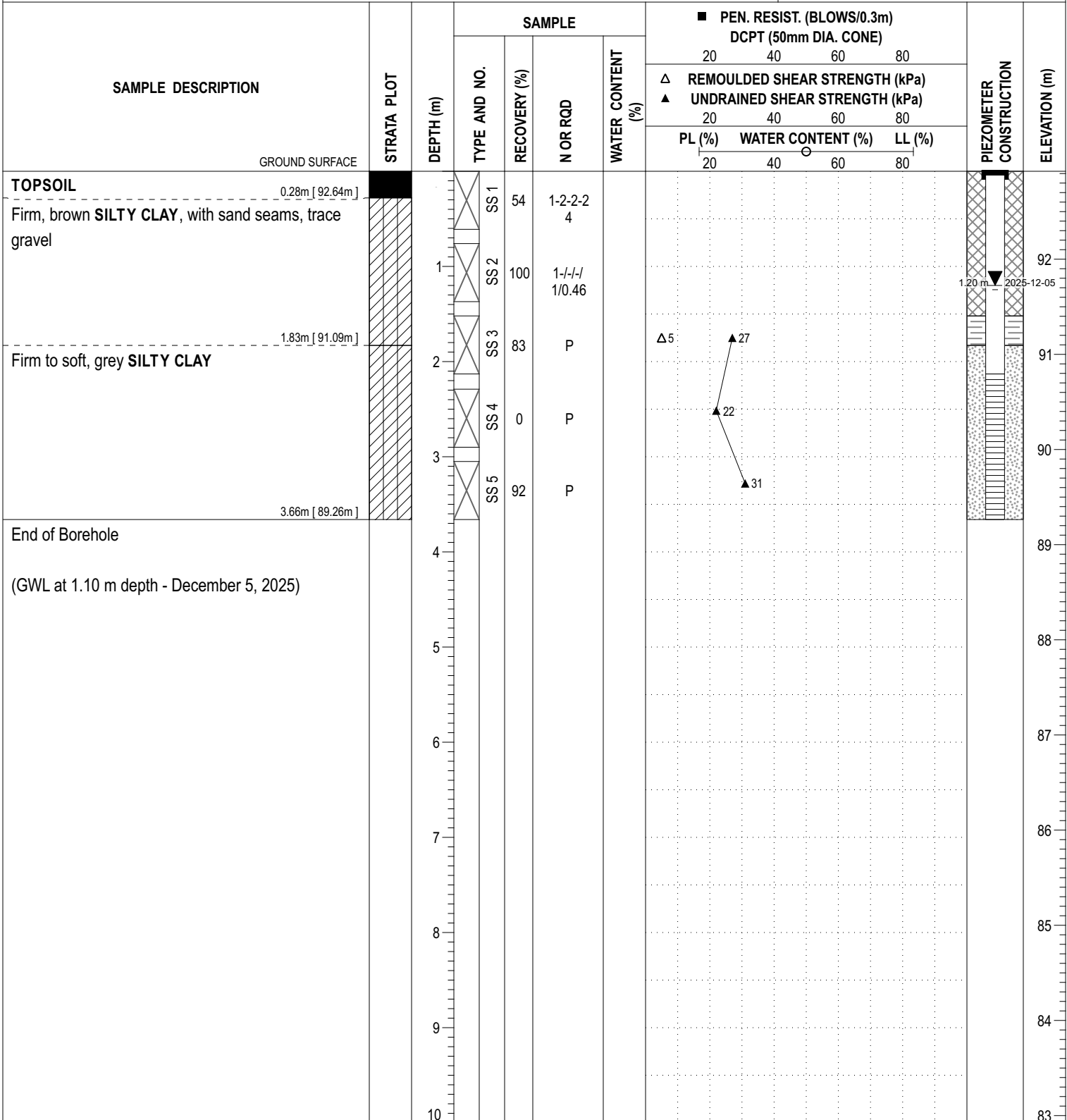
COORD. SYS.: MTM ZONE 9 **EASTING:** 350066.32 **NORTHING:** 5018832.97 **ELEVATION:** 92.92

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 13, 2025

HOLE NO. : BH30-25


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COORD. SYS.: MTM ZONE 9 **EASTING:** 350004.21 **NORTHING:** 5018747.33 **ELEVATION:** 93.58

PROJECT: Proposed Commercial Development

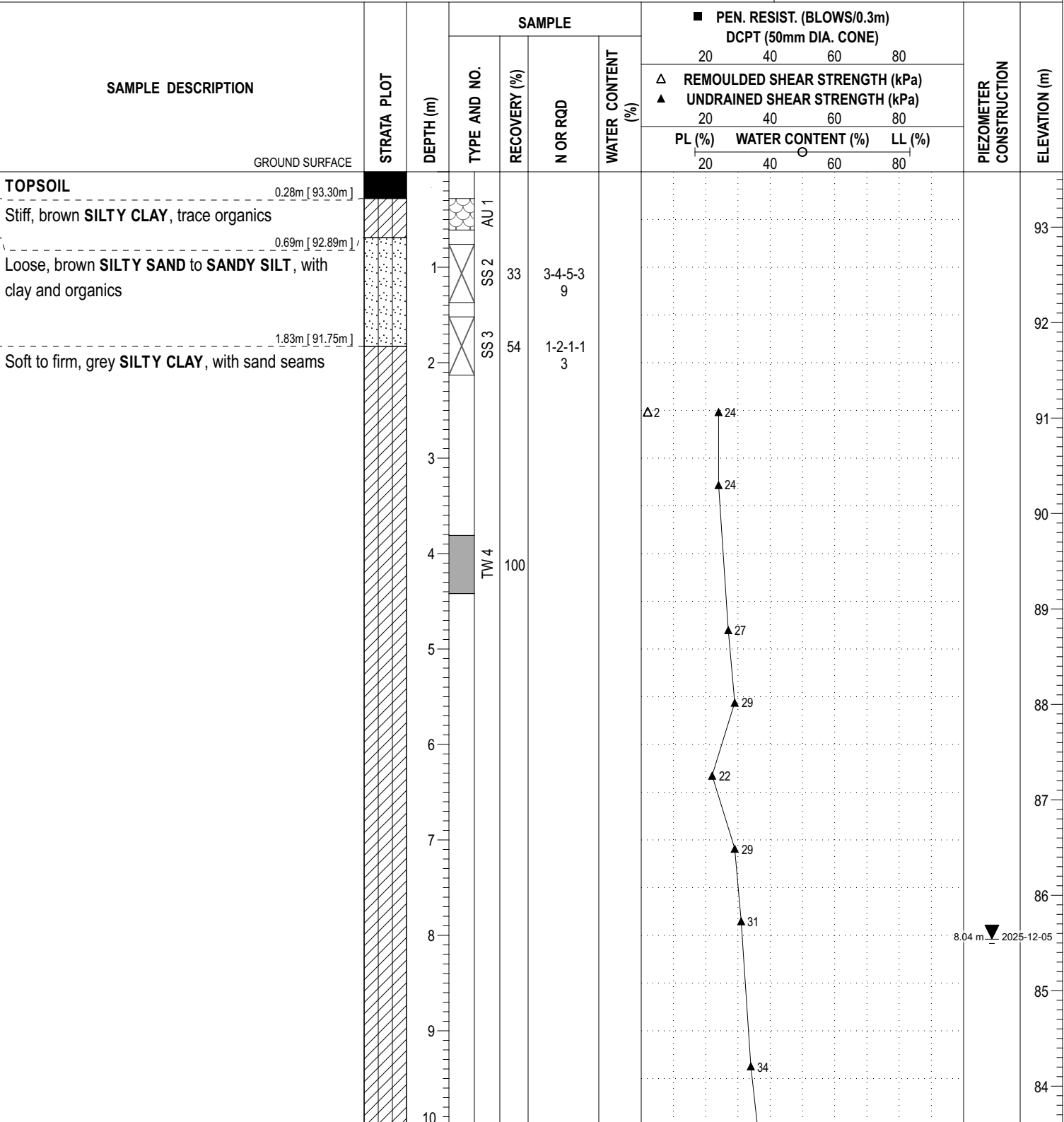
ADVANCED BY: CME-55 Low Clearance Drill

FILE NO. : PG7751

REMARKS:

DATE: November 13, 2025

HOLE NO. : BH31-25



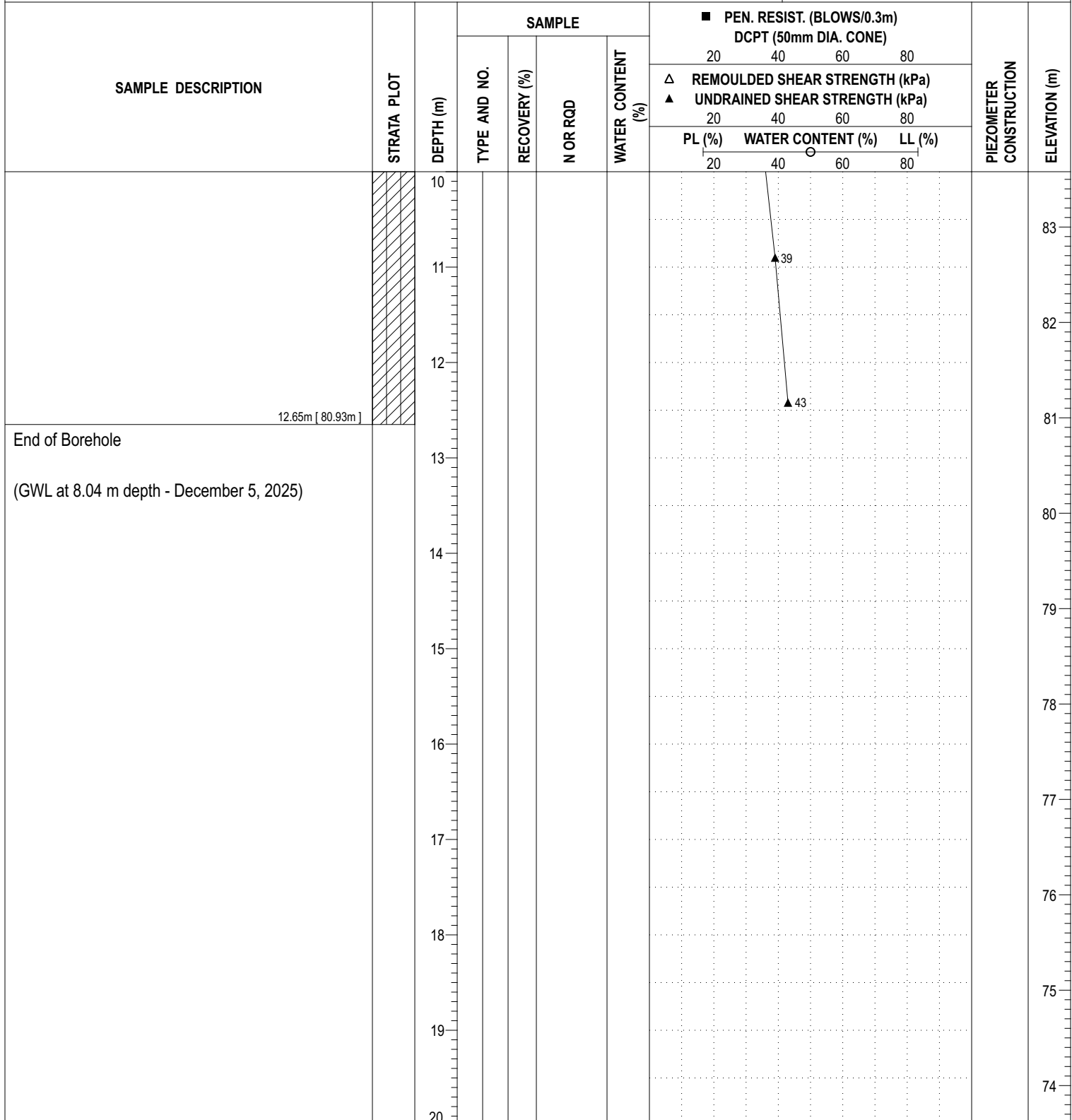
DISCLAIMER: THE DATA PRESENTED IN THIS SHEET IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHOM IT WAS PRODUCED. THIS SHEET SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

COORD. SYS.: MTM ZONE 9	EASTING: 350004.21	NORTHING: 5018747.33	ELEVATION: 93.58
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PROJECT: Proposed Commercial Development	FILE NO. : PG7751
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ADVANCED BY: CME-55 Low Clearance Drill	HOLE NO. : BH31-25
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REMARKS:	DATE: November 13, 2025
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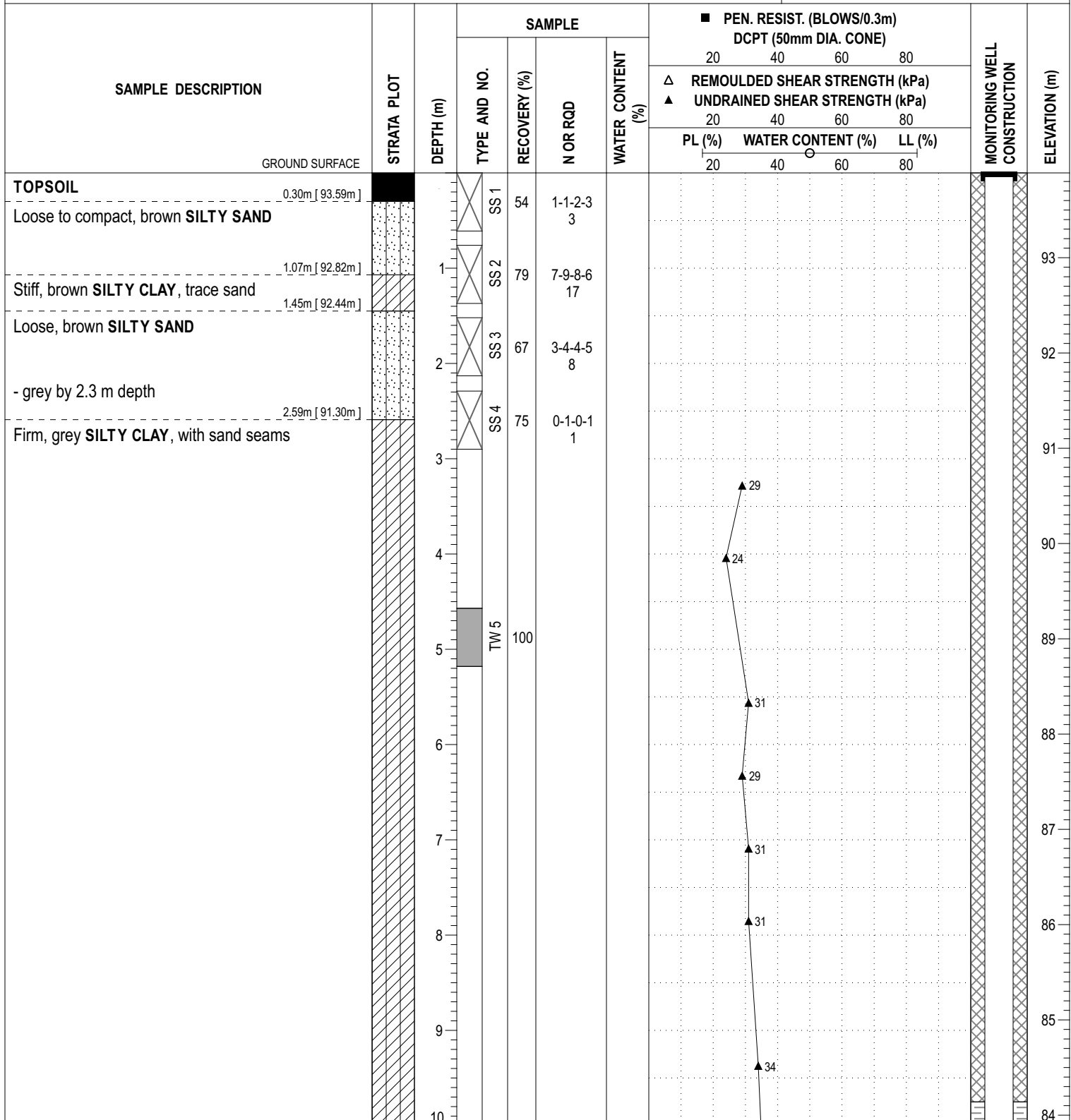
COORD. SYS.: MTM ZONE 9 **EASTING:** 349914.93 **NORTHING:** 5018695.14 **ELEVATION:** 93.89

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 14, 2025

HOLE NO. : BH32-25


DISCLAIMER: THE DATA PRESENTED IN THIS SHEET IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHOM IT WAS PRODUCED. THIS SHEET SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

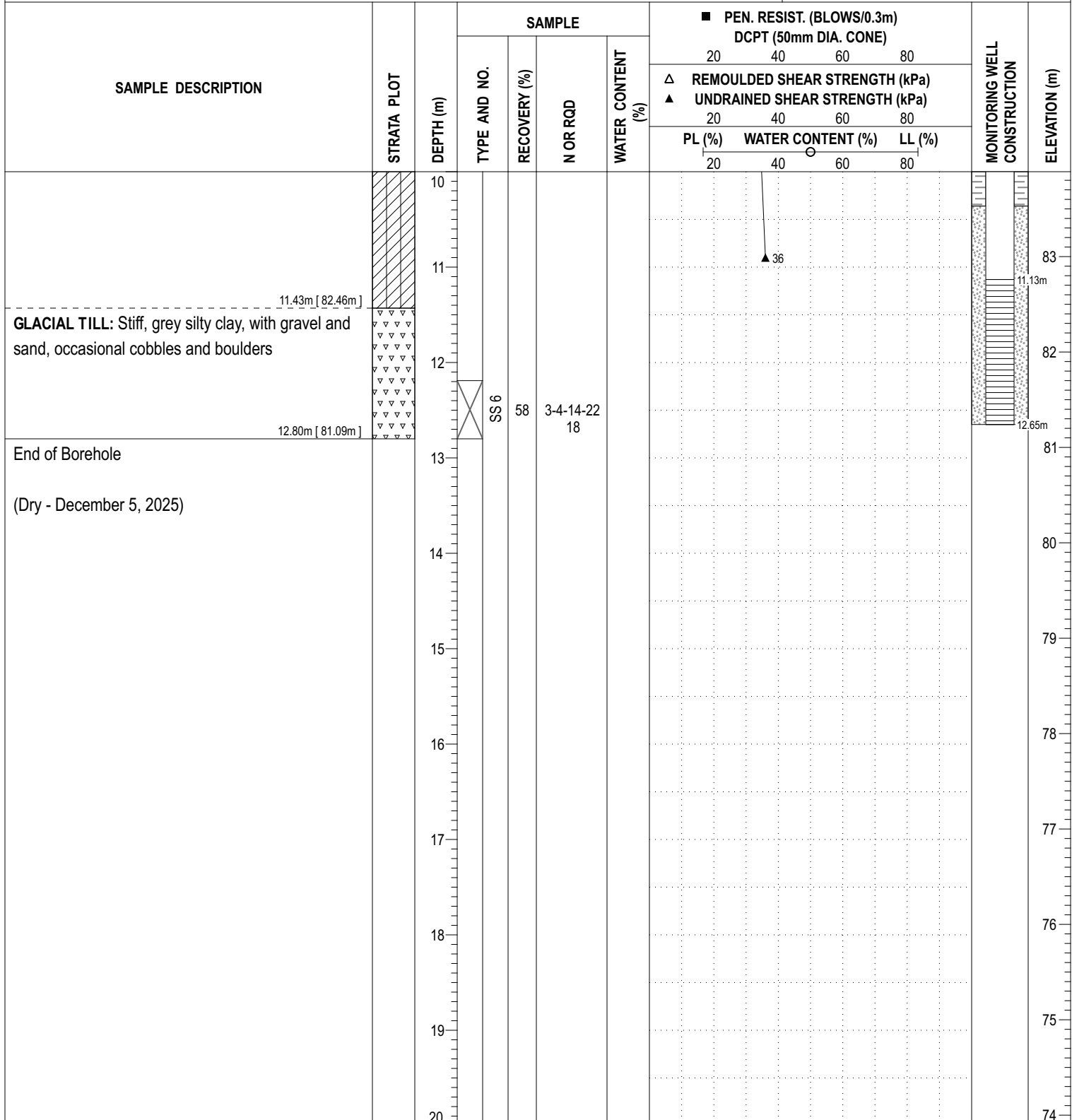
COORD. SYS.: MTM ZONE 9 **EASTING:** 349914.93 **NORTHING:** 5018695.14 **ELEVATION:** 93.89

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 14, 2025

HOLE NO. : BH32-25


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COORD. SYS.: MTM ZONE 9 **EASTING:** 350014.26 **NORTHING:** 5018644.26 **ELEVATION:** 93.54

PROJECT: Proposed Commercial Development

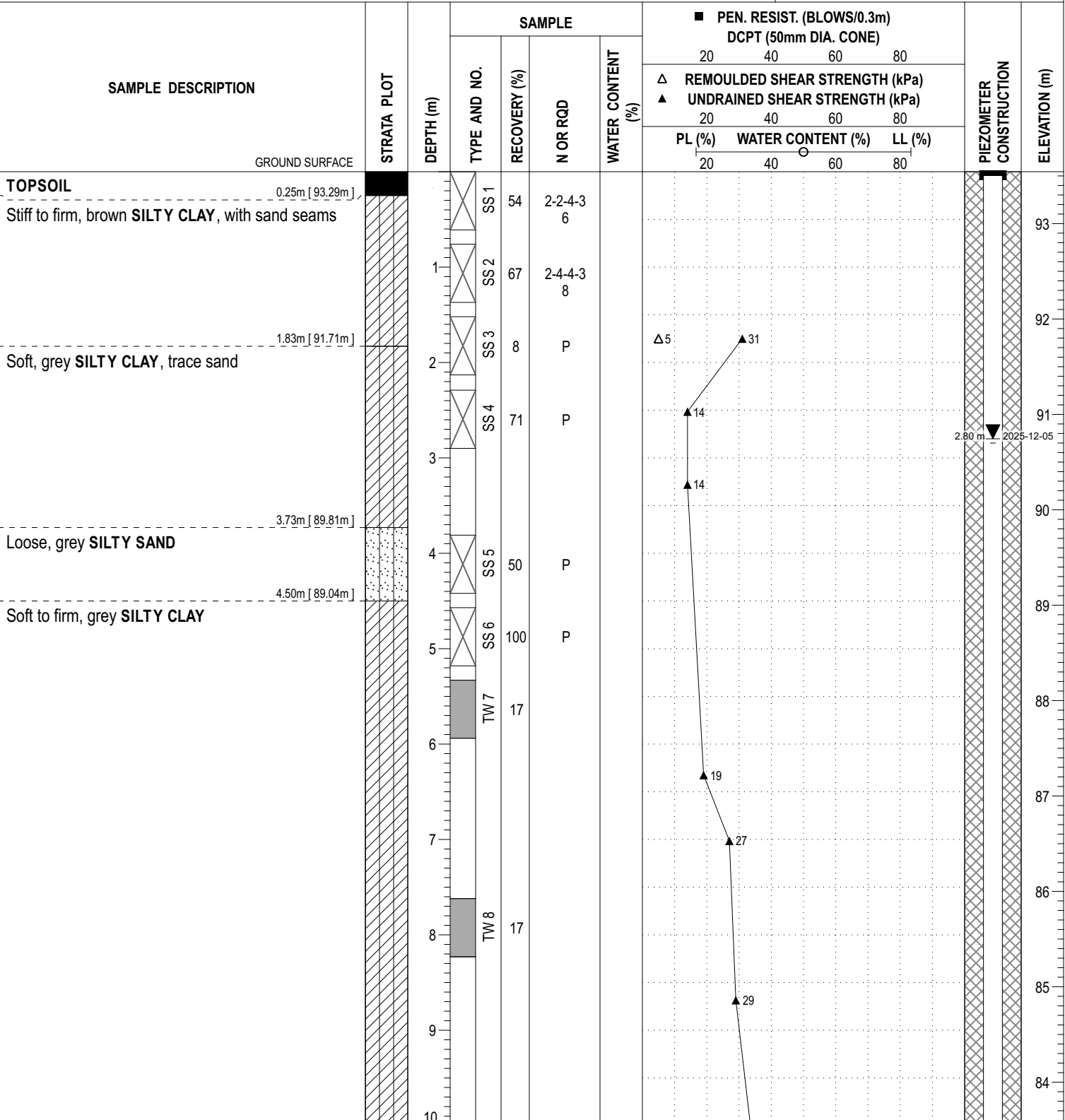
FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:

DATE: November 17, 2025

HOLE NO. : BH33-25



DISCLAIMER: THE DATA PRESENTED IN THIS SHEET IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHOM IT WAS PRODUCED. THIS SHEET SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

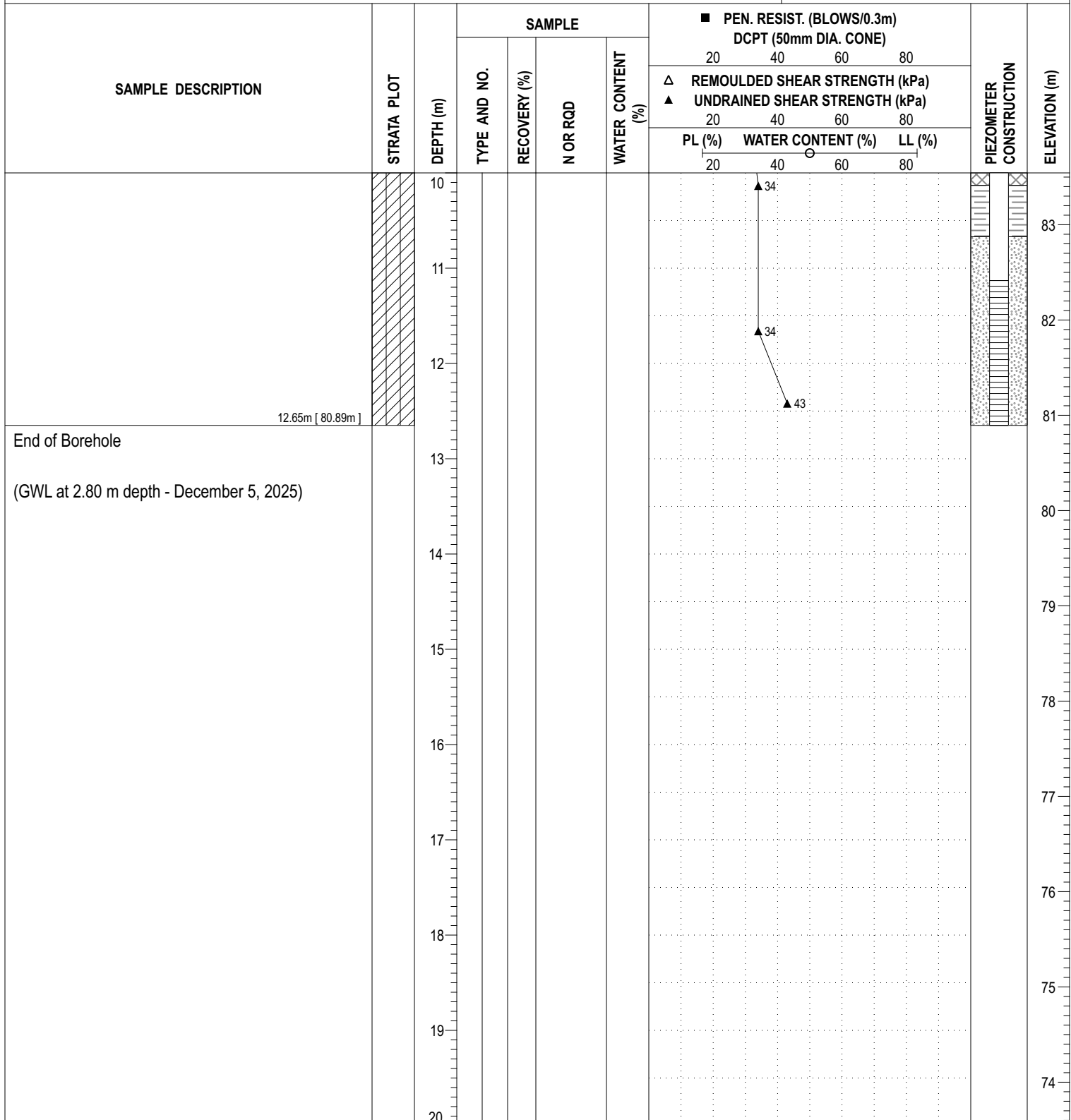
COORD. SYS.: MTM ZONE 9 **EASTING:** 350014.26 **NORTHING:** 5018644.26 **ELEVATION:** 93.54

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 17, 2025

HOLE NO. : BH33-25


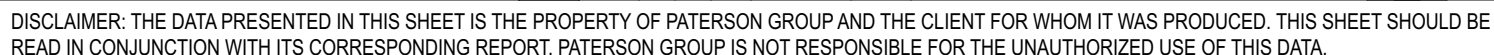
DISCLAIMER: THE DATA PRESENTED IN THIS SHEET IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHOM IT WAS PRODUCED. THIS SHEET SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

ELEVATION: 92.87

FILE NO. : PG7751

HOLE NO. : BH34-25

DATE: November 17, 2025





ELEVATION: 92.87

FILE NO. : PG7751

HOLE NO. : BH34-25

DATE: November 17, 2025

PAGE: 2 / 2

COORD. SYS.: MTM ZONE 9

EASTING: 350063.31

NORTHING: 5018901.38

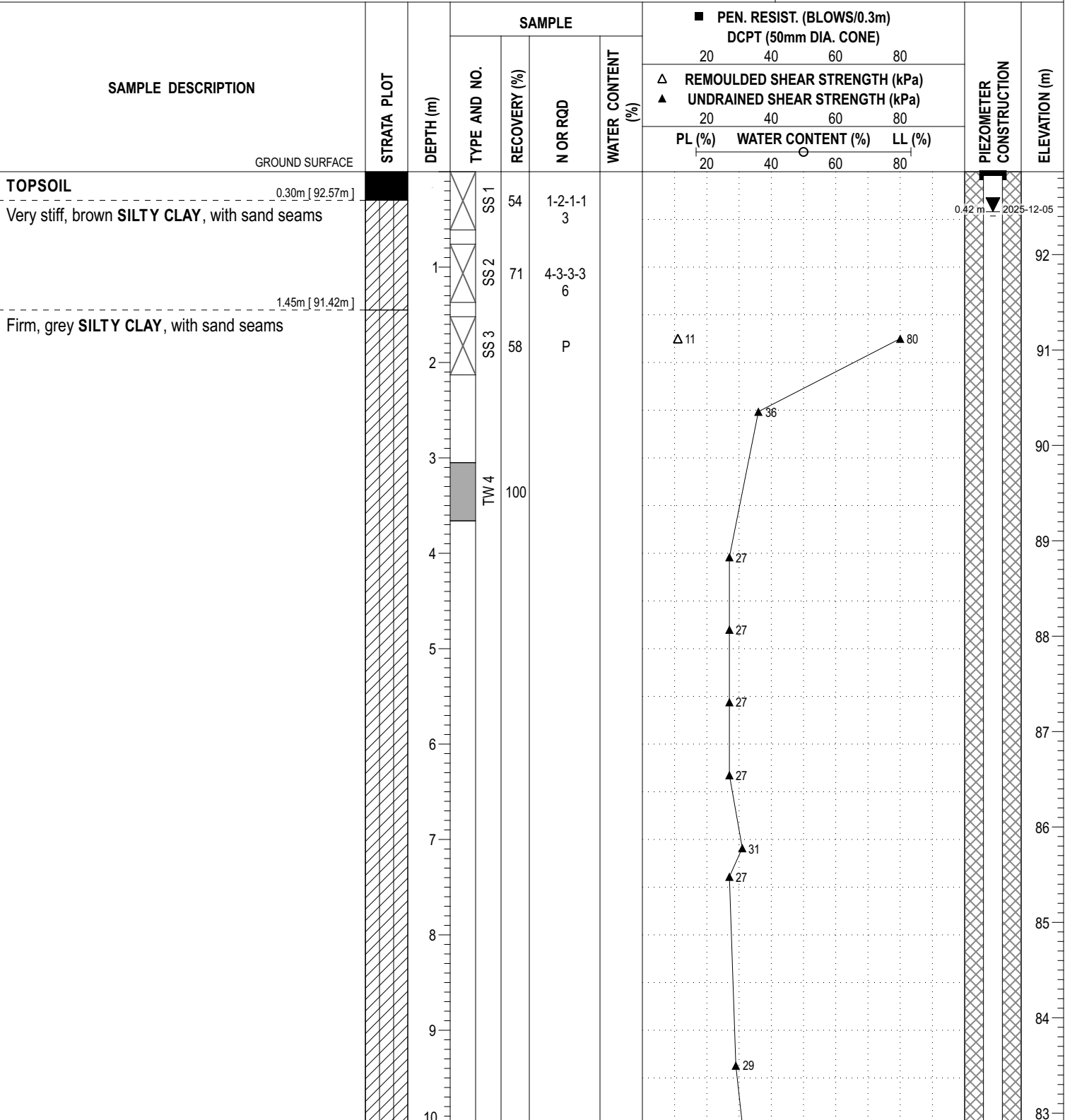
ELEVATION: 92.87

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

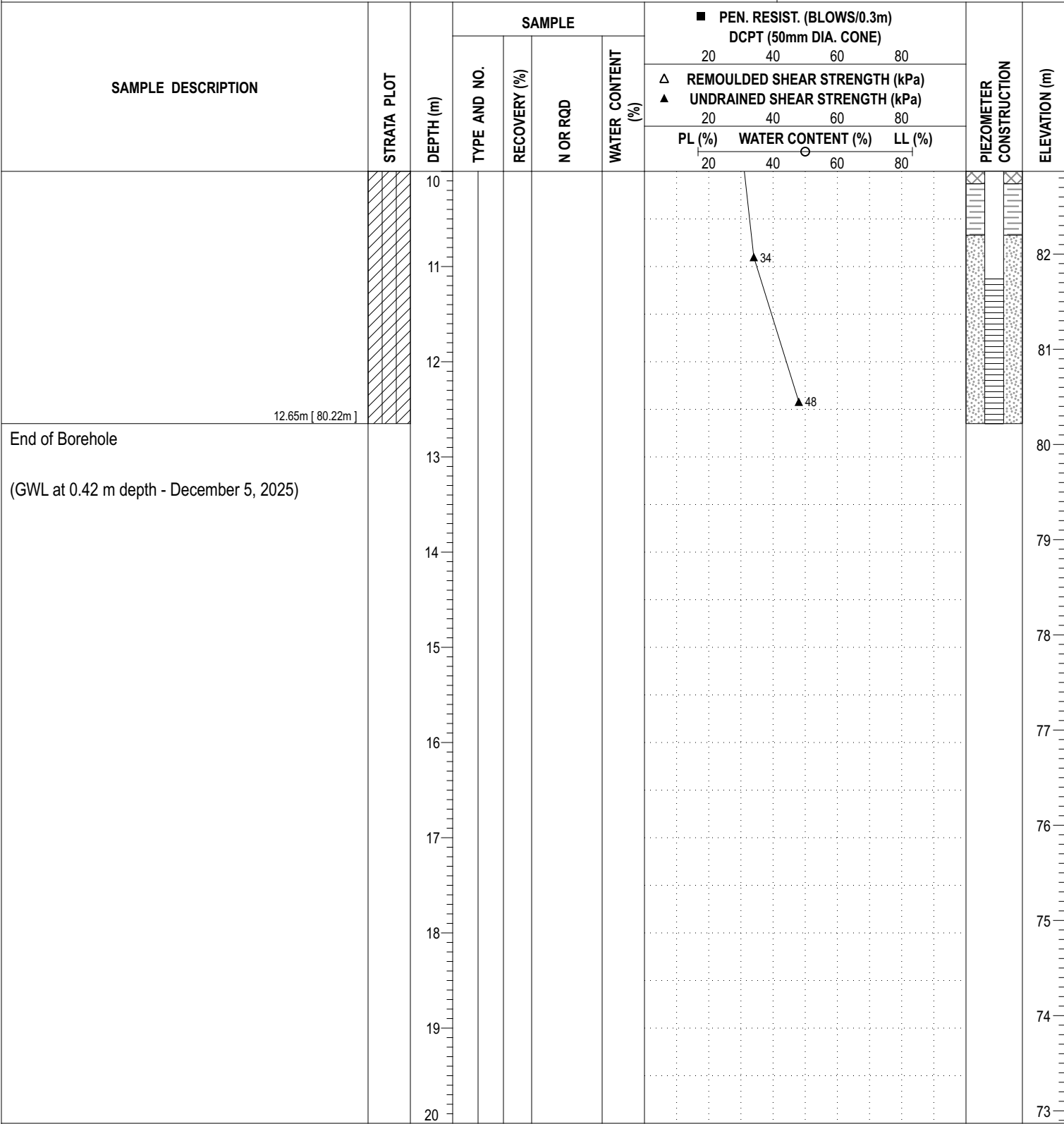
REMARKS:
DATE: November 18, 2025

HOLE NO. : BH35-25


DISCLAIMER: THE DATA PRESENTED IN THIS SHEET IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHOM IT WAS PRODUCED. THIS SHEET SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.



COORD. SYS.: MTM ZONE 9		EASTING: 350063.31	NORTHING: 5018901.38	ELEVATION: 92.87
PROJECT: Proposed Commercial Development				FILE NO. : PG7751
ADVANCED BY: CME-55 Low Clearance Drill				HOLE NO. : BH35-25
REMARKS:				DATE: November 18, 2025



DISCLAIMER: THE DATA PRESENTED IN THIS SHEET IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHOM IT WAS PRODUCED. THIS SHEET SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.



COORD. SYS.: MTM ZONE 9 **EASTING:** 350083.06 **NORTHING:** 5018964.83 **ELEVATION:** 93.49

PROJECT: Proposed Commercial Development

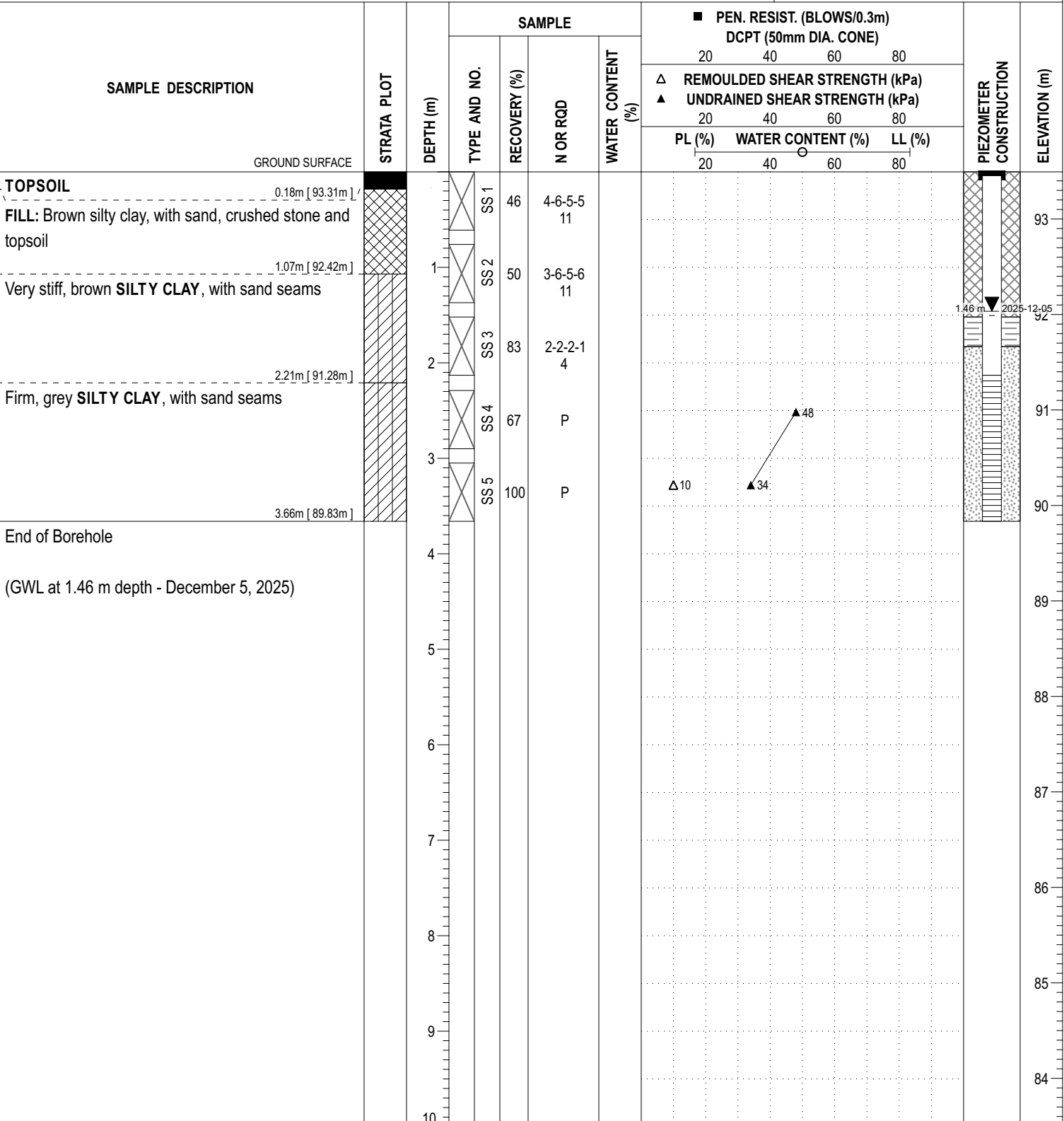
ADVANCED BY: CME-55 Low Clearance Drill

FILE NO. : PG7751

REMARKS:

DATE: November 18, 2025

HOLE NO. : BH36-25



DISCLAIMER: THE DATA PRESENTED IN THIS SHEET IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHOM IT WAS PRODUCED. THIS SHEET SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

COORD. SYS.: MTM ZONE 9 **EASTING:** 350088.68

NORTHING: 5018774.23

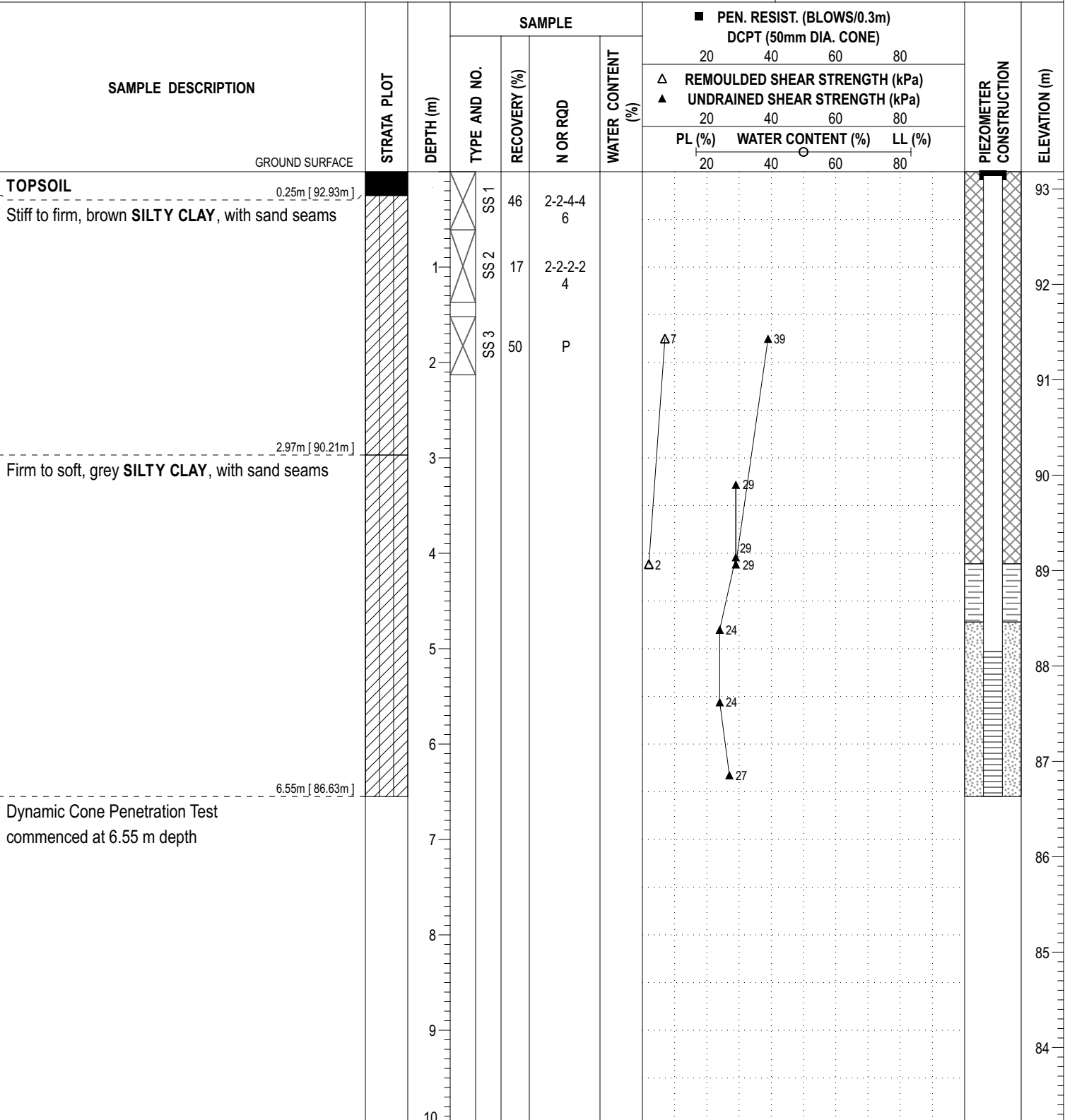
ELEVATION: 93.18

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 18, 2025

HOLE NO. : BH37-25


DISCLAIMER: THE DATA PRESENTED IN THIS SHEET IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHOM IT WAS PRODUCED. THIS SHEET SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

COORD. SYS.: MTM ZONE 9 **EASTING:** 350088.68 **NORTHING:** 5018774.23 **ELEVATION:** 93.18

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 18, 2025

HOLE NO. : BH37-25

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)				PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N OR RQD	WATER CONTENT (%)	20	40	60	80			
							Δ	REMOULDED SHEAR STRENGTH (kPa)					
							▲	UNDRAINED SHEAR STRENGTH (kPa)					
							PL (%)	WATER CONTENT (%)		LL (%)			
20	40	60	80										
Dynamic Cone Penetration Test		10										83	
		11										82	
		12										81	
		13										80	
		14										79	
		15										78	
		16										77	
		17										76	
		18										75	
		19										74	
		20											

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COORD. SYS.: MTM ZONE 9 **EASTING:** 350088.68 **NORTHING:** 5018774.23 **ELEVATION:** 93.18

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 18, 2025

HOLE NO. : BH37-25

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)				PIEZOMETER CONSTRUCTION	ELEVATION (m)
			TYPE AND NO.	RECOVERY (%)	N OR RQD	WATER CONTENT (%)	20	40	60	80		
							△ REMOULDED SHEAR STRENGTH (kPa)					
							▲ UNDRAINED SHEAR STRENGTH (kPa)					
							PL (%)	WATER CONTENT (%)		LL (%)		
					20	40	60	80				
Dynamic Cone Penetration Test		20									73	
		21									72	
		22									71	
		23									70	
		24									69	
		25									68	
		26									67	
		27									66	
		28									65	
		29									64	
		30										

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COORD. SYS.: MTM ZONE 9 EASTING: 350088.68 NORTHING: 5018774.23 ELEVATION: 93.18

PROJECT: Proposed Commercial Development FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS: DATE: November 18, 2025 HOLE NO. : BH37-25

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)				PIEZOMETER CONSTRUCTION	ELEVATION (m)
			TYPE AND NO.	RECOVERY (%)	N OR RQD	WATER CONTENT (%)	20	40	60	80		
							△ REMOULDED SHEAR STRENGTH (kPa)					
							▲ UNDRAINED SHEAR STRENGTH (kPa)					
							PL (%)	WATER CONTENT (%)		LL (%)		
					20	40	60	80				
Dynamic Cone Penetration Test		30										63
		31										62
		32										61
		33										60
		34										59
		35										58
		36										57
		37										56
		38										55
		39										54
		40										

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ELEVATION: 93.18

FILE NO. : PG7751

HOLE NO. : BH37-25

DATE: November 18, 2025

PAGE: 5 / 5



COORD. SYS.: MTM ZONE 9		EASTING: 350088.68	NORTHING: 5018774.23	ELEVATION: 93.18
PROJECT: Proposed Commercial Development				FILE NO. : PG7751
ADVANCED BY: CME-55 Low Clearance Drill				HOLE NO. : BH37B-25
REMARKS:				DATE: November 18, 2025

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)				PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N OR RQD	WATER CONTENT (%)	20	40	60	80			
							△ REMOULDED SHEAR STRENGTH (kPa)						
							▲ UNDRAINED SHEAR STRENGTH (kPa)						
							20	40	60	80			
PL (%)	WATER CONTENT (%)		LL (%)										
20	40	60	80										
GROUND SURFACE													
	Refer to soil profile in BH 37-25											93	
													92
													91
													90
													89
													88
													87
													86
													85
													84

COORD. SYS.: MTM ZONE 9 **EASTING:** 350088.68 **NORTHING:** 5018774.23 **ELEVATION:** 93.18

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 18, 2025

HOLE NO. : BH37B-25

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)				PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N OR RQD	WATER CONTENT (%)	20	40	60	80			
							Δ	REMOULDED SHEAR STRENGTH (kPa)					
							▲	UNDRAINED SHEAR STRENGTH (kPa)					
							PL (%)	WATER CONTENT (%)		LL (%)			
Dynamic Cone Penetration Test		10										83	
		11										82	
		12										81	
		13										80	
		14										79	
		15										78	
		16										77	
		17										76	
		18										75	
		19										74	
		20											

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COORD. SYS.: MTM ZONE 9 **EASTING:** 350088.68 **NORTHING:** 5018774.23 **ELEVATION:** 93.18

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS:
DATE: November 18, 2025

HOLE NO. : BH37B-25

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)				PIEZOMETER CONSTRUCTION	ELEVATION (m)
			TYPE AND NO.	RECOVERY (%)	N OR RQD	WATER CONTENT (%)	20	40	60	80		
							△ REMOULDED SHEAR STRENGTH (kPa)					
							▲ UNDRAINED SHEAR STRENGTH (kPa)					
							PL (%)	WATER CONTENT (%)		LL (%)		
					20	40	60	80				
Dynamic Cone Penetration Test		20										73
		21										72
		22										71
		23										70
		24										69
		25										68
		26										67
		27										66
		28										65
		29										64
		30										

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COORD. SYS.: MTM ZONE 9		EASTING: 350088.68	NORTHING: 5018774.23	ELEVATION: 93.18
PROJECT: Proposed Commercial Development				FILE NO. : PG7751
ADVANCED BY: CME-55 Low Clearance Drill				HOLE NO. : BH37B-25
REMARKS:				DATE: November 18, 2025

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)				PIEZOMETER CONSTRUCTION	ELEVATION (m)
			TYPE AND NO.	RECOVERY (%)	N OR RQD	WATER CONTENT (%)	20	40	60	80		
							△ REMOULDED SHEAR STRENGTH (kPa)					
							▲ UNDRAINED SHEAR STRENGTH (kPa)					
							20	40	60	80		
PL (%)		WATER CONTENT (%)		LL (%)								
20		40		60		80						

Dynamic Cone Penetration Test		30										63
		31										62
		32										61
		33										60
		34										59
		35										58
	36										57	
	37										56	
	38										55	
	39										54	
	40											

COORD. SYS.: MTM ZONE 9	EASTING: 350088.68	NORTHING: 5018774.23	ELEVATION: 93.18
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PROJECT: Proposed Commercial Development ADVANCED BY: CME-55 Low Clearance Drill REMARKS:	FILE NO. : PG7751 HOLE NO. : BH37B-25
--	--

DATE: November 18, 2025

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)				PIEZOMETER CONSTRUCTION	ELEVATION (m)
			TYPE AND NO.	RECOVERY (%)	N OR RQD	WATER CONTENT (%)	20	40	60	80		
							△ REMOULDED SHEAR STRENGTH (kPa)					
							▲ UNDRAINED SHEAR STRENGTH (kPa)					
							PL (%) WATER CONTENT (%) LL (%)					
						20	40	60	80			
44.32m [48.86m] End of Borehole Practical refusal to DCPT at 44.32 m depth DCPT pushed to 44.32 m depth		40									53	
		41									52	
		42									51	
		43									50	
		44									49	
		45									48	
		46								47		
		47								46		
		48								45		
		49								44		
		50										

44.32m [48.86m]

End of Borehole

Practical refusal to DCPT at 44.32 m depth

DCPT pushed to 44.32 m depth

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COORD. SYS.: MTM ZONE 9

EASTING: 350143.77

NORTHING: 5018687.55

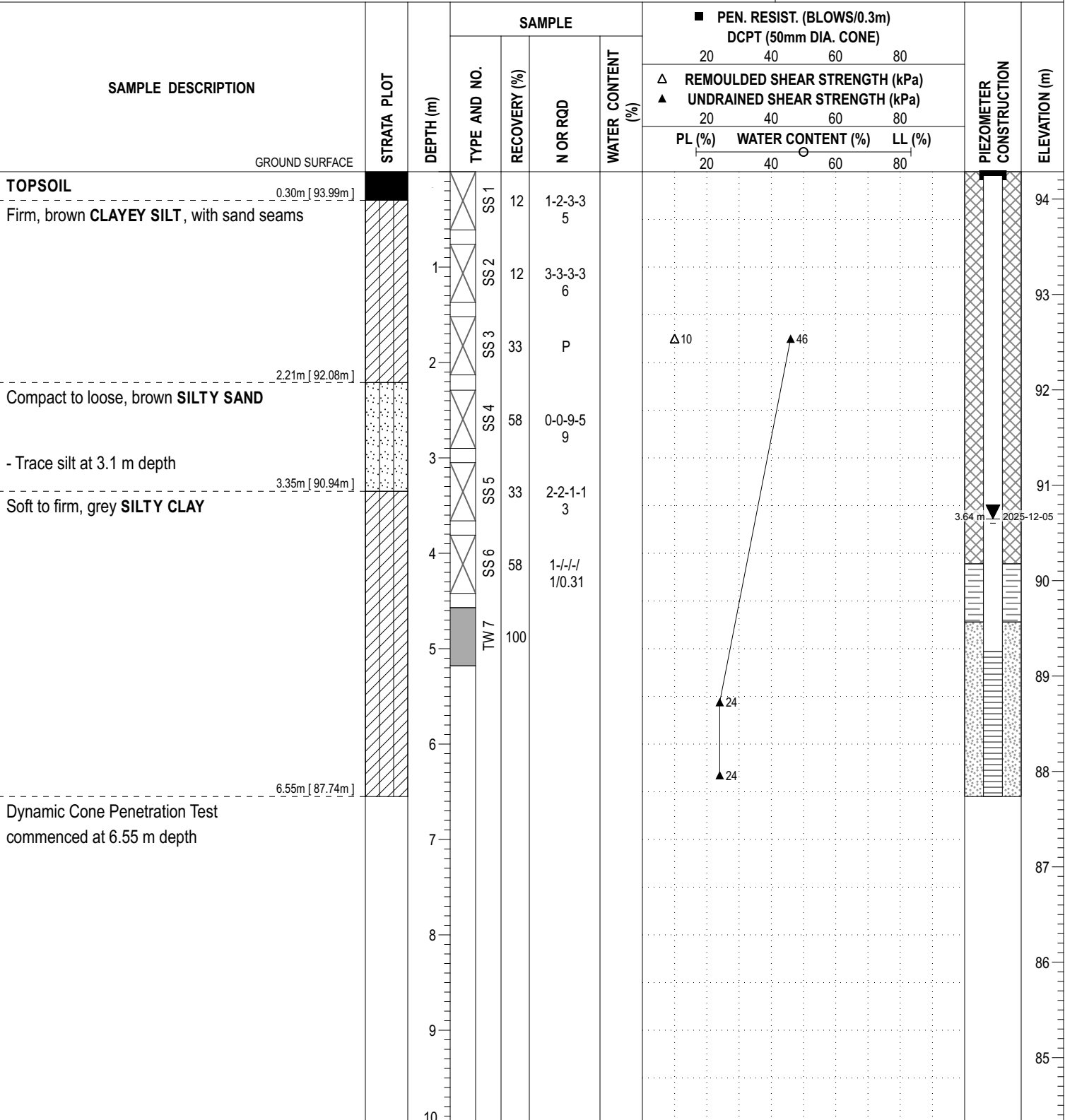
ELEVATION: 94.29

PROJECT: Proposed Commercial Development

ADVANCED BY: CME-55 Low Clearance Drill

FILE NO. : PG7751

REMARKS:
DATE: November 19, 2025

HOLE NO. : BH38-25


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COORD. SYS.: MTM ZONE 9		EASTING: 350143.77	NORTHING: 5018687.55	ELEVATION: 94.29
PROJECT: Proposed Commercial Development			FILE NO. : PG7751	HOLE NO. : BH38-25
ADVANCED BY: CME-55 Low Clearance Drill				
REMARKS:			DATE: November 19, 2025	

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)				PIEZOMETER CONSTRUCTION	ELEVATION (m)
			TYPE AND NO.	RECOVERY (%)	N OR RQD	WATER CONTENT (%)	20	40	60	80		
							△ REMOULDED SHEAR STRENGTH (kPa)					
							▲ UNDRAINED SHEAR STRENGTH (kPa)					
							20	40	60	80		
PL (%)		WATER CONTENT (%)		LL (%)								
20		40		60		80						

Dynamic Cone Penetration Test		10											84
		11											83
		12											82
		13											81
		14											80
		15											79
		16											78
		17											77
	18											76	
	19											75	
	20												

COORD. SYS.: MTM ZONE 9 **EASTING:** 350143.77 **NORTHING:** 5018687.55 **ELEVATION:** 94.29

PROJECT: Proposed Commercial Development **FILE NO. :** PG7751

ADVANCED BY: CME-55 Low Clearance Drill

REMARKS: **DATE:** November 19, 2025 **HOLE NO. :** BH38-25

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)				PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N OR RQD	WATER CONTENT (%)	20	40	60	80			
							Δ REMOULDED SHEAR STRENGTH (kPa)						
							▲ UNDRAINED SHEAR STRENGTH (kPa)	20	40	60			80
							PL (%)	WATER CONTENT (%)		LL (%)			
	20	40	60	80									
Dynamic Cone Penetration Test		20										74	
		21										73	
		22										72	
		23										71	
		24										70	
25.15m [69.14m]		25									69		
End of Borehole													
Practical refusal to DCPT at 25.15 m depth		26									68		
DCPT pushed to 25.15 m depth													
(GWL at 3.64 m depth - December 5, 2025)		27									67		
		28									66		
		29									65		
		30											

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic
elevation = 95.01m.

REMARKS

FILE NO.

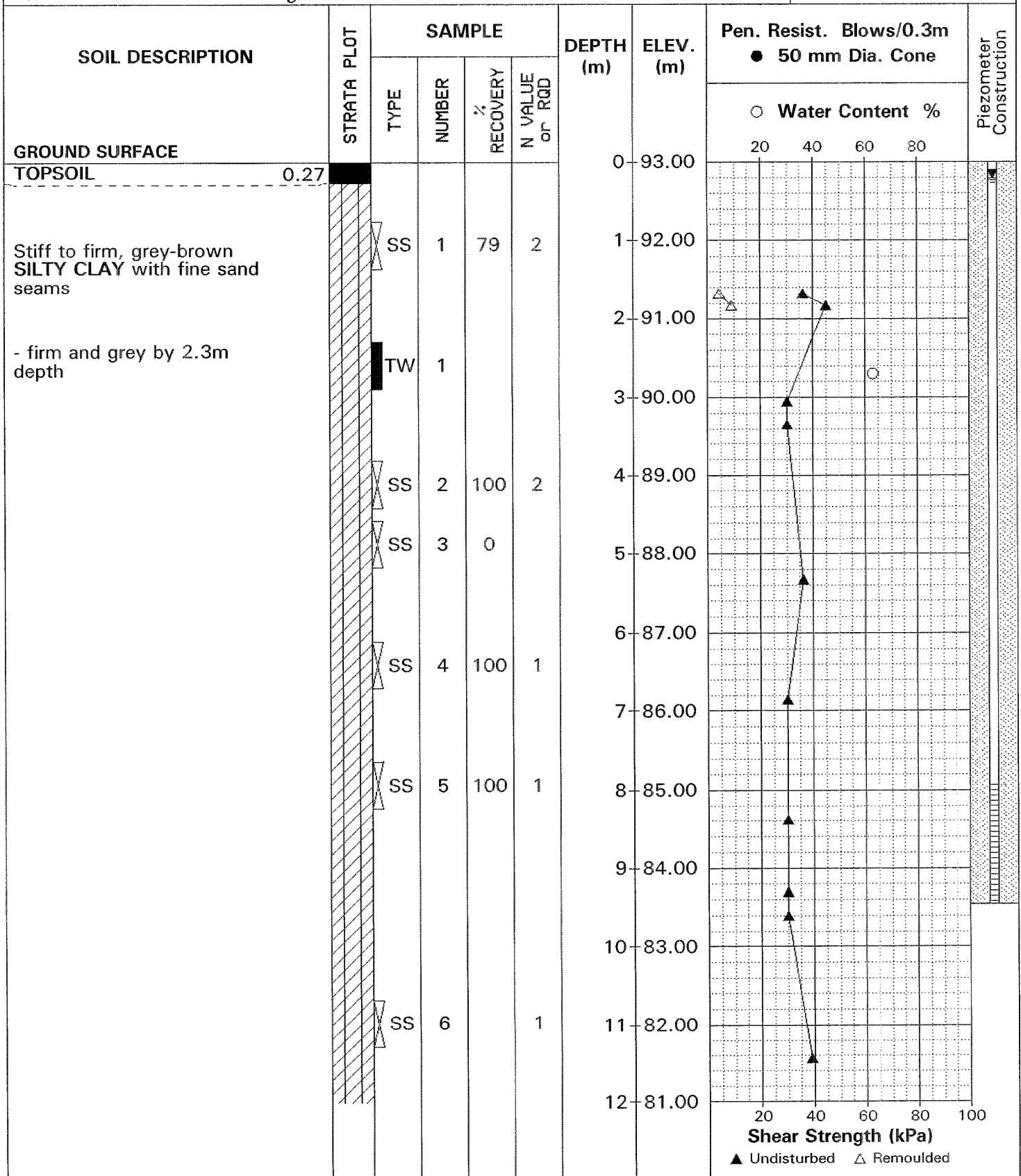
PG0475

HOLE NO.

BH 1

BORINGS BY CME 55 Power Auger

DATE 18 NOV 04



SOIL PROFILE & TEST DATA

Geotechnical Investigation

Proposed Commercial Development, Didsbury Road
Ottawa (Kanata), Ontario

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic
elevation = 95.01m.

REMARKS

FILE NO.

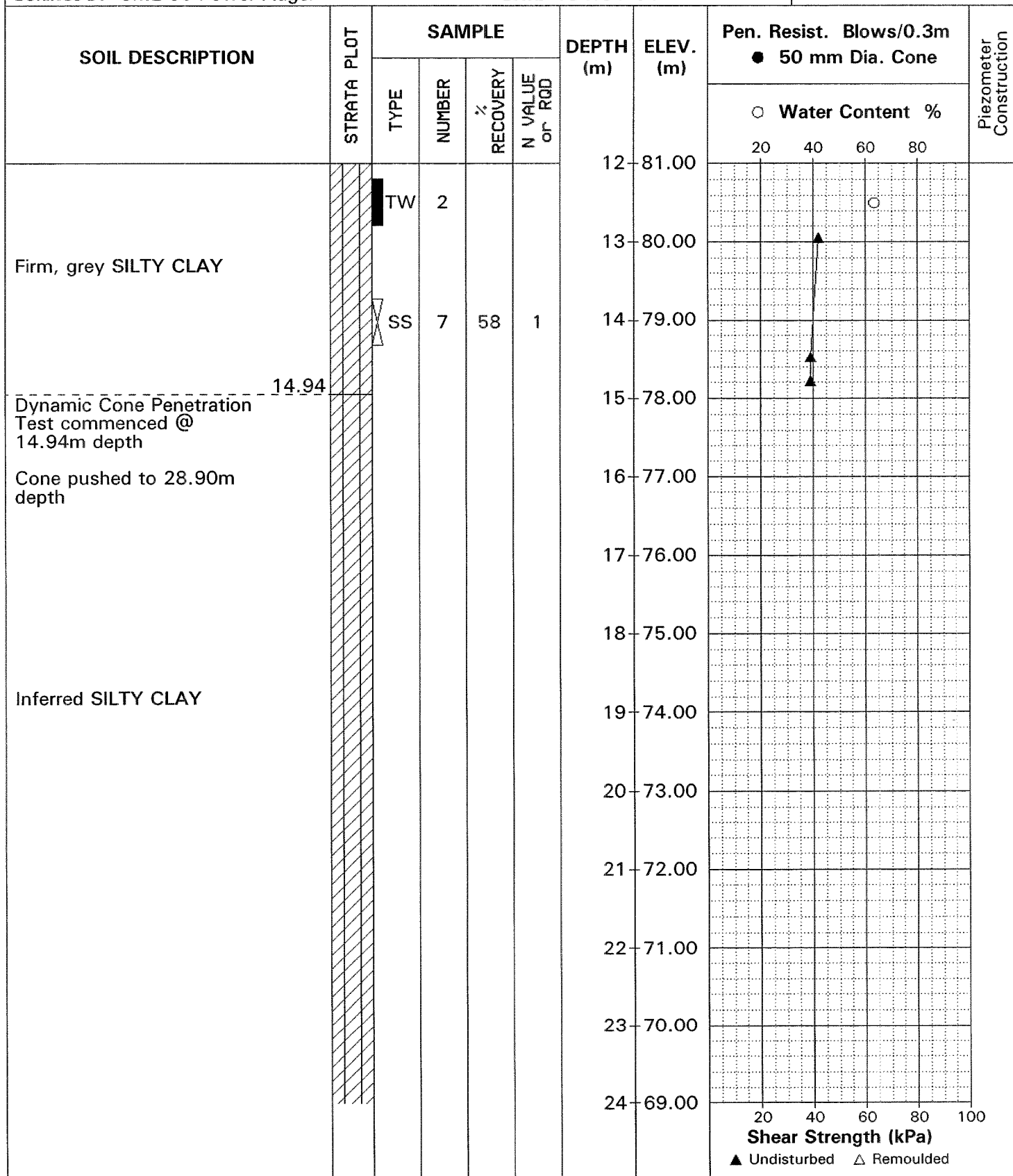
PG0475

HOLE NO.

BH 1

BORINGS BY CME 55 Power Auger

DATE 18 NOV 04



SOIL PROFILE & TEST DATA

Geotechnical Investigation

Proposed Commercial Development, Didsbury Road
Ottawa (Kanata), Ontario

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic
elevation = 95.01m.

REMARKS

FILE NO.

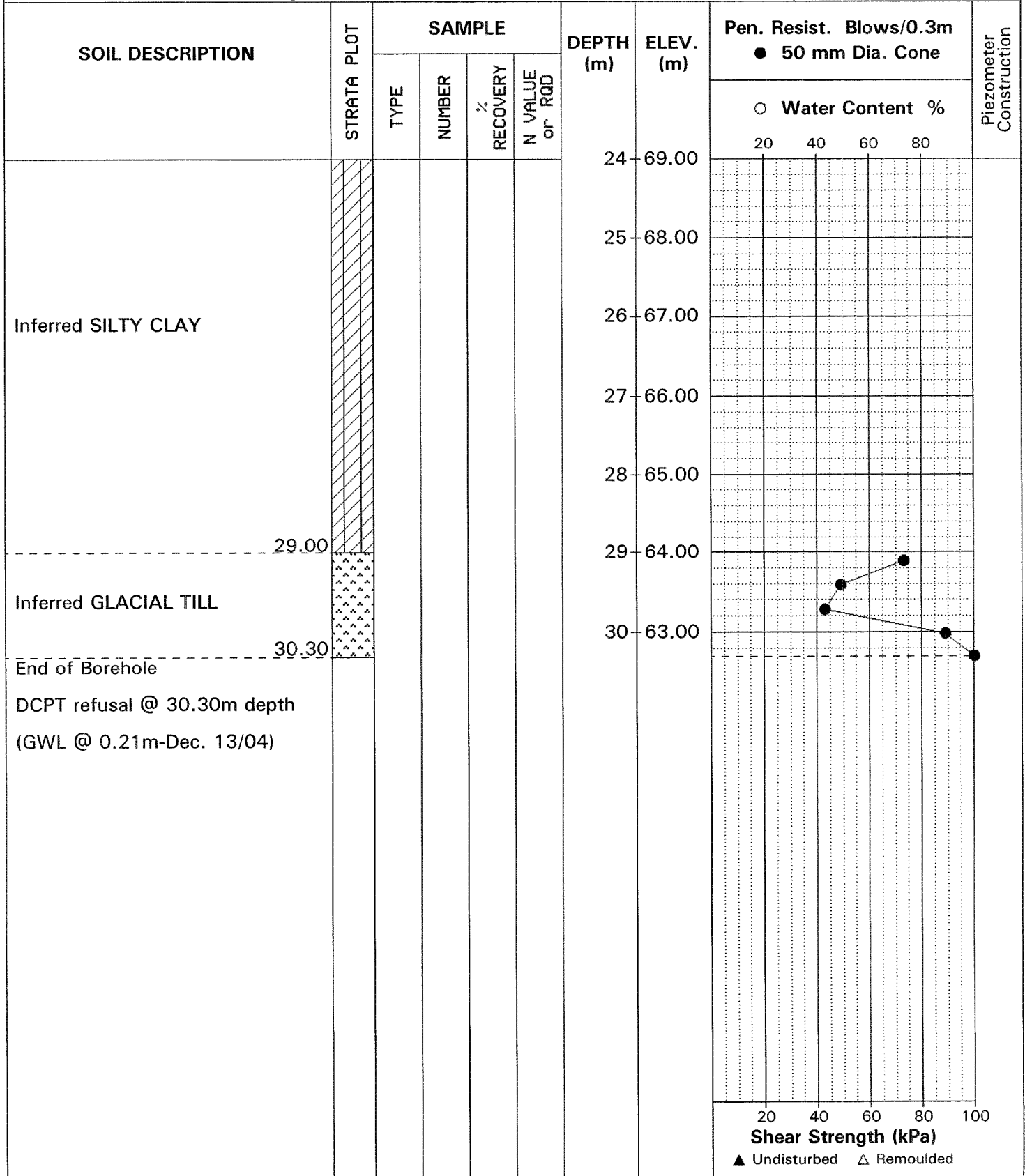
PG0475

HOLE NO.

BH 1

BORINGS BY CME 55 Power Auger

DATE 18 NOV 04



DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic
elevation = 95.01m.

REMARKS

FILE NO.

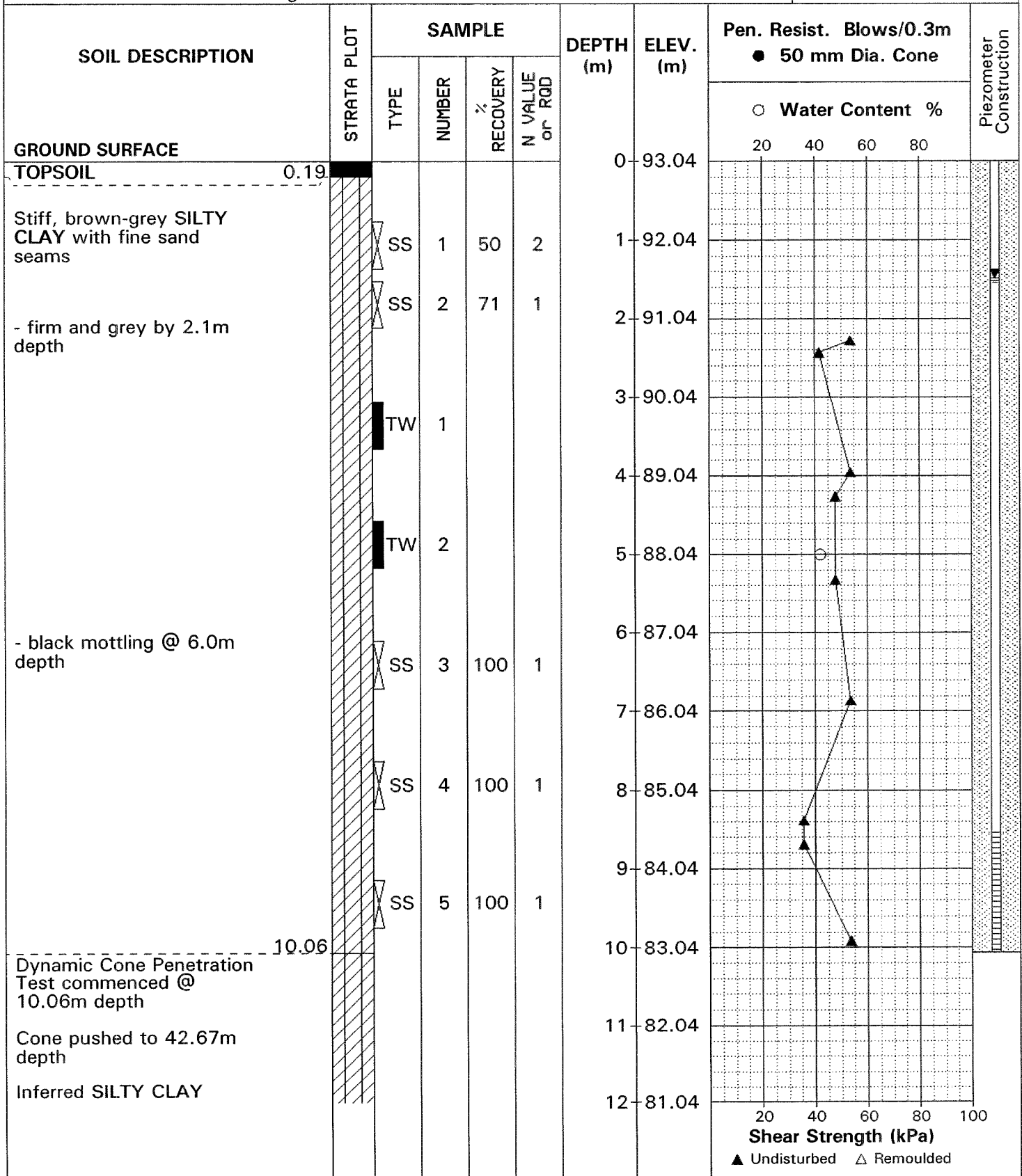
PG0475

HOLE NO.

BH 2

BORINGS BY CME 55 Power Auger

DATE 22 NOV 04



SOIL PROFILE & TEST DATA

Geotechnical Investigation
Proposed Commercial Development, Didsbury Road
Ottawa (Kanata), Ontario

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic elevation = 95.01m.

REMARKS

FILE NO.

PG0475

HOLE NO.

BH 2

BORINGS BY CME 55 Power Auger

DATE 22 NOV 04

SOIL DESCRIPTION	STRATA PLOT	SAMPLE				DEPTH (m)	ELEV. (m)	Pen. Resist. Blows/0.3m ● 50 mm Dia. Cone				Piezometer Construction
		TYPE	NUMBER	½ RECOVERY	N VALUE or RQD			○ Water Content %				
								20	40	60	80	
Inferred SILTY CLAY						12	81.04					
						13	80.04					
						14	79.04					
						15	78.04					
						16	77.04					
						17	76.04					
						18	75.04					
						19	74.04					
						20	73.04					
						21	72.04					
						22	71.04					
						23	70.04					
						24	69.04					
								20	40	60	80	100
								Shear Strength (kPa)				
								▲ Undisturbed △ Remoulded				

SOIL PROFILE & TEST DATA

Geotechnical Investigation

Proposed Commercial Development, Didsbury Road
Ottawa (Kanata), Ontario

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic
elevation = 95.01m.

REMARKS

FILE NO.

PG0475

HOLE NO.

BH 2

BORINGS BY CME 55 Power Auger

DATE 22 NOV 04

SOIL DESCRIPTION	STRATA PLOT	SAMPLE				DEPTH (m)	ELEV. (m)	Pen. Resist. Blows/0.3m ● 50 mm Dia. Cone				Piezometer Construction	
		TYPE	NUMBER	¾ RECOVERY	N VALUE or RQD			○ Water Content %					
								20	40	60	80		
Inferred SILTY CLAY						24	69.04						
						25	68.04						
						26	67.04						
						27	66.04						
						28	65.04						
						29	64.04						
						30	63.04						
						31	62.04						
						32	61.04						
						33	60.04						
						34	59.04						
						35	58.04						
						36	57.04						
							20	40	60	80	100		
							Shear Strength (kPa)						
							▲ Undisturbed △ Remoulded						

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic elevation = 95.01m.

REMARKS

FILE NO.

PG0475

HOLE NO.

BH 2

BORINGS BY CME 55 Power Auger

DATE 22 NOV 04

SOIL DESCRIPTION	STRATA PLOT	SAMPLE				DEPTH (m)	ELEV. (m)	Pen. Resist. Blows/0.3m ● 50 mm Dia. Cone				Piezometer Construction	
		TYPE	NUMBER	% RECOVERY	N VALUE or RQD			○ Water Content %					
								20	40	60	80		
Inferred SILTY CLAY						36	57.04						
						37	56.04						
						38	55.04						
						39	54.04						
						40	53.04						
						41	52.04						
						42	51.04						
Inferred GLACIAL TILL													
End of Borehole													
DCPT refusal @ 42.82m depth (GWL 1.49m-Dec. 13/04)													

42.60
42.82

20406080100

Shear Strength (kPa)

▲ Undisturbed △ Remoulded

SOIL PROFILE & TEST DATA

Geotechnical Investigation

Proposed Commercial Development, Didsbury Road
Ottawa (Kanata), Ontario

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic
elevation = 95.01m.

REMARKS

FILE NO.

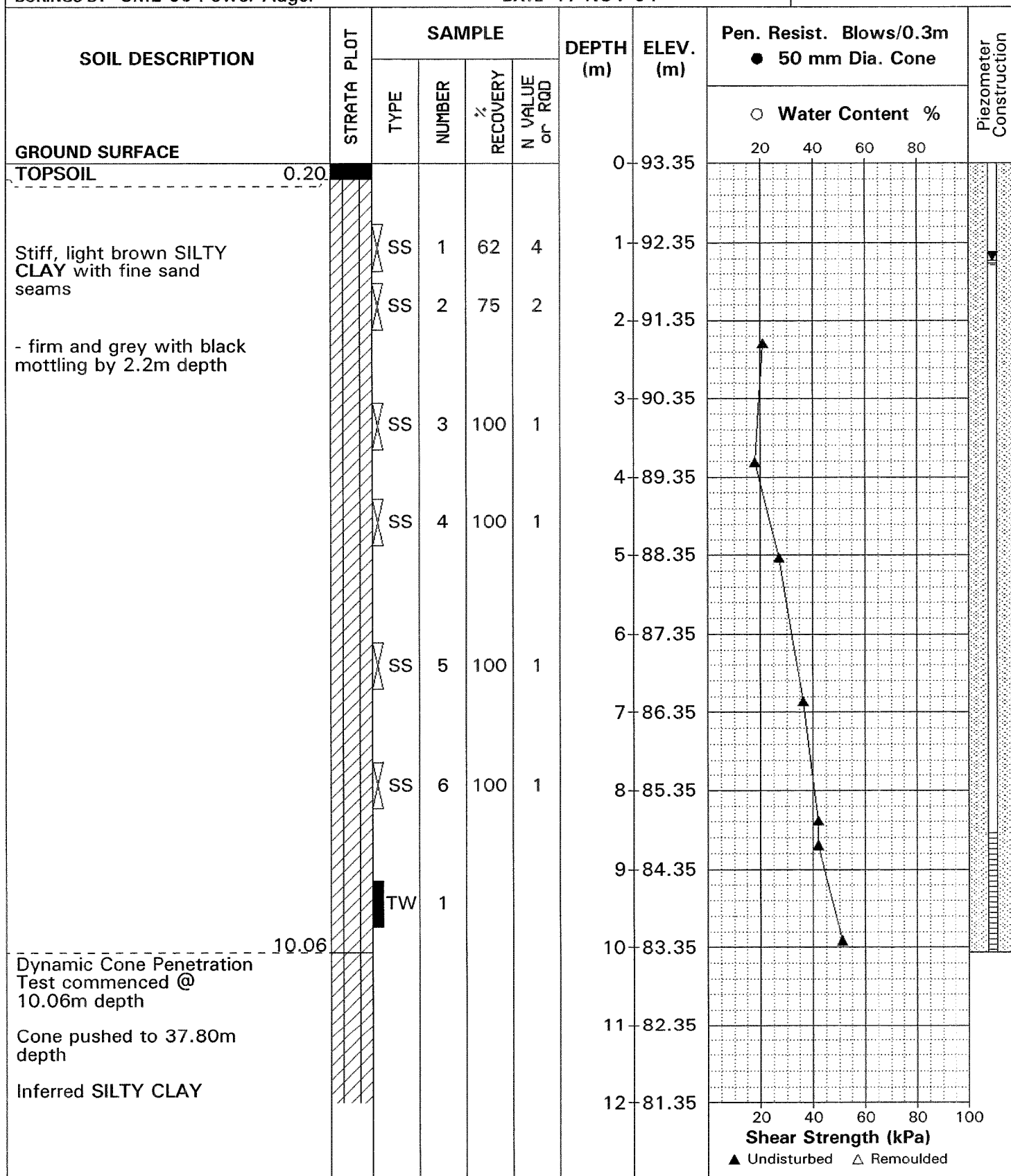
PG0475

HOLE NO.

BH 3

BORINGS BY CME 55 Power Auger

DATE 17 NOV 04



SOIL PROFILE & TEST DATA

Geotechnical Investigation

Proposed Commercial Development, Didsbury Road
Ottawa (Kanata), Ontario

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic
elevation = 95.01m.

REMARKS

FILE NO.

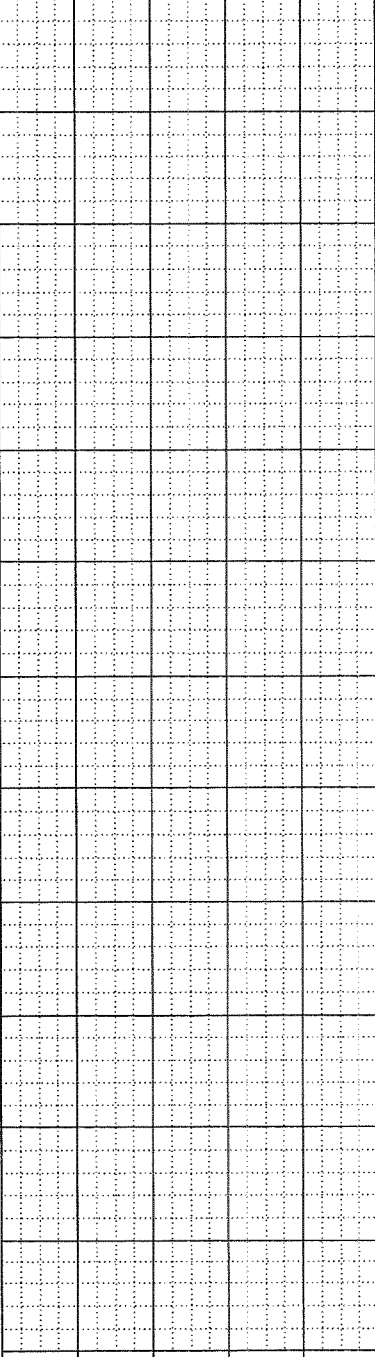
PG0475

HOLE NO.

BH 3

BORINGS BY CME 55 Power Auger

DATE 17 NOV 04

SOIL DESCRIPTION	STRATA PLOT	SAMPLE				DEPTH (m)	ELEV. (m)	Pen. Resist. Blows/0.3m ● 50 mm Dia. Cone				Piezometer Construction
		TYPE	NUMBER	% RECOVERY	N VALUE or RQD			○ Water Content %				
								20	40	60	80	
Inferred SILTY CLAY						12	81.35					
						13	80.35					
						14	79.35					
						15	78.35					
						16	77.35					
						17	76.35					
						18	75.35					
						19	74.35					
						20	73.35					
						21	72.35					
						22	71.35					
						23	70.35					
						24	69.35					
								20	40	60	80	100
								Shear Strength (kPa)				
								▲ Undisturbed △ Remoulded				

SOIL PROFILE & TEST DATA

Geotechnical Investigation

Proposed Commercial Development, Didsbury Road
Ottawa (Kanata), Ontario

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic
elevation = 95.01m.

REMARKS

FILE NO.

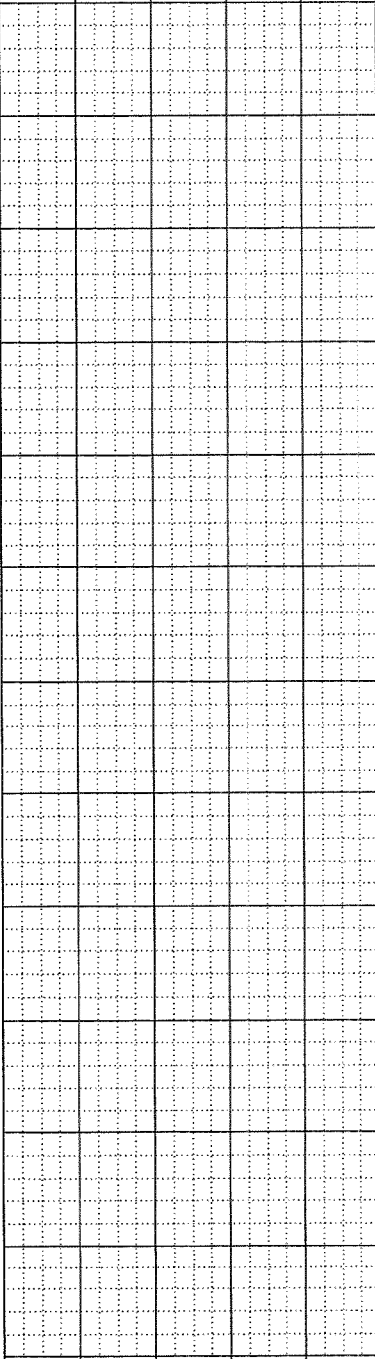
PG0475

HOLE NO.

BH 3

BORINGS BY CME 55 Power Auger

DATE 17 NOV 04

SOIL DESCRIPTION	STRATA PLOT	SAMPLE				DEPTH (m)	ELEV. (m)	Pen. Resist. Blows/0.3m ● 50 mm Dia. Cone				Piezometer Construction
		TYPE	NUMBER	RECOVERY %	N VALUE or RQD			○ Water Content %				
								20	40	60	80	
Inferred SILTY CLAY						24	69.35					
						25	68.35					
						26	67.35					
						27	66.35					
						28	65.35					
						29	64.35					
						30	63.35					
						31	62.35					
						32	61.35					
						33	60.35					
						34	59.35					
						35	58.35					
						36	57.35					
								20	40	60	80	100
								Shear Strength (kPa)				
								▲ Undisturbed △ Remoulded				

SOIL PROFILE & TEST DATA

DATE 17 NOV 04

SOIL DESCRIPTION	STRATA PLOT	SAMPLE				DEPTH (m)	ELEV. (m)	Pen. Resist. Blows/0.3m ● 50 mm Dia. Cone				Piezometer Construction
		TYPE	NUMBER	% RECOVERY	N VALUE or RQD			○ Water Content %				
								20	40	60	80	
Inferred SILTY CLAY						36	57.35					
						37	56.35					
End of Borehole ----- 37.80												
(GWL @ 1.23-Dec. 13/04)												

Shear Strength (kPa)
▲ Undisturbed △ Remoulded

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic elevation = 95.01m.

REMARKS

FILE NO.

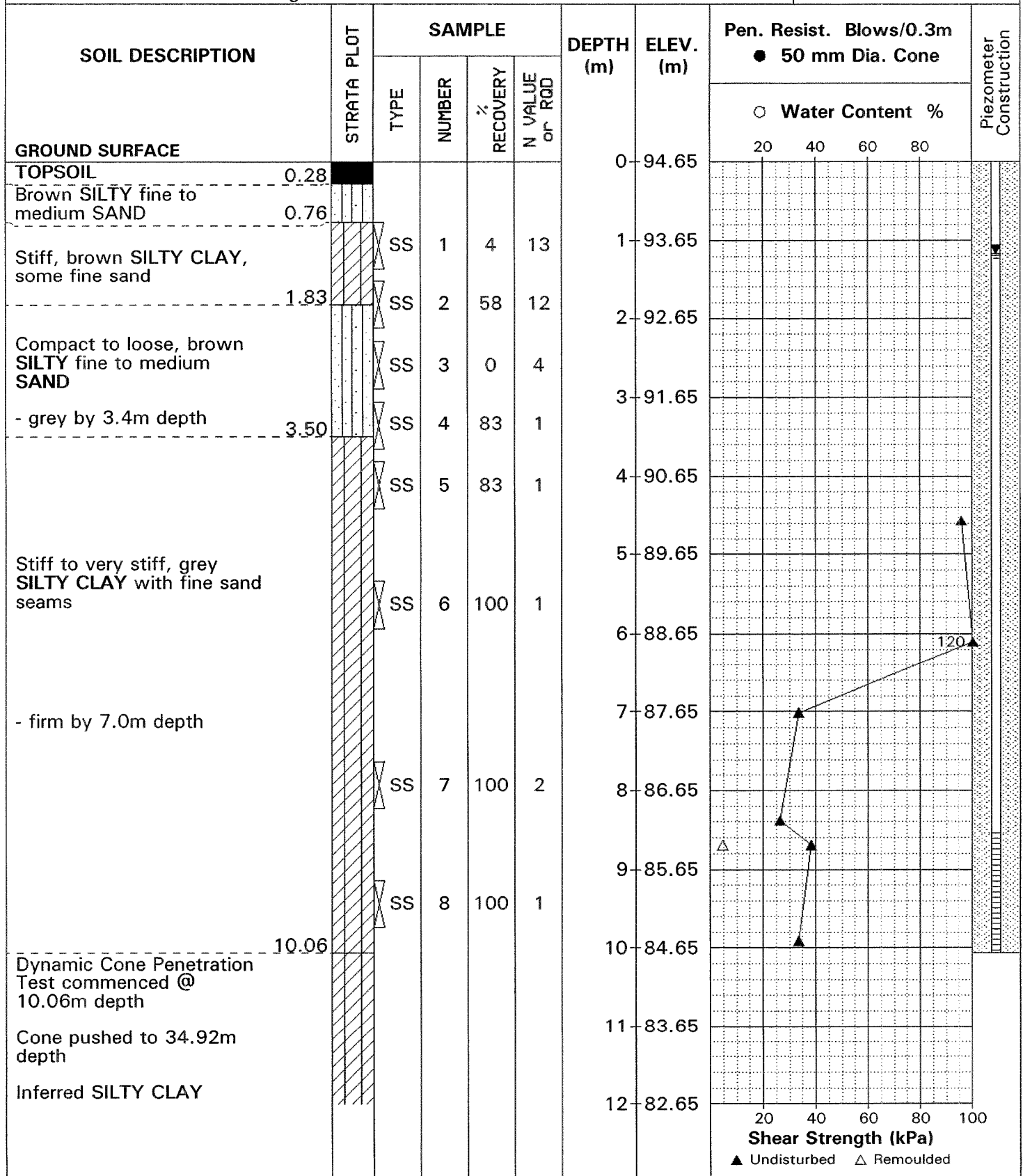
PG0475

HOLE NO.

BH 4

BORINGS BY CME 55 Power Auger

DATE 17 NOV 04



SOIL PROFILE & TEST DATA

Geotechnical Investigation

Proposed Commercial Development, Didsbury Road
Ottawa (Kanata), Ontario

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic
elevation = 95.01m.

REMARKS

FILE NO.

PG0475

HOLE NO.

BH 4

BORINGS BY CME 55 Power Auger

DATE 17 NOV 04

SOIL DESCRIPTION	STRATA PLOT	SAMPLE				DEPTH (m)	ELEV. (m)	Pen. Resist. Blows/0.3m ● 50 mm Dia. Cone				Piezometer Construction
		TYPE	NUMBER	% RECOVERY	N VALUE or RQD			○ Water Content %				
								20	40	60	80	
Inferred SILTY CLAY						12	82.65					
						13	81.65					
						14	80.65					
						15	79.65					
						16	78.65					
						17	77.65					
						18	76.65					
						19	75.65					
						20	74.65					
						21	73.65					
						22	72.65					
23	71.65											
24	70.65											

Shear Strength (kPa)

▲ Undisturbed △ Remoulded

SOIL PROFILE & TEST DATA

Geotechnical Investigation
Proposed Commercial Development, Didsbury Road
Ottawa (Kanata), Ontario

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic elevation = 95.01m.

REMARKS

FILE NO.

PG0475

HOLE NO.

BH 4

BORINGS BY CME 55 Power Auger

DATE 17 NOV 04

SOIL DESCRIPTION	STRATA PLOT	SAMPLE				DEPTH (m)	ELEV. (m)	Pen. Resist. Blows/0.3m ● 50 mm Dia. Cone				Piezometer Construction
		TYPE	NUMBER	RECOVERY %	N VALUE or RQD			○ Water Content %				
								20	40	60	80	
Inferred SILTY CLAY						24	70.65					
						25	69.65					
						26	68.65					
						27	67.65					
						28	66.65					
						29	65.65					
						30	64.65					
						31	63.65					
						32	62.65					
						33	61.65					
						34	60.65					
						35	59.65					
DCPT refusal @ 35.00m depth (GWL @ 1.17m-Dec. 13/04)												
								Shear Strength (kPa)				
								▲ Undisturbed △ Remoulded				

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic elevation = 95.01m.

REMARKS

FILE NO.

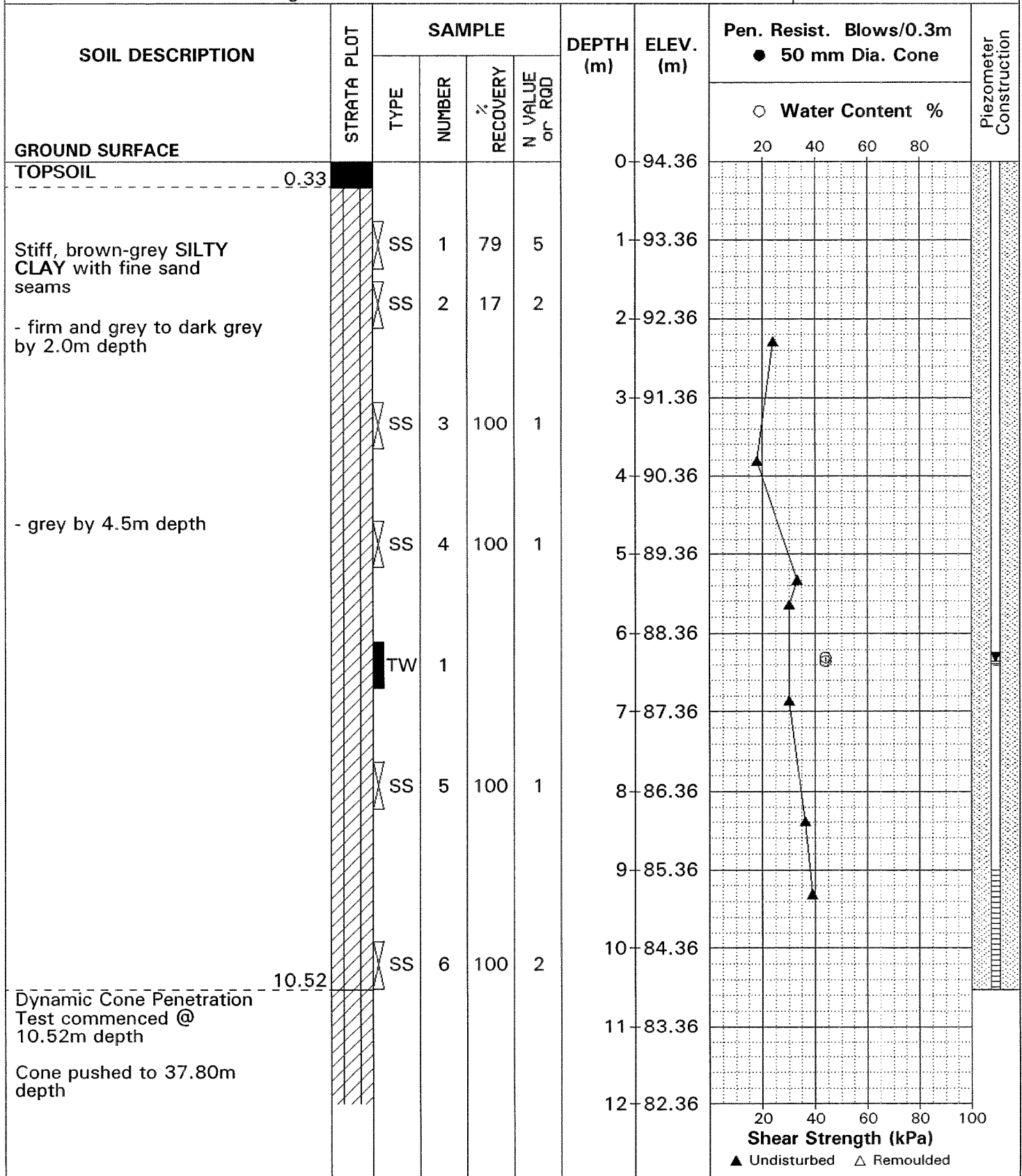
PG0475

HOLE NO.

BH 5

BORINGS BY CME 55 Power Auger

DATE 17 NOV 04



SOIL PROFILE & TEST DATA

Geotechnical Investigation
Proposed Commercial Development, Didsbury Road
Ottawa (Kanata), Ontario

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic elevation = 95.01m.

REMARKS

FILE NO.

PG0475

HOLE NO.

BH 5

BORINGS BY CME 55 Power Auger

DATE 17 NOV 04

SOIL DESCRIPTION	STRATA PLOT	SAMPLE				DEPTH (m)	ELEV. (m)	Pen. Resist. Blows/0.3m ● 50 mm Dia. Cone				Piezometer Construction
		TYPE	NUMBER	½ RECOVERY	N VALUE or RQD			○ Water Content %				
								20	40	60	80	
Inferred SILTY CLAY						12	82.36					
						13	81.36					
						14	80.36					
						15	79.36					
						16	78.36					
						17	77.36					
						18	76.36					
						19	75.36					
						20	74.36					
						21	73.36					
						22	72.36					
						23	71.36					
						24	70.36					
								20	40	60	80	100
								Shear Strength (kPa)				
								▲ Undisturbed △ Remoulded				

SOIL PROFILE & TEST DATA

Geotechnical Investigation

Proposed Commercial Development, Didsbury Road
Ottawa (Kanata), Ontario

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic
elevation = 95.01m.

REMARKS

FILE NO.

PG0475

HOLE NO.

BH 5

BORINGS BY CME 55 Power Auger

DATE 17 NOV 04

SOIL DESCRIPTION	STRATA PLOT	SAMPLE				DEPTH (m)	ELEV. (m)	Pen. Resist. Blows/0.3m ● 50 mm Dia. Cone				Piezometer Construction
		TYPE	NUMBER	% RECOVERY	N VALUE or RQD			○ Water Content %				
								20	40	60	80	
Inferred SILTY CLAY						24	70.36					
						25	69.36					
						26	68.36					
						27	67.36					
						28	66.36					
						29	65.36					
						30	64.36					
						31	63.36					
						32	62.36					
						33	61.36					
						34	60.36					
						35	59.36					
						36	58.36					
							20	40	60	80	100	
							Shear Strength (kPa)					
							▲ Undisturbed △ Remoulded					

28 Concourse Gate, Unit 1, Ottawa, ON K2E 7T7

SOIL PROFILE & TEST DATA

Geotechnical Investigation

**Proposed Commercial Development, Didsbury Road
Ottawa (Kanata), Ontario**

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic elevation = 95.01m.

REMARKS

FILE NO.

PG0475

HOLE NO.

BH 5

BORINGS BY CME 55 Power Auger

DATE 17 NOV 04

SOIL DESCRIPTION	STRATA PLOT	SAMPLE				DEPTH (m)	ELEV. (m)	Pen. Resist. Blows/0.3m ● 50 mm Dia. Cone				Piezometer Construction
		TYPE	NUMBER	% RECOVERY	N VALUE or RQD			○ Water Content %				
								20	40	60	80	
Inferred SILTY CLAY						36	58.36					
						37	57.36					
End of Borehole ----- 37.80												
(GWL @ 6.35m-Dec. 13/04)												

Shear Strength (kPa)
▲ Undisturbed △ Remoulded

SOIL PROFILE & TEST DATA

Geotechnical Investigation

Proposed Commercial Development, Didsbury Road
Ottawa (Kanata), Ontario

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic
elevation = 95.01m.

REMARKS

FILE NO.

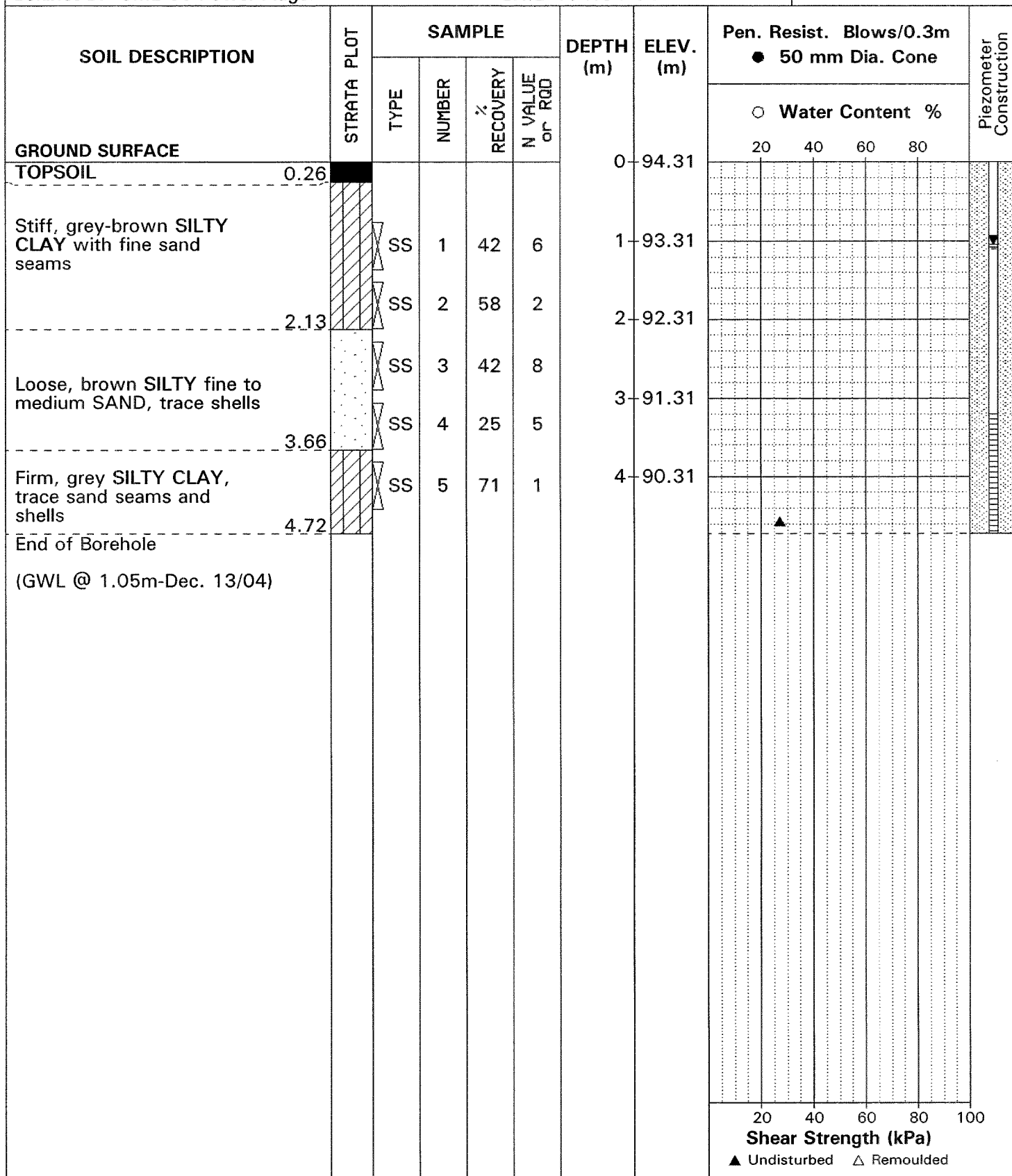
PG0475

HOLE NO.

BH 6

BORINGS BY CME 55 Power Auger

DATE 19 NOV 04



DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic elevation = 95.01m.

REMARKS

FILE NO.

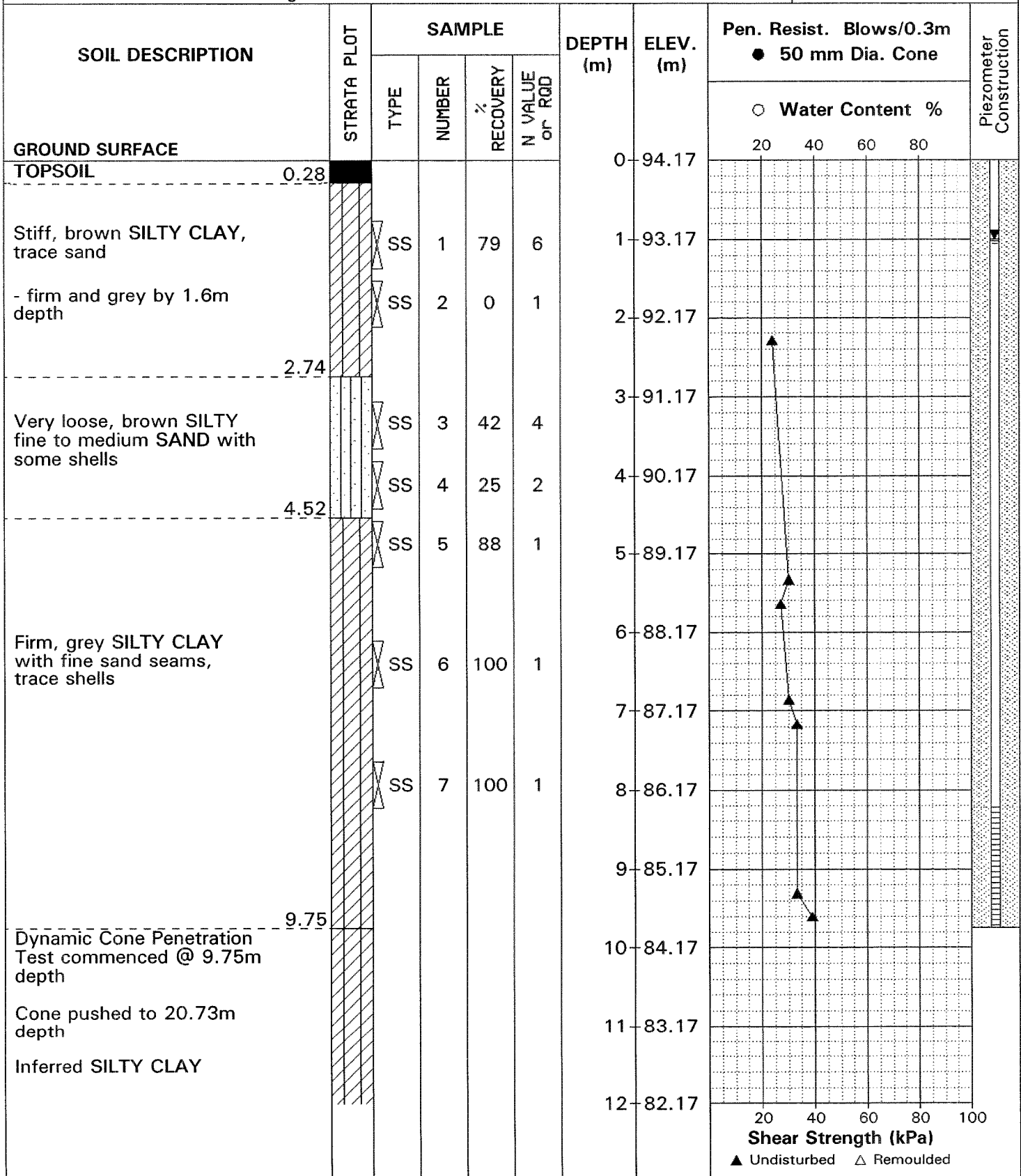
PG0475

HOLE NO.

BH 7

BORINGS BY CME 55 Power Auger

DATE 19 NOV 04



SOIL PROFILE & TEST DATA

**Proposed Commercial Development, Didsbury Road
Ottawa (Kanata), Ontario**

FILE NO.

PG0475

HOLE NO.

BH 7

DATE 19 NOV 04

SOIL DESCRIPTION	STRATA PLOT	SAMPLE				DEPTH (m)	ELEV. (m)	Pen. Resist. Blows/0.3m ● 50 mm Dia. Cone				Piezometer Construction	
		TYPE	NUMBER	% RECOVERY	N VALUE or RQD			○ Water Content %					
								20	40	60	80		
Inferred SILTY CLAY						12	82.17						
						13	81.17						
						14	80.17						
						15	79.17						
						16	78.17						
						17	77.17						
						18	76.17						
						19	75.17						
						20	74.17						
End of Borehole													
DCPT refusal @ 20.73m depth (GWL @ 1.00m-Dec. 13/04)													

20406080100

Shear Strength (kPa)

▲ Undisturbed △ Remoulded

SOIL PROFILE & TEST DATA

Geotechnical Investigation

Proposed Commercial Development, Didsbury Road
Ottawa (Kanata), Ontario

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic
elevation = 95.01m.

REMARKS

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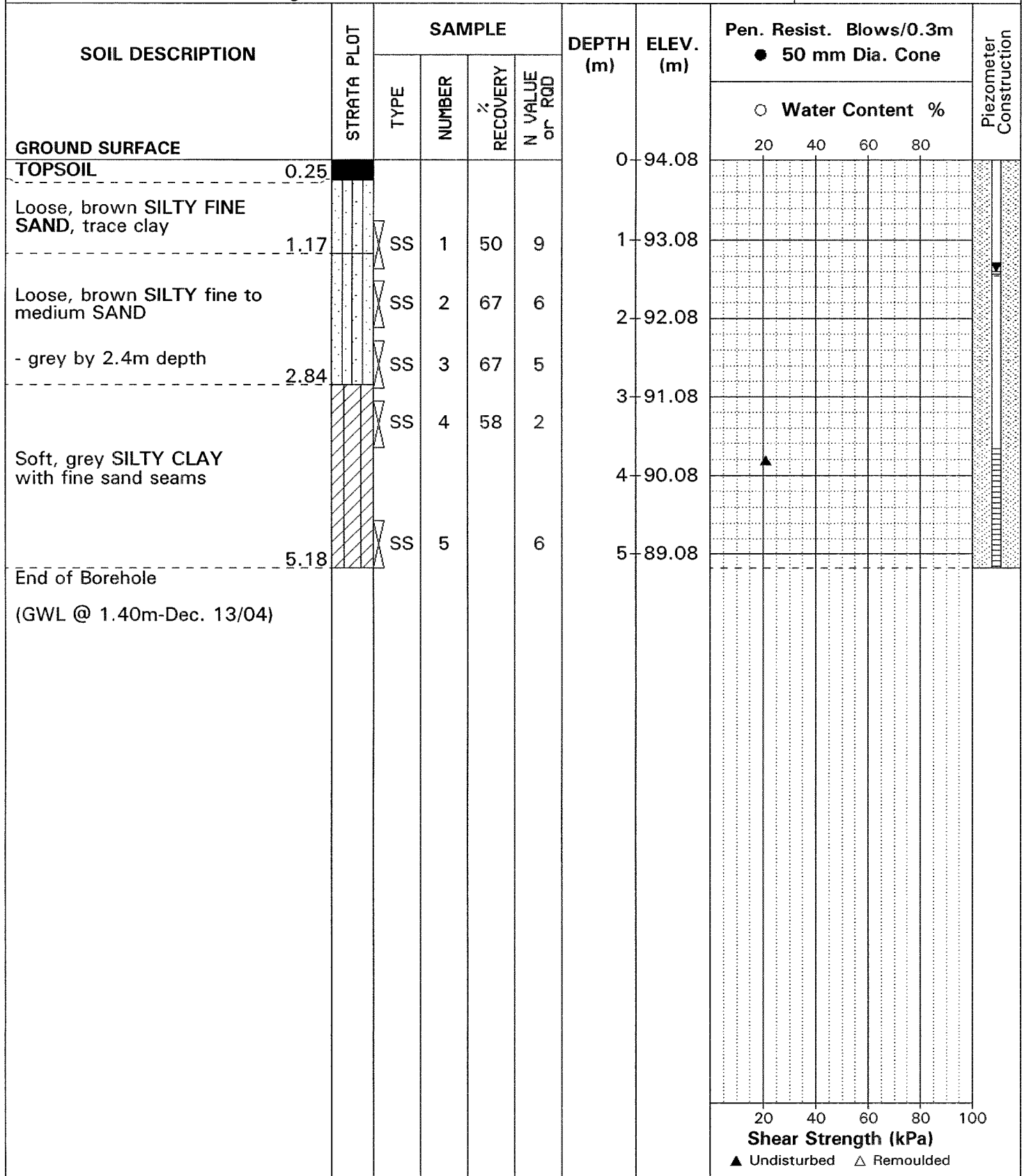
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HOLE NO.

BH 8

BORINGS BY CME 55 Power Auger

DATE 18 NOV 04



SOIL PROFILE & TEST DATA

Geotechnical Investigation

Proposed Commercial Development, Didsbury Road
Ottawa (Kanata), Ontario

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic
elevation = 95.01m.

REMARKS

FILE NO.

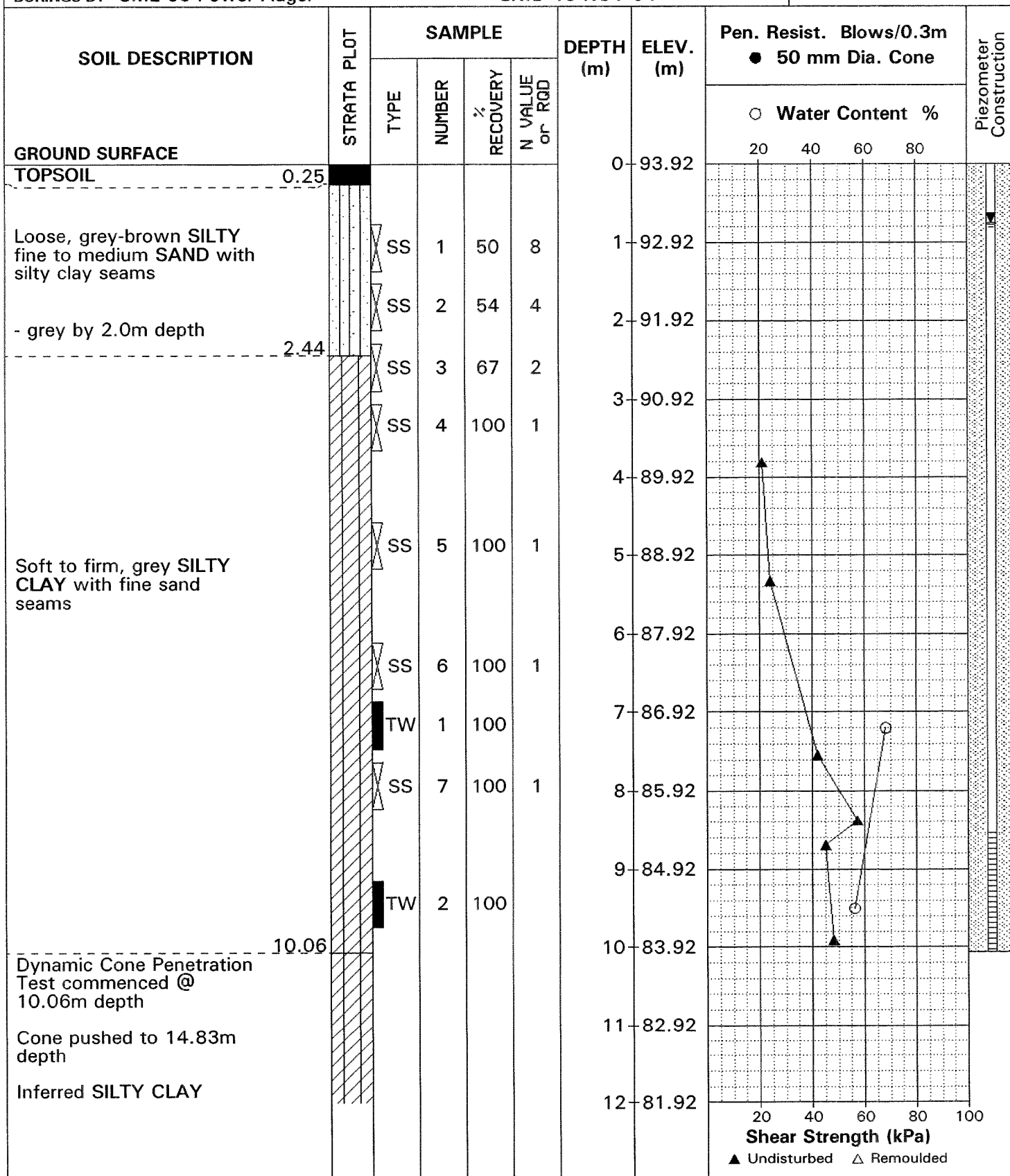
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HOLE NO.

BH 9

BORINGS BY CME 55 Power Auger

DATE 19 NOV 04



DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic elevation = 95.01m.

REMARKS

FILE NO.

PG0475

HOLE NO.

BH 9

BORINGS BY CME 55 Power Auger

DATE 19 NOV 04

SOIL DESCRIPTION	STRATA PLOT	SAMPLE				DEPTH (m)	ELEV. (m)	Pen. Resist. Blows/0.3m ● 50 mm Dia. Cone				Piezometer Construction	
		TYPE	NUMBER	% RECOVERY	N VALUE or RQD			○ Water Content %					
								20	40	60	80		
Inferred SILTY CLAY						12	81.92						
						13	80.92						
						14	79.92						
End of Borehole ----- 14.83													
DCPT refusal @ 14.83m depth (GWL @ 0.75m-Dec. 13/04)													

20406080100

Shear Strength (kPa)

▲ Undisturbed △ Remoulded

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic elevation = 95.01m.

REMARKS

FILE NO.

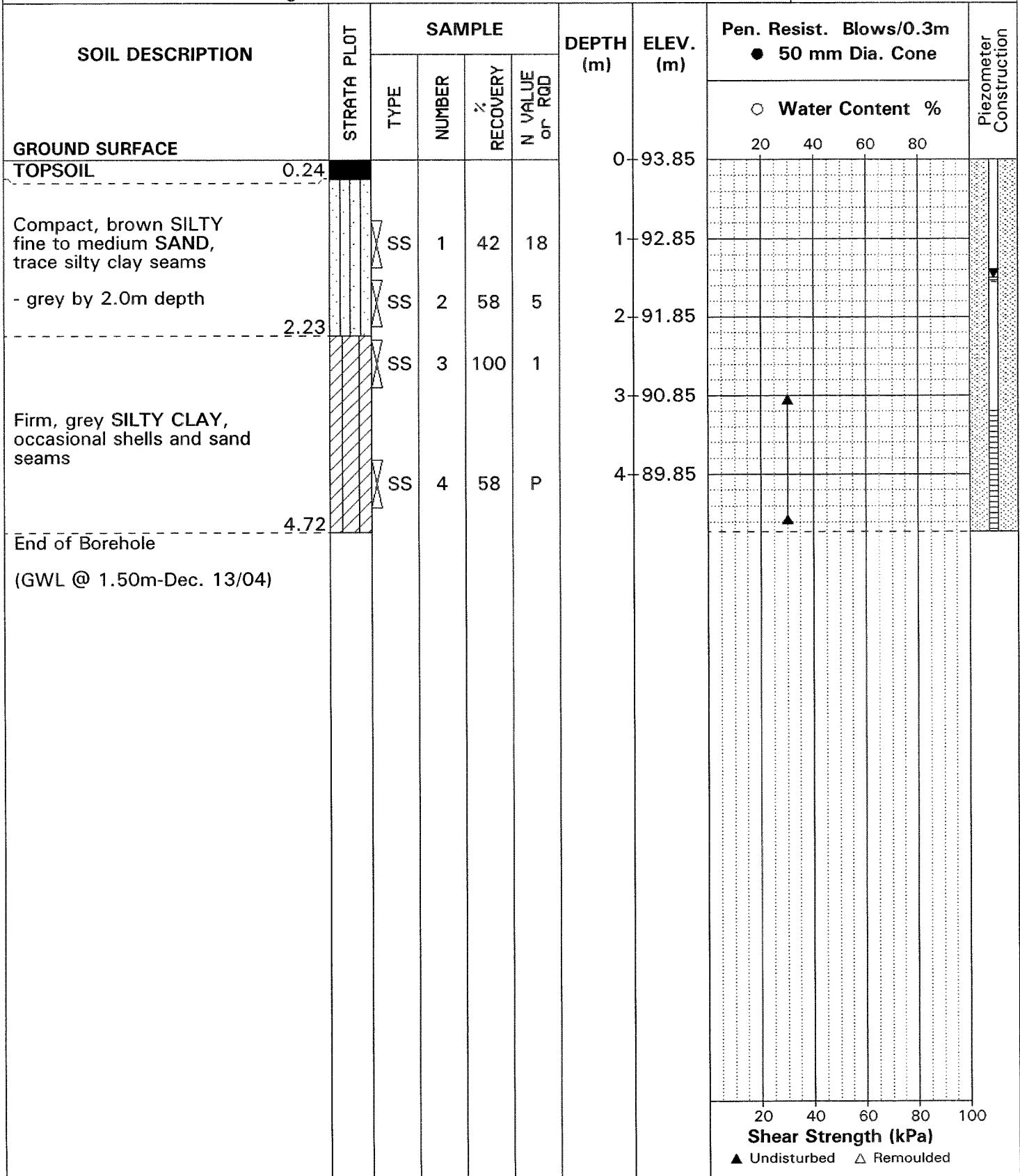
PG0475

HOLE NO.

BH10

BORINGS BY CME 55 Power Auger

DATE 19 NOV 04



SOIL PROFILE & TEST DATA

Geotechnical Investigation

Proposed Commercial Development, Didsbury Road
Ottawa (Kanata), Ontario

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic
elevation = 95.01m.

REMARKS

FILE NO.

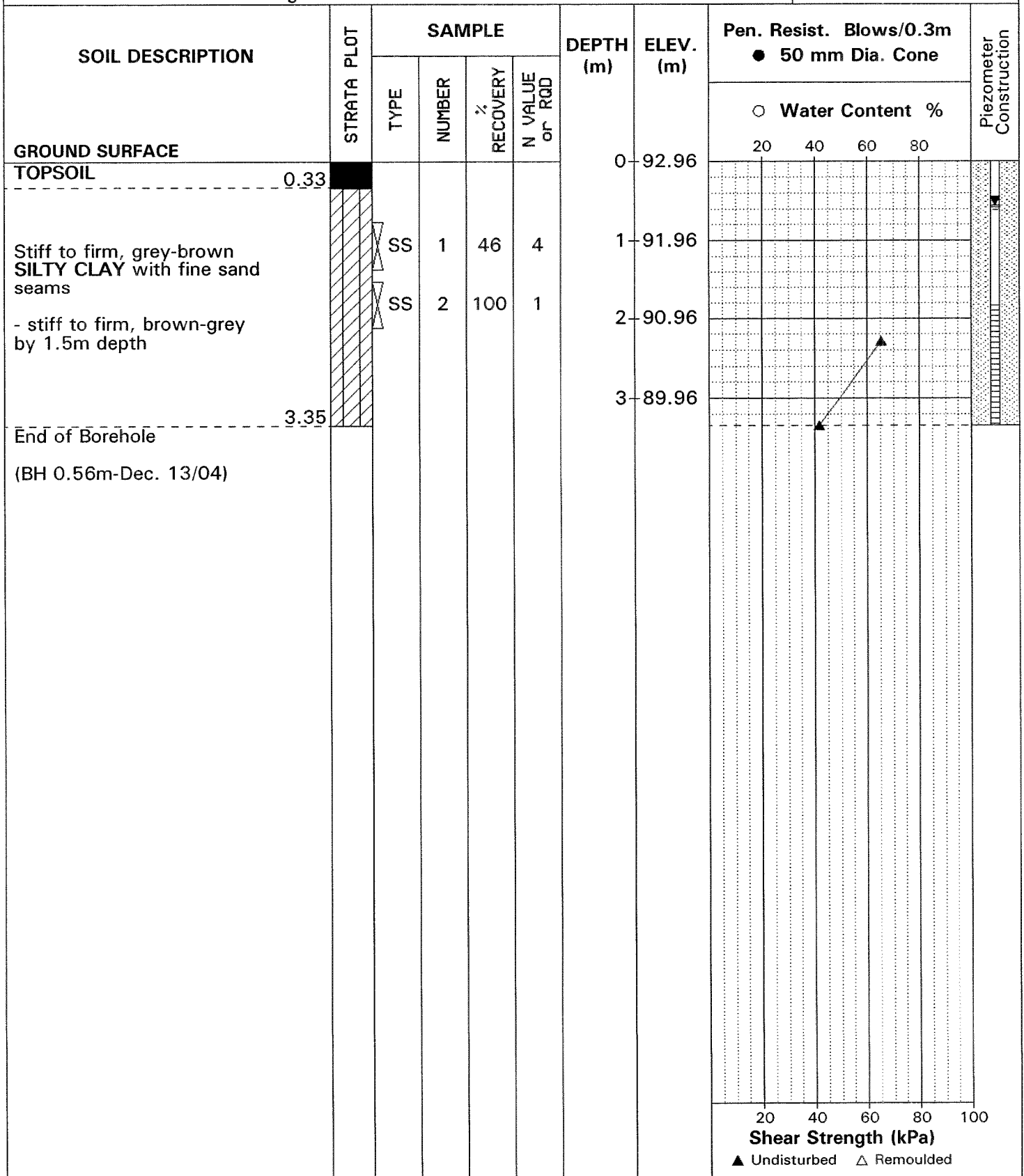
PG0475

HOLE NO.

BH11

BORINGS BY CME 55 Power Auger

DATE 22 NOV 04



SOIL DESCRIPTION	STRATA PLOT	SAMPLE				DEPTH (m)	ELEV. (m)	Pen. Resist. Blows/0.3m ● 50 mm Dia. Cone				Piezometer Construction
		TYPE	NUMBER	% RECOVERY	N VALUE or RQD			○ Water Content % 20 40 60 80				
GROUND SURFACE												
TOPSOIL	0.30					0	93.67					
Stiff, brown SILTY CLAY with fine sand seams		SS	1	29	6	1	92.67					
		SS	2	83	3	2	91.67					
- brown-grey by 1.5m depth												
End of Borehole	3.35					3	90.67					
(BH 2.56m-Dec. 13/04)												

<

SOIL PROFILE & TEST DATA

Geotechnical Investigation

Proposed Commercial Development, Didsbury Road
Ottawa (Kanata), Ontario

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic
elevation = 95.01m.

REMARKS

FILE NO.

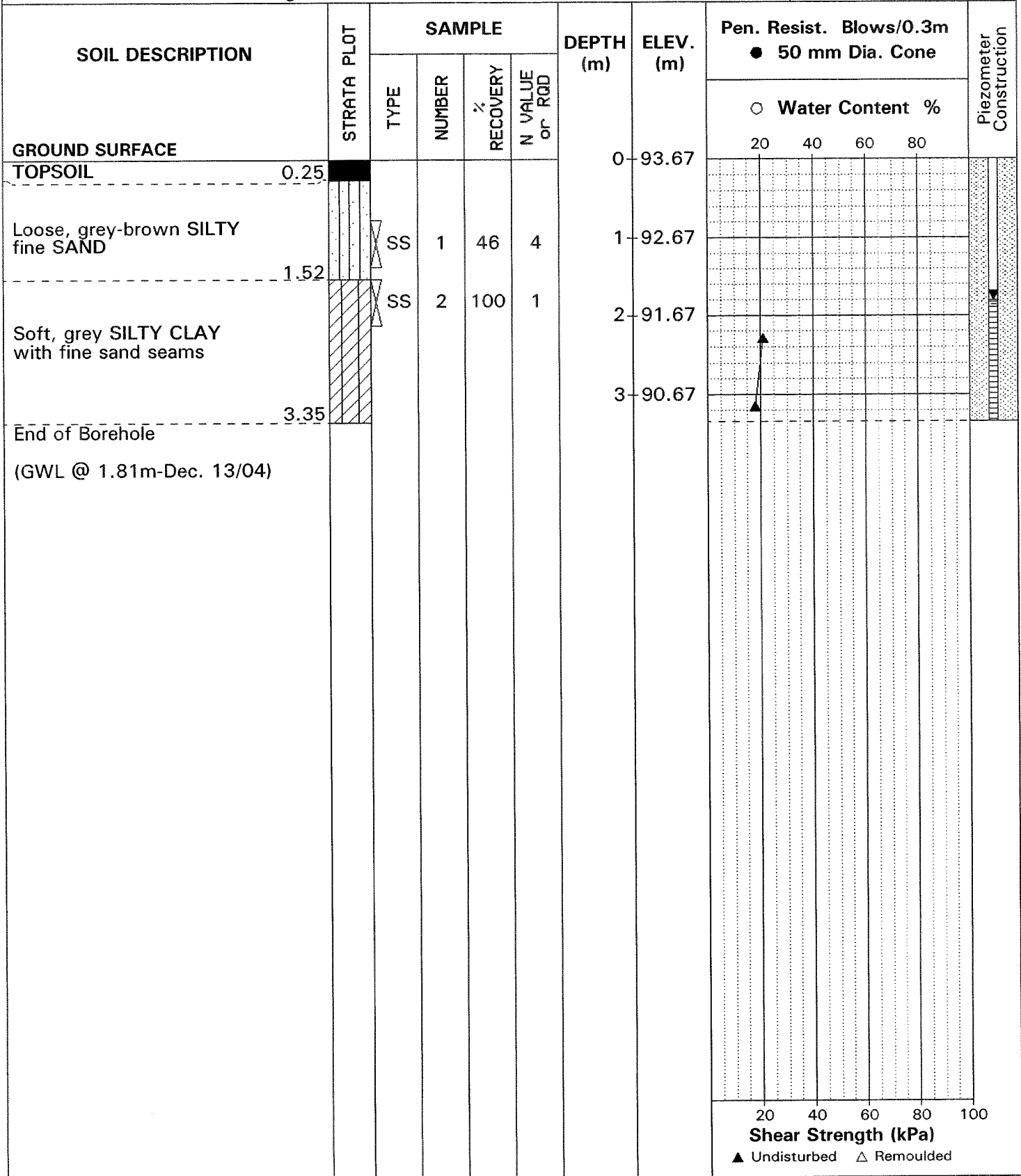
PG0475

HOLE NO.

BH13

BORINGS BY CME 55 Power Auger

DATE 18 NOV 04



DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic elevation = 95.01m.

REMARKS

FILE NO.

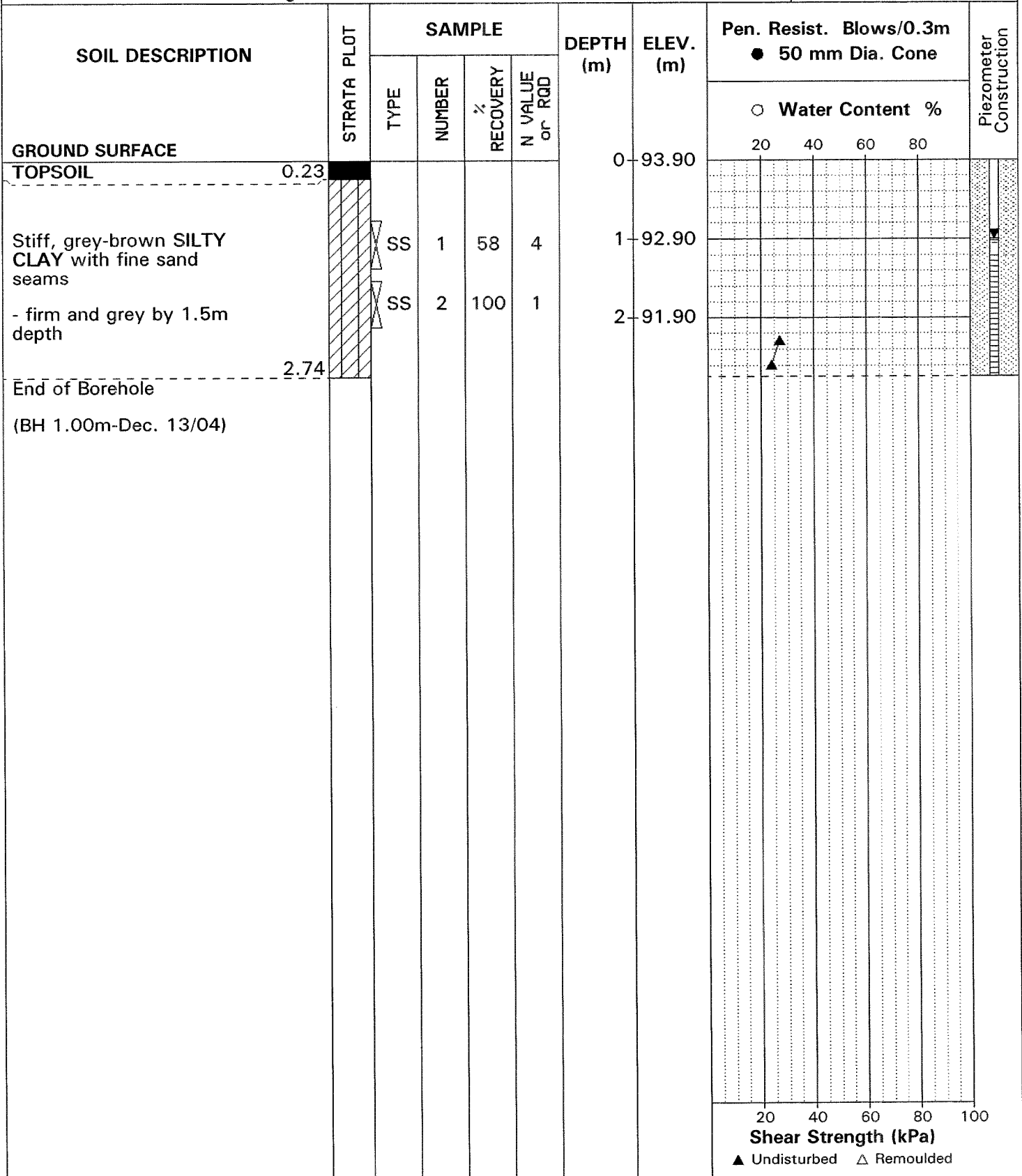
PG0475

HOLE NO.

BH14

BORINGS BY CME 55 Power Auger

DATE 18 NOV 04



SOIL PROFILE & TEST DATA

Geotechnical Investigation

Proposed Commercial Development, Didsbury Road
Ottawa (Kanata), Ontario

DATUM TBM - Top spindle of fire hydrant (see plan). Approximate geodetic
elevation = 95.01m.

REMARKS

FILE NO.

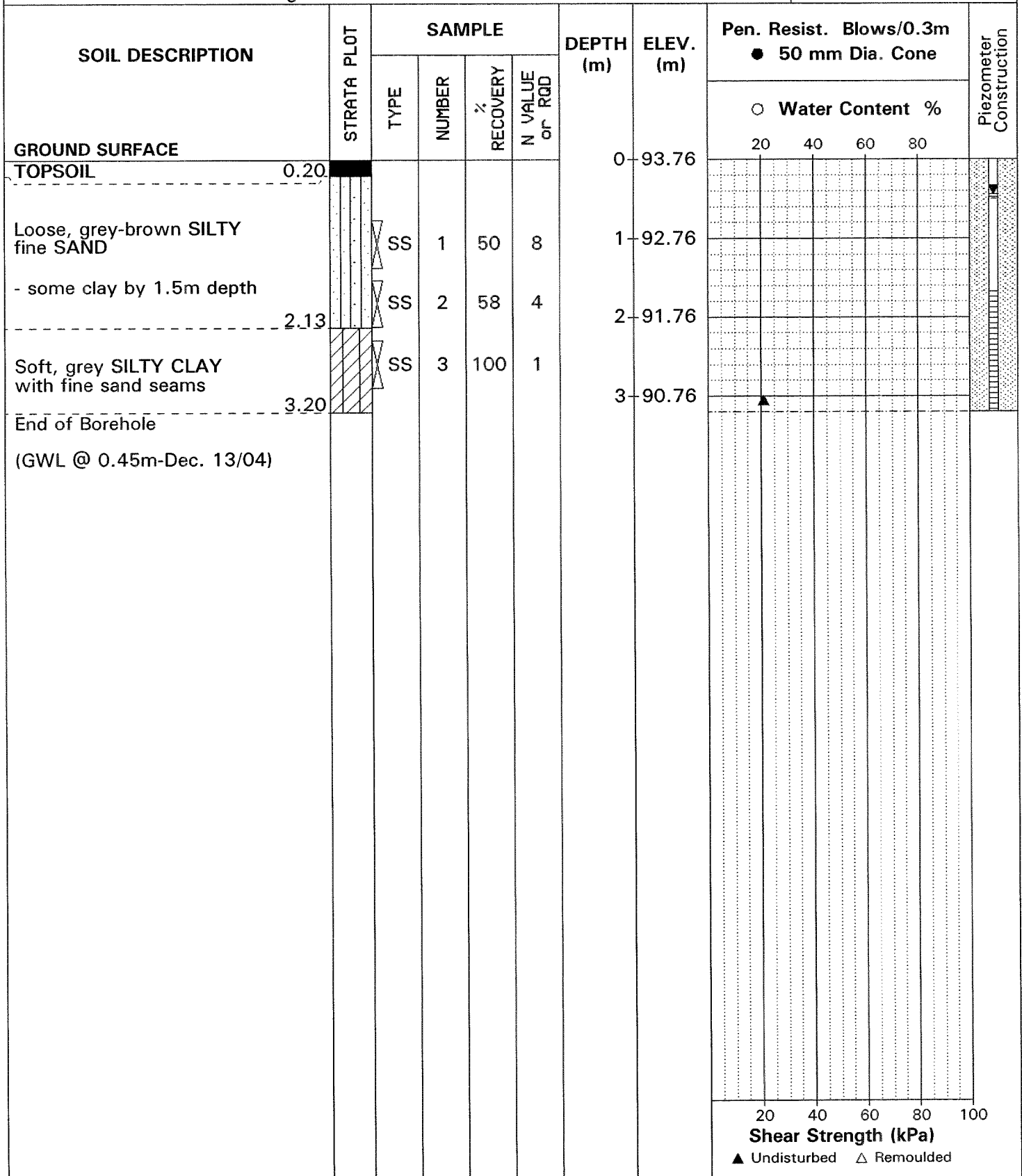
PG0475

HOLE NO.

BH15

BORINGS BY CME 55 Power Auger

DATE 18 NOV 04



ELEVATION: 92.79

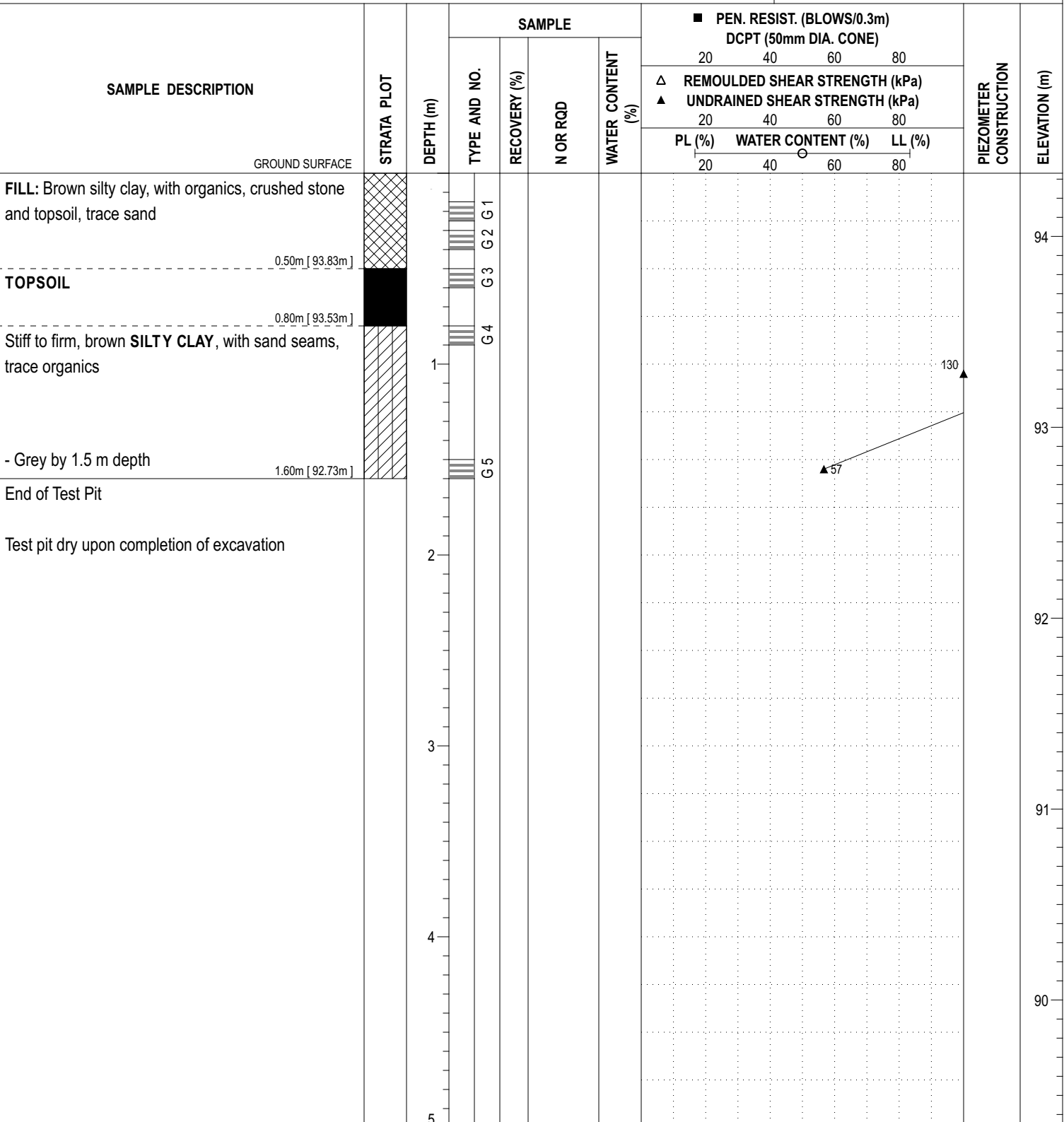
FILE NO. : PG7751

HOLE NO.: TP 1-25

DATE: November 21, 2025



COORD. SYS.: MTM ZONE 9	EASTING: 350228.58	NORTHING: 5018795.34	ELEVATION: 94.33
PROJECT: Proposed Commercial Development			FILE NO. : PG7751
ADVANCED BY: Back Hoe			HOLE NO. : TP 2-25
REMARKS:			DATE: November 21, 2025



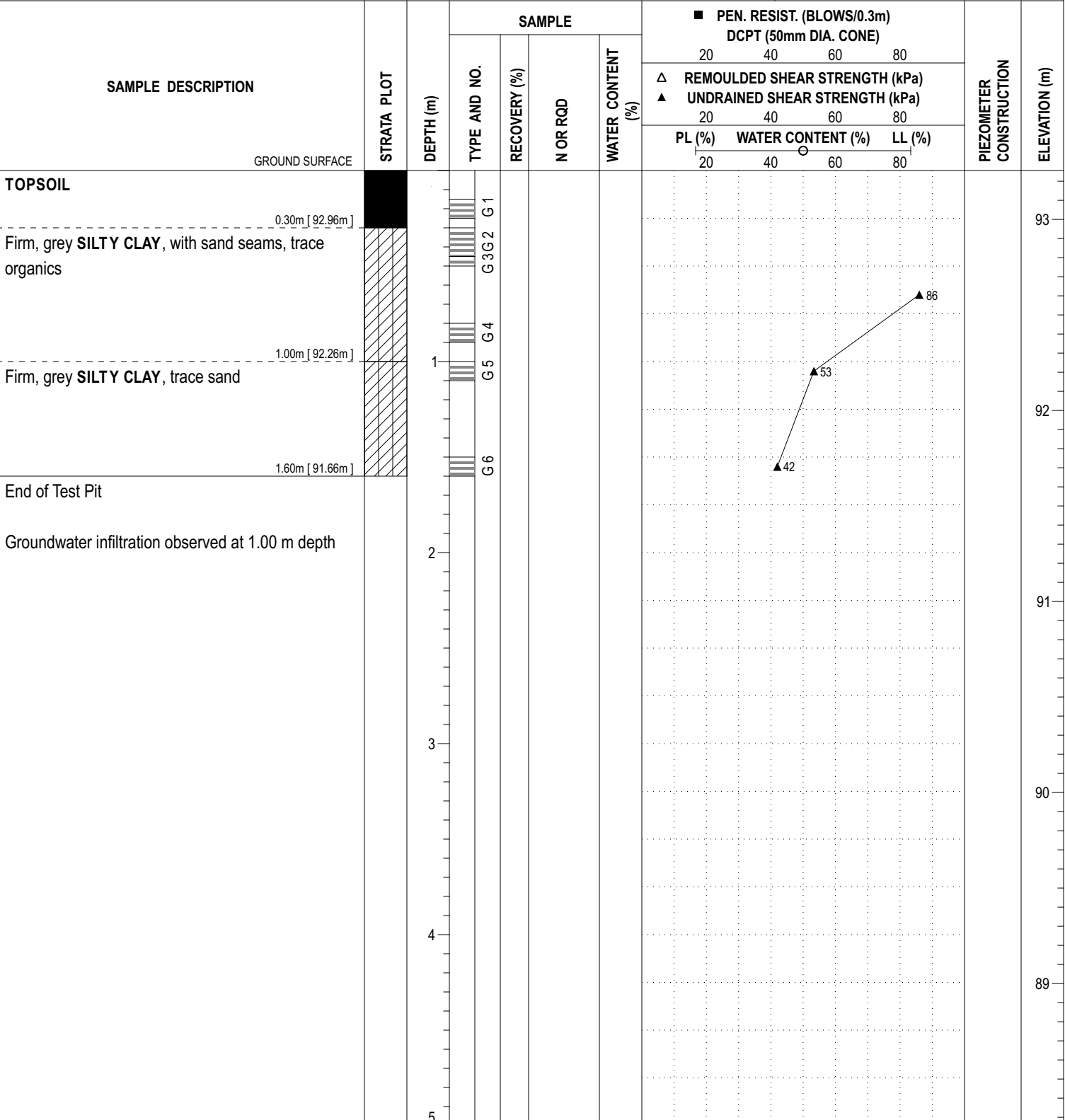
DISCLAIMER: THE DATA PRESENTED IN THIS SHEET IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHOM IT WAS PRODUCED. THIS SHEET SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

COORD. SYS.: MTM ZONE 9	EASTING: 350174.88	NORTHING: 5018820.53	ELEVATION: 93.26
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PROJECT: Proposed Commercial Development	FILE NO. : PG7751
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ADVANCED BY: Back Hoe	HOLE NO. : TP 3-25
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REMARKS:	DATE: November 21, 2025
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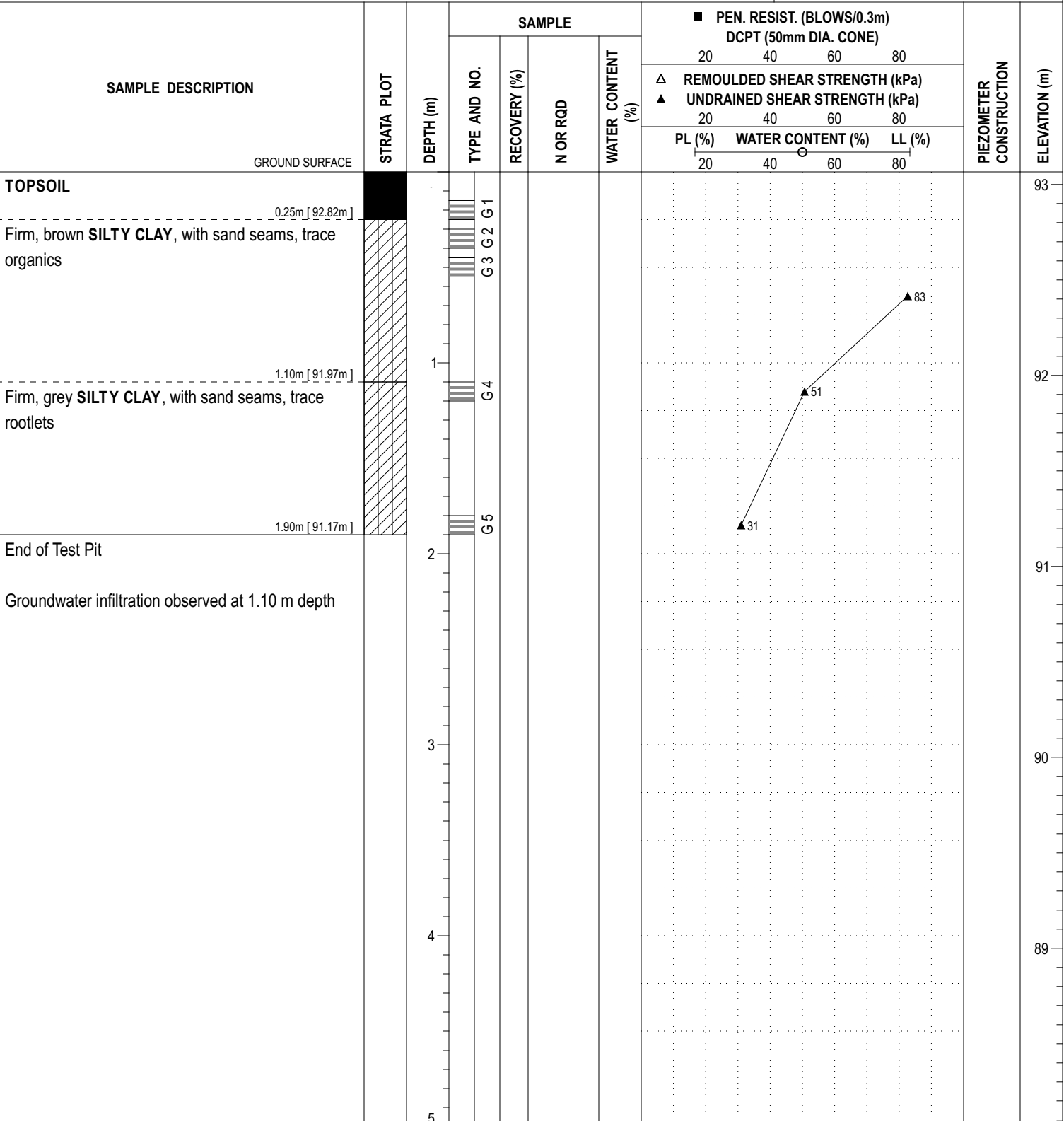
COORD. SYS.: MTM ZONE 9 **EASTING:** 350109.59 **NORTHING:** 5018788.78 **ELEVATION:** 93.07

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

ADVANCED BY: Back Hoe

REMARKS:
DATE: November 21, 2025

HOLE NO. : TP 4-25


DISCLAIMER: THE DATA PRESENTED IN THIS SHEET IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHOM IT WAS PRODUCED. THIS SHEET SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

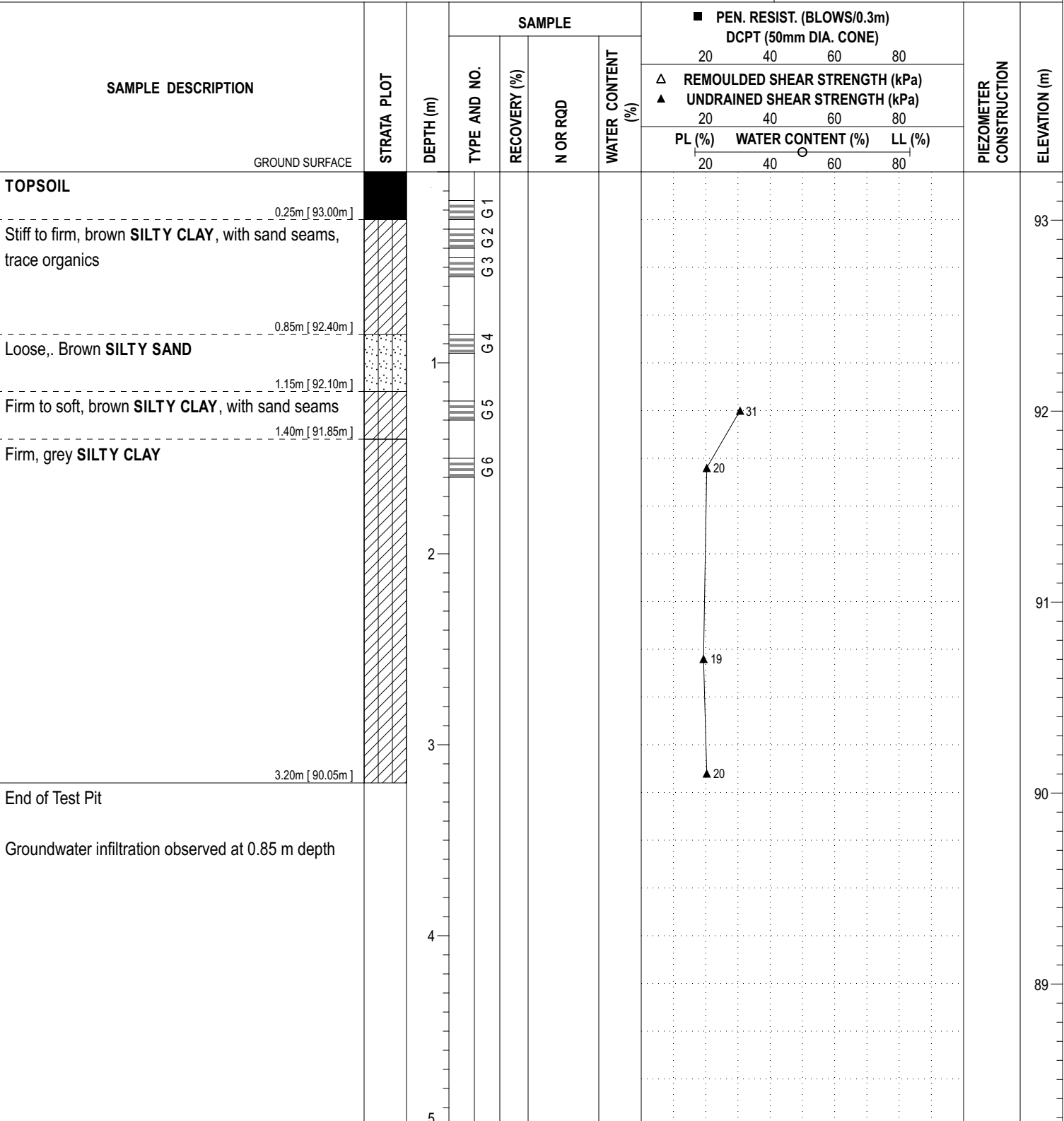
COORD. SYS.: MTM ZONE 9 **EASTING:** 350054.10 **NORTHING:** 5018791.40 **ELEVATION:** 93.25

PROJECT: Proposed Commercial Development

FILE NO. : PG7751

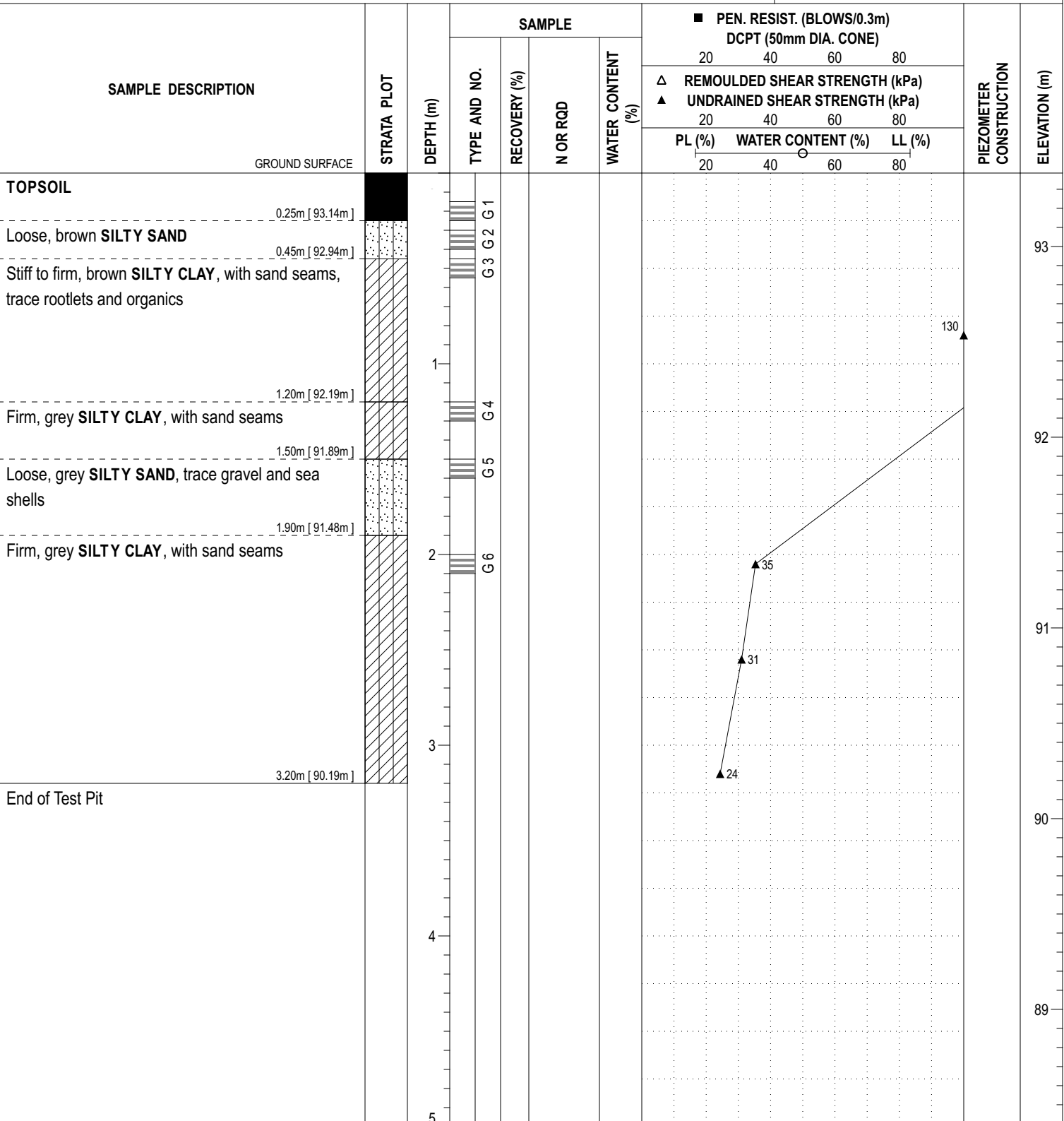
ADVANCED BY: Back Hoe

REMARKS:
DATE: November 21, 2025

HOLE NO. : TP 5-25


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COORD. SYS.: MTM ZONE 9	EASTING: 349969.41	NORTHING: 5018695.58	ELEVATION: 93.39
PROJECT: Proposed Commercial Development			FILE NO. : PG7751
ADVANCED BY: Back Hoe			HOLE NO. : TP 6-25
REMARKS:			DATE: November 21, 2025



DISCLAIMER: THE DATA PRESENTED IN THIS SHEET IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHOM IT WAS PRODUCED. THIS SHEET SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

COORD. SYS.: MTM ZONE 9 EASTING: 350073.41 NORTHING: 5018714.57 ELEVATION: 93.68

PROJECT: Proposed Commercial Development

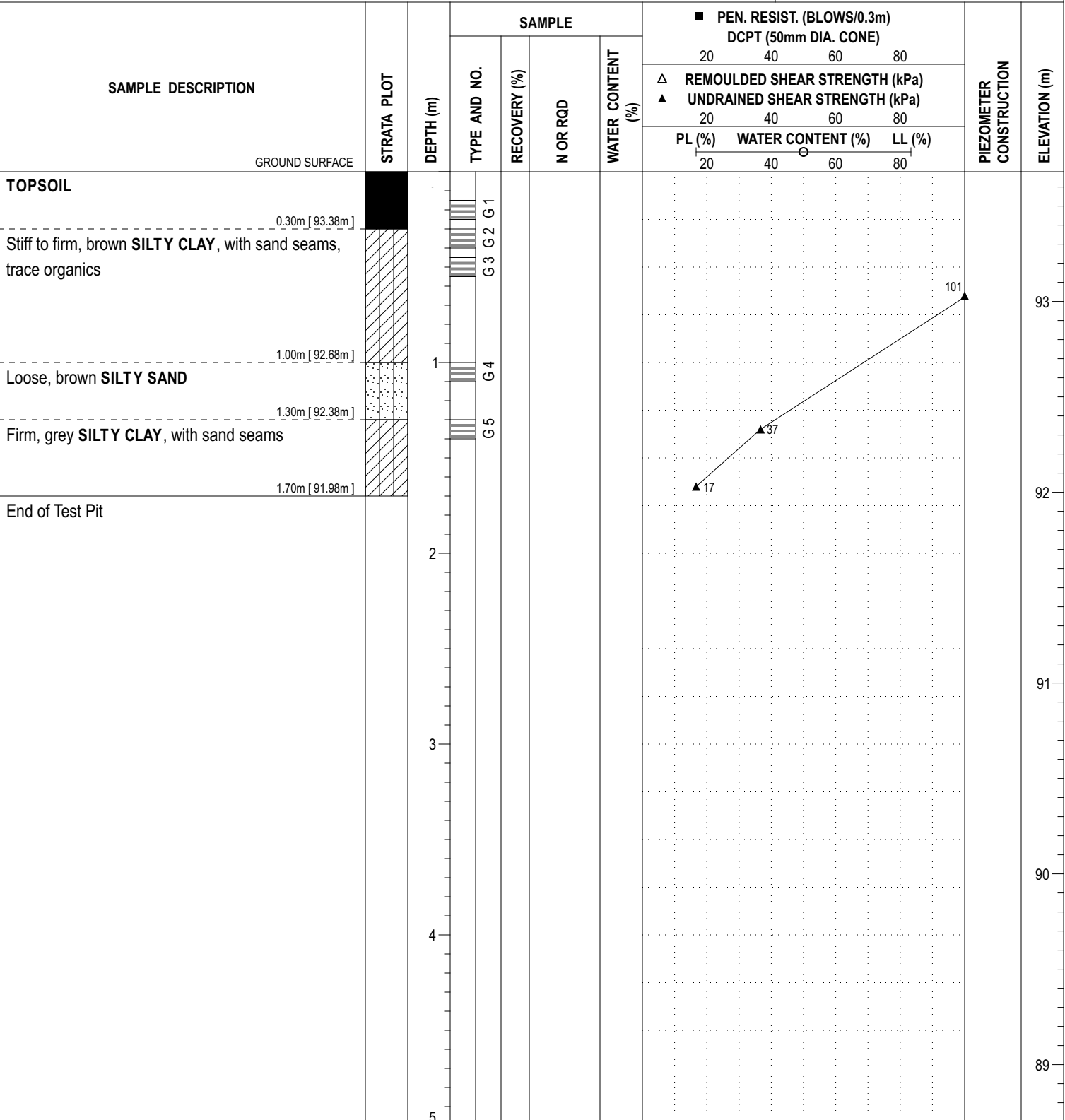
ADVANCED BY: Back Hoe

REMARKS:

DATE: November 21, 2025

FILE NO. : PG7751

HOLE NO. : TP 7-25



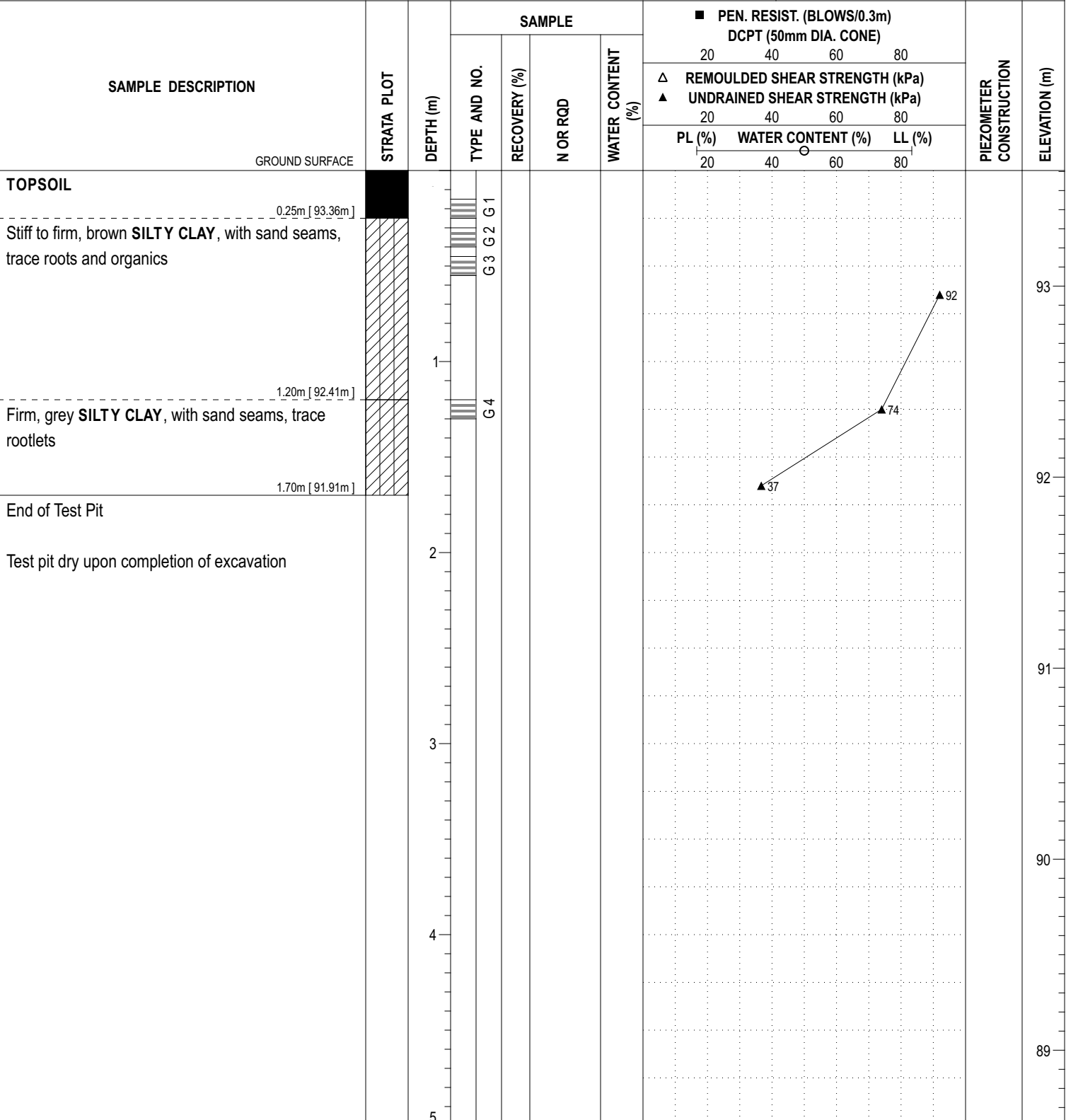
DISCLAIMER: THE DATA PRESENTED IN THIS SHEET IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHOM IT WAS PRODUCED. THIS SHEET SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

COORD. SYS.: MTM ZONE 9	EASTING: 350148.97	NORTHING: 5018751.83	ELEVATION: 93.61
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PROJECT: Proposed Commercial Development	FILE NO. : PG7751
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ADVANCED BY: Back Hoe	HOLE NO. : TP 8-25
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REMARKS:	DATE: November 21, 2025
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ELEVATION: 94.31

FILE NO. : PG7751

REMARKS:

DATE: November 21, 2025

HOLE NO.: TP 9-25

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SYMBOLS AND TERMS

SOIL DESCRIPTION

Behavioural properties, such as structure and strength, take precedence over particle gradation in describing soils. Terminology describing soil structure are as follows:

Desiccated	-	having visible signs of weathering by oxidation of clay minerals, shrinkage cracks, etc.
Fissured	-	having cracks, and hence a blocky structure.
Varved	-	composed of regular alternating layers of silt and clay.
Stratified	-	composed of alternating layers of different soil types, e.g. silt and sand or silt and clay.
Well-Graded	-	Having wide range in grain sizes and substantial amounts of all intermediate particle sizes (see Grain Size Distribution).
Uniformly-Graded	-	Predominantly of one grain size (see Grain Size Distribution).

The standard terminology to describe the strength of cohesionless soils is the relative density, usually inferred from the results of the Standard Penetration Test (SPT) 'N' value. The SPT N value is the number of blows of a 63.5 kg hammer, falling 760 mm, required to drive a 51 mm O.D. split spoon sampler 300 mm into the soil after an initial penetration of 150 mm.

Relative Density	'N' Value	Relative Density %
Very Loose	<4	<15
Loose	4-10	15-35
Compact	10-30	35-65
Dense	30-50	65-85
Very Dense	>50	>85

The standard terminology to describe the strength of cohesive soils is the consistency, which is based on the undisturbed undrained shear strength as measured by the in situ or laboratory vane tests, penetrometer tests, unconfined compression tests, or occasionally by Standard Penetration Tests.

Consistency	Undrained Shear Strength (kPa)	'N' Value
Very Soft	<12	<2
Soft	12-25	2-4
Firm	25-50	4-8
Stiff	50-100	8-15
Very Stiff	100-200	15-30
Hard	>200	>30

SYMBOLS AND TERMS (continued)

SOIL DESCRIPTION (continued)

Cohesive soils can also be classified according to their “sensitivity”. The sensitivity is the ratio between the undisturbed undrained shear strength and the remoulded undrained shear strength of the soil.

Terminology used for describing soil strata based upon texture, or the proportion of individual particle sizes present is provided on the Textural Soil Classification Chart at the end of this information package.

ROCK DESCRIPTION

The structural description of the bedrock mass is based on the Rock Quality Designation (RQD).

The RQD classification is based on a modified core recovery percentage in which all pieces of sound core over 100 mm long are counted as recovery. The smaller pieces are considered to be a result of closely-spaced discontinuities (resulting from shearing, jointing, faulting, or weathering) in the rock mass and are not counted. RQD is ideally determined from NXL size core. However, it can be used on smaller core sizes, such as BX, if the bulk of the fractures caused by drilling stresses (called “mechanical breaks”) are easily distinguishable from the normal in situ fractures.

RQD %	ROCK QUALITY
90-100	Excellent, intact, very sound
75-90	Good, massive, moderately jointed or sound
50-75	Fair, blocky and seamy, fractured
25-50	Poor, shattered and very seamy or blocky, severely fractured
0-25	Very poor, crushed, very severely fractured

SAMPLE TYPES

SS	-	Split spoon sample (obtained in conjunction with the performing of the Standard Penetration Test (SPT))
TW	-	Thin wall tube or Shelby tube
PS	-	Piston sample
AU	-	Auger sample or bulk sample
WS	-	Wash sample
RC	-	Rock core sample (Core bit size AXT, BXL, etc.). Rock core samples are obtained with the use of standard diamond drilling bits.

SYMBOLS AND TERMS (continued)

GRAIN SIZE DISTRIBUTION

MC%	-	Natural moisture content or water content of sample, %
LL	-	Liquid Limit, % (water content above which soil behaves as a liquid)
PL	-	Plastic limit, % (water content above which soil behaves plastically)
PI	-	Plasticity index, % (difference between LL and PL)
Dxx	-	Grain size which xx% of the soil, by weight, is of finer grain sizes These grain size descriptions are not used below 0.075 mm grain size
D10	-	Grain size at which 10% of the soil is finer (effective grain size)
D60	-	Grain size at which 60% of the soil is finer
Cc	-	Concavity coefficient = $(D_{30})^2 / (D_{10} \times D_{60})$
Cu	-	Uniformity coefficient = D_{60} / D_{10}

Cc and Cu are used to assess the grading of sands and gravels:

Well-graded gravels have: $1 < Cc < 3$ and $Cu > 4$

Well-graded sands have: $1 < Cc < 3$ and $Cu > 6$

Sands and gravels not meeting the above requirements are poorly-graded or uniformly-graded.

Cc and Cu are not applicable for the description of soils with more than 10% silt and clay
(more than 10% finer than 0.075 mm or the #200 sieve)

CONSOLIDATION TEST

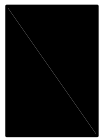
p'_o	-	Present effective overburden pressure at sample depth
p'_c	-	Preconsolidation pressure of (maximum past pressure on) sample
Ccr	-	Recompression index (in effect at pressures below p'_c)
Cc	-	Compression index (in effect at pressures above p'_c)
OC Ratio		Overconsolidation ratio = p'_c / p'_o
Void Ratio		Initial sample void ratio = volume of voids / volume of solids
Wo	-	Initial water content (at start of consolidation test)

PERMEABILITY TEST

k	-	Coefficient of permeability or hydraulic conductivity is a measure of the ability of water to flow through the sample. The value of k is measured at a specified unit weight for (remoulded) cohesionless soil samples, because its value will vary with the unit weight or density of the sample during the test.
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SYMBOLS AND TERMS (continued)

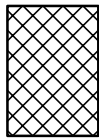
STRATA PLOT



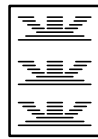
Topsoil



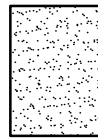
Asphalt



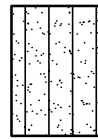
Fill



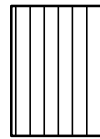
Peat



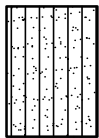
Sand



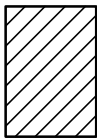
Silty Sand



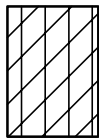
Silt



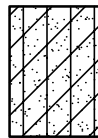
Sandy Silt



Clay



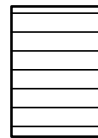
Silty Clay



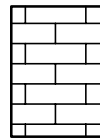
Clayey Silty Sand



Glacial Till



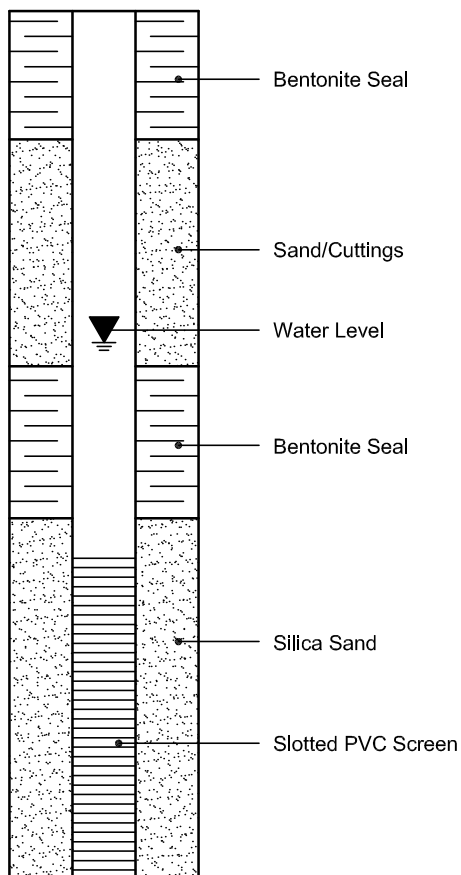
Shale



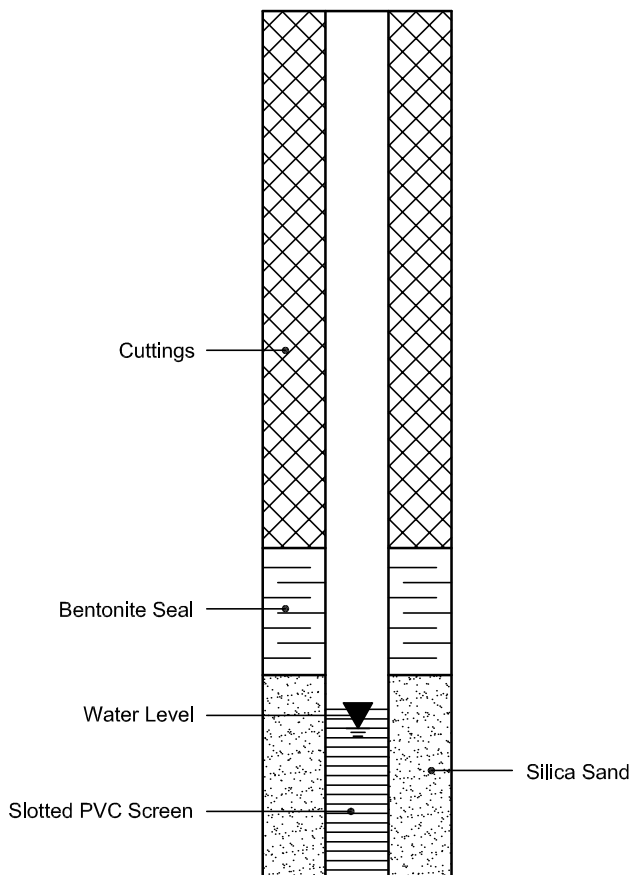
Bedrock

MONITORING WELL AND PIEZOMETER CONSTRUCTION

MONITORING WELL CONSTRUCTION

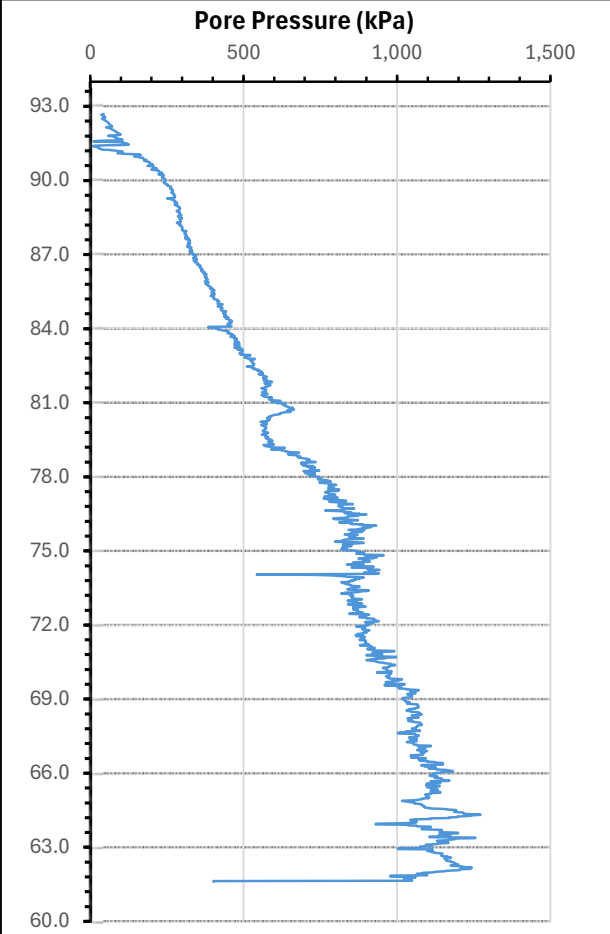
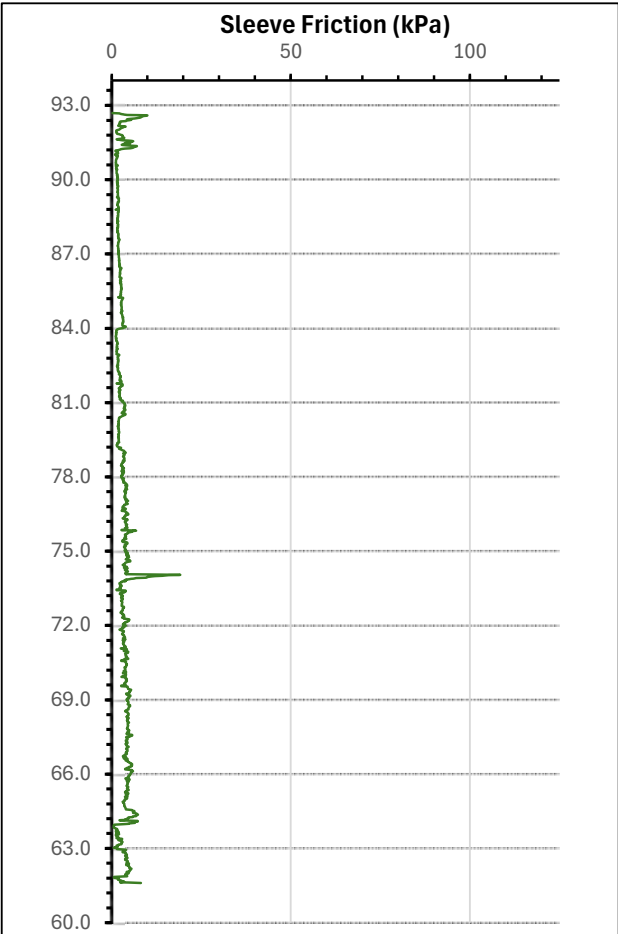
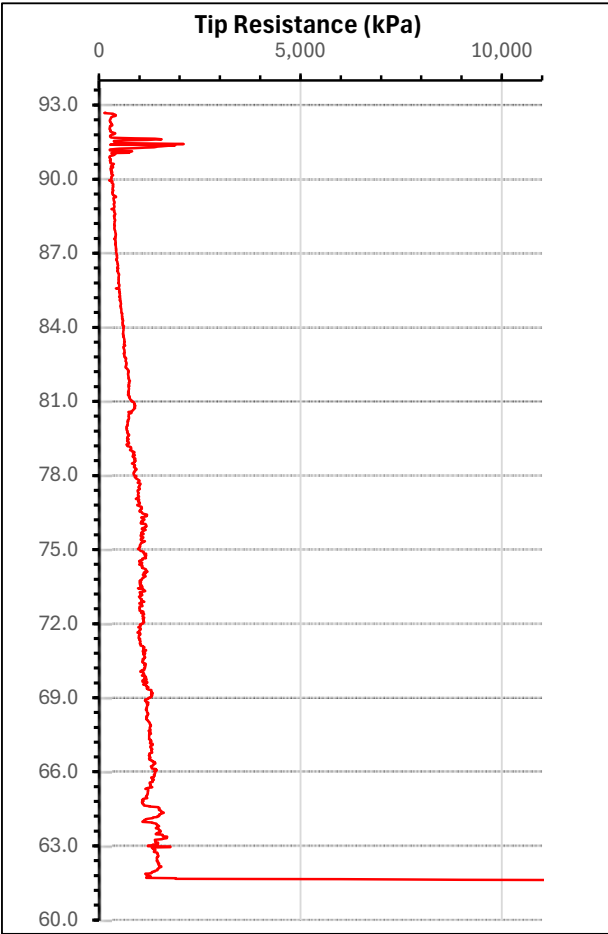


PIEZOMETER CONSTRUCTION



Paterson File: PG7751
Client: FCRI Properties LP
Project: Proposed Commercial Development
Address: 375 Didsbury Road, Ottawa, Ontario

Test Hole ID: CPT 1-26
Ground Surface Elevation (m): 94.09
Investigation Date: 18-Feb-26
Test Hole Depth (m): 32.48

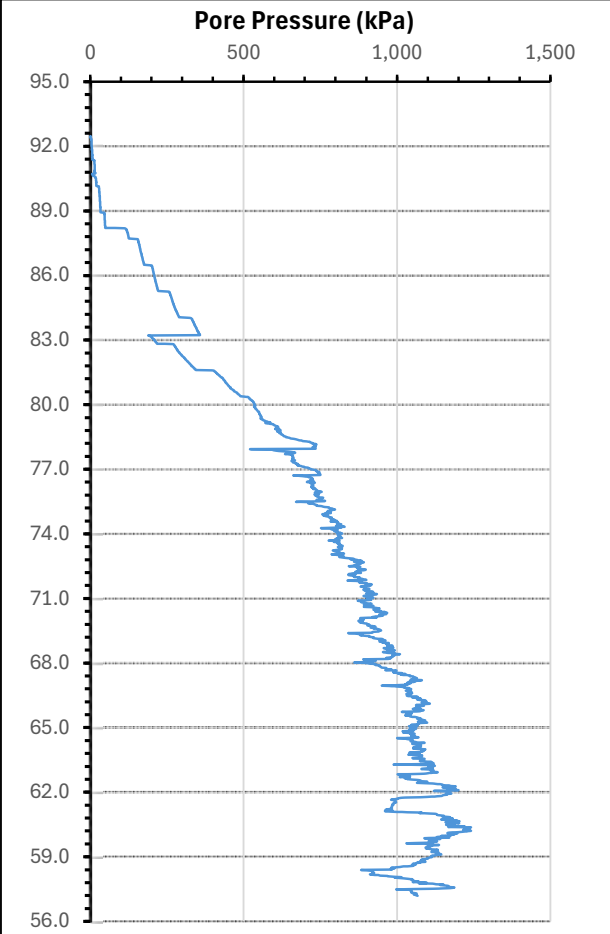
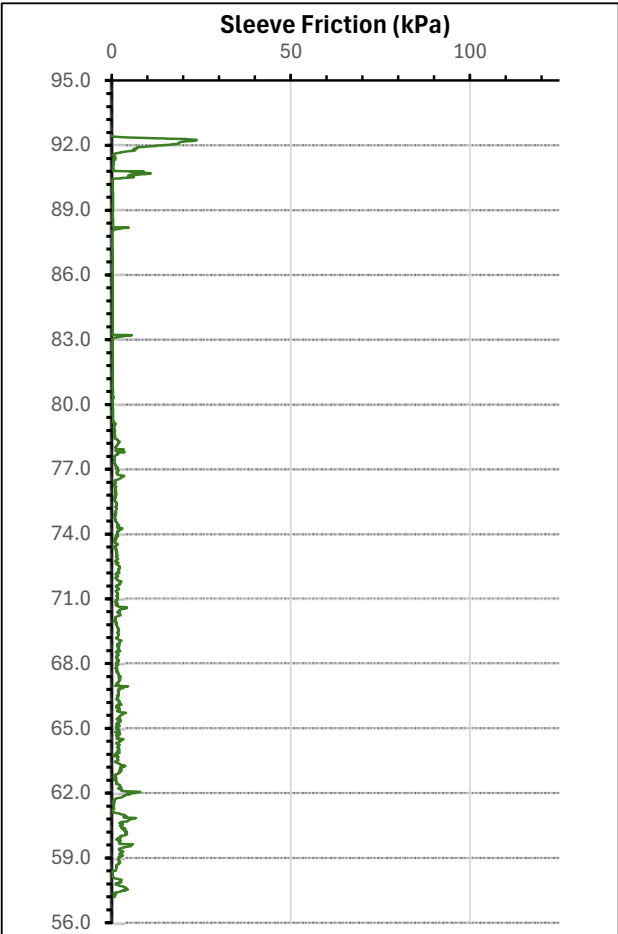
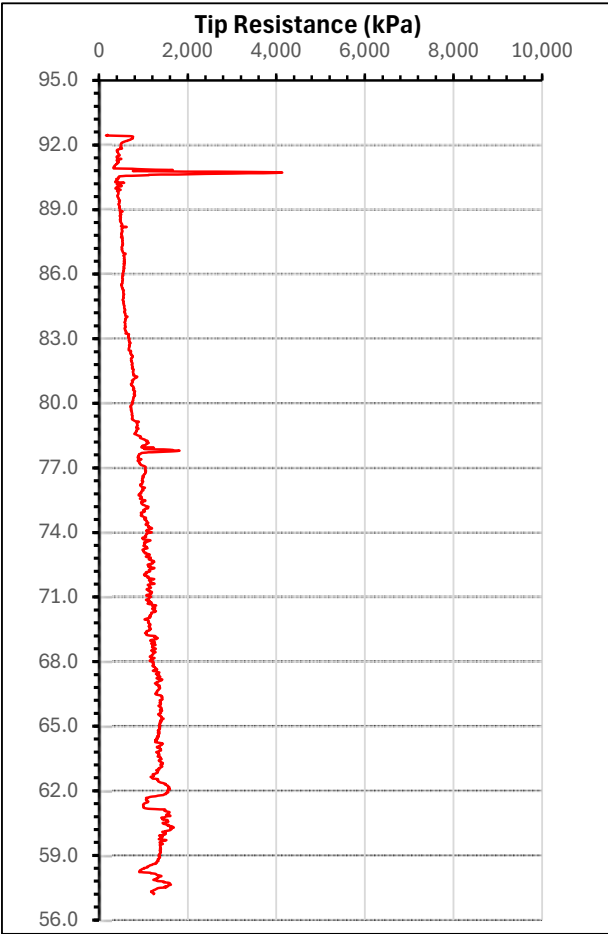


NOTES: TEST HOLE TERMINATED AT DEPTH OF 32.48 m (ELEV. = 61.61 m) BELOW GROUND SURFACE. THE UPPER 1.4 m WERE AUGERED OUT PRIOR TO ADVANCEMENT OF THE CPT.

DISCLAIMER: THE DATA PRESENTED IN THIS LOG IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHO IT WAS PRODUCED. THIS LOG SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

Paterson File: PG7751
Client: FCRI Properties LP
Project: Proposed Commercial Development
Address: 375 Didsbury Road, Ottawa, Ontario

Test Hole ID: CPT 2-26
Ground Surface Elevation (m): 93.25
Investigation Date: 05-Mar-26
Test Hole Depth (m): 36.06

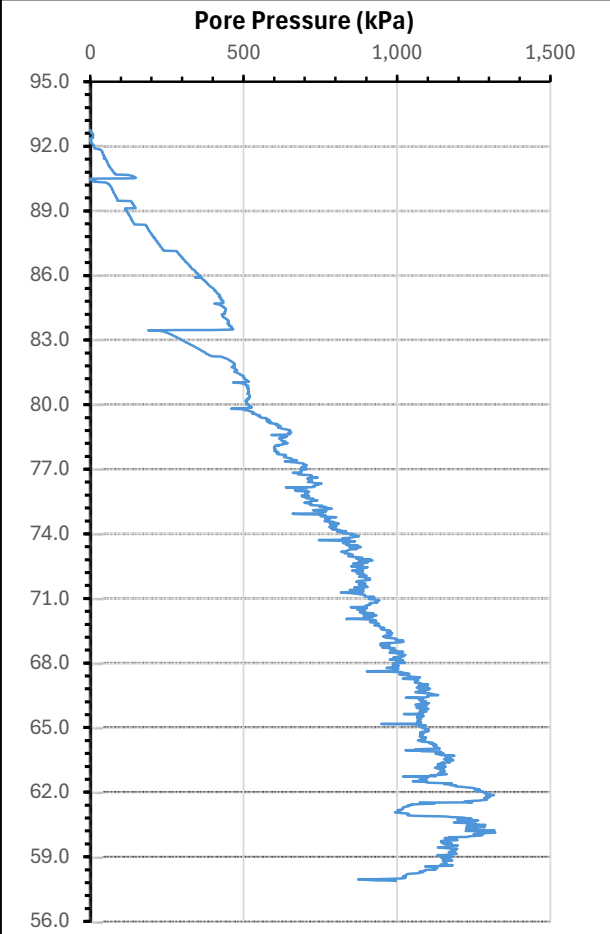
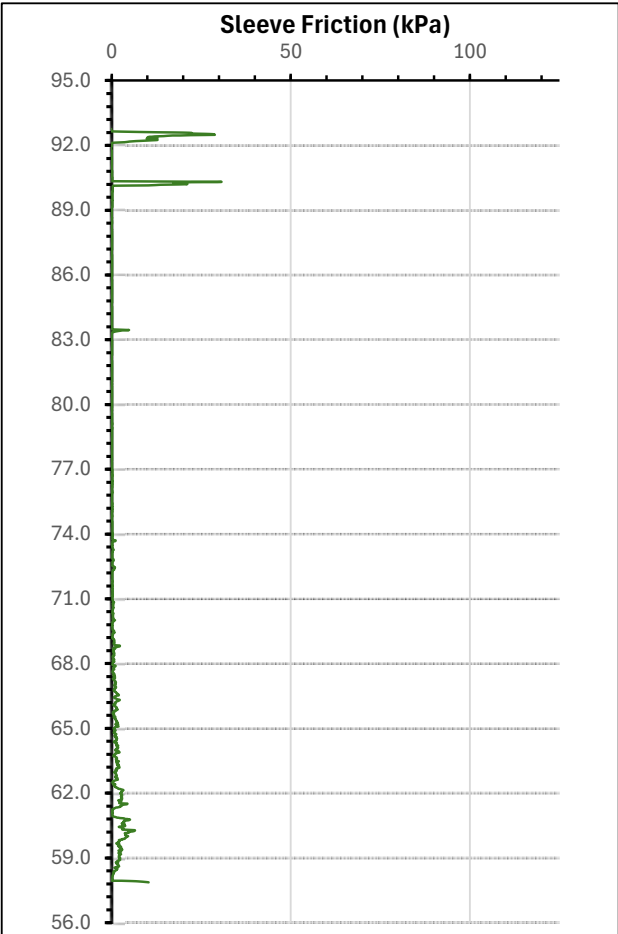
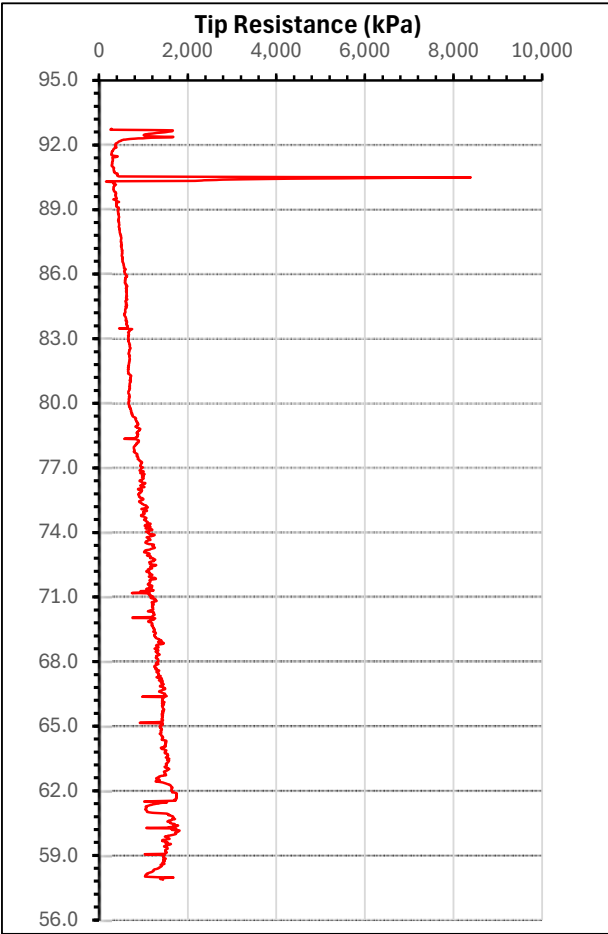


NOTES: TEST HOLE TERMINATED AT DEPTH OF 36.06 m (ELEV. = 57.19 m) BELOW GROUND SURFACE. THE UPPER 0.78 m WERE AUGERED OUT PRIOR TO ADVANCEMENT OF THE CPT.

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Paterson File: PG7751
Client: FCRI Properties LP
Project: Proposed Commercial Development
Address: 375 Didsbury Road, Ottawa, Ontario

Test Hole ID: CPT 3-26
Ground Surface Elevation (m): 93.65
Investigation Date: 06-Mar-26
Test Hole Depth (m): 35.78

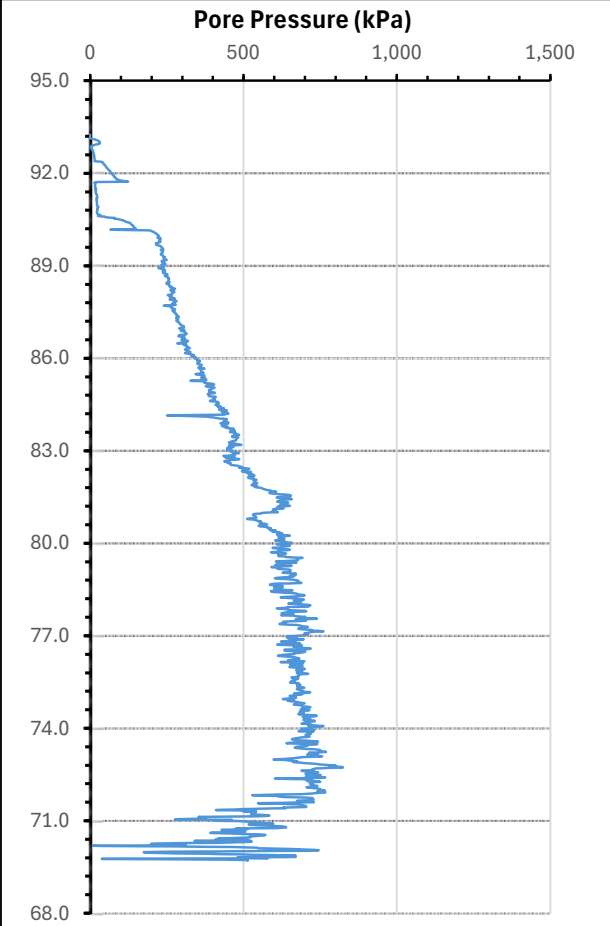
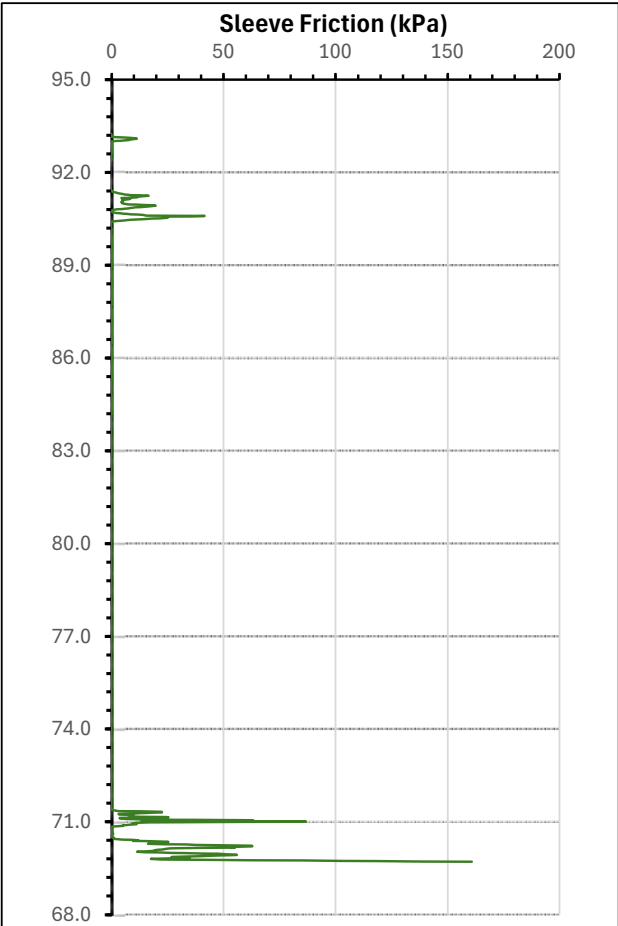
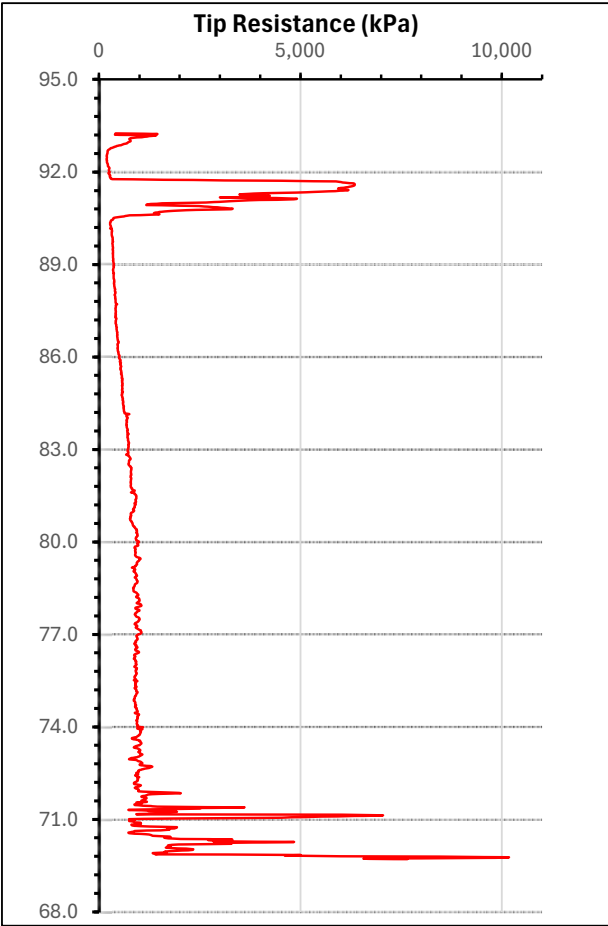


NOTES: TEST HOLE TERMINATED AT DEPTH OF 35.78 m (ELEV. = 57.87 m) BELOW GROUND SURFACE. THE UPPER 0.9 m WERE AUGERED OUT PRIOR TO ADVANCEMENT OF THE CPT.

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Paterson File: PG7751
Client: FCRI Properties LP
Project: Proposed Commercial Development
Address 375 Didsbury Road, Ottawa, Ontario

Test Hole ID: CPT 4-26
Ground Surface Elevation (m): 94.19
Investigation Date: 09-Mar-26
Test Hole Depth (m): 24.48

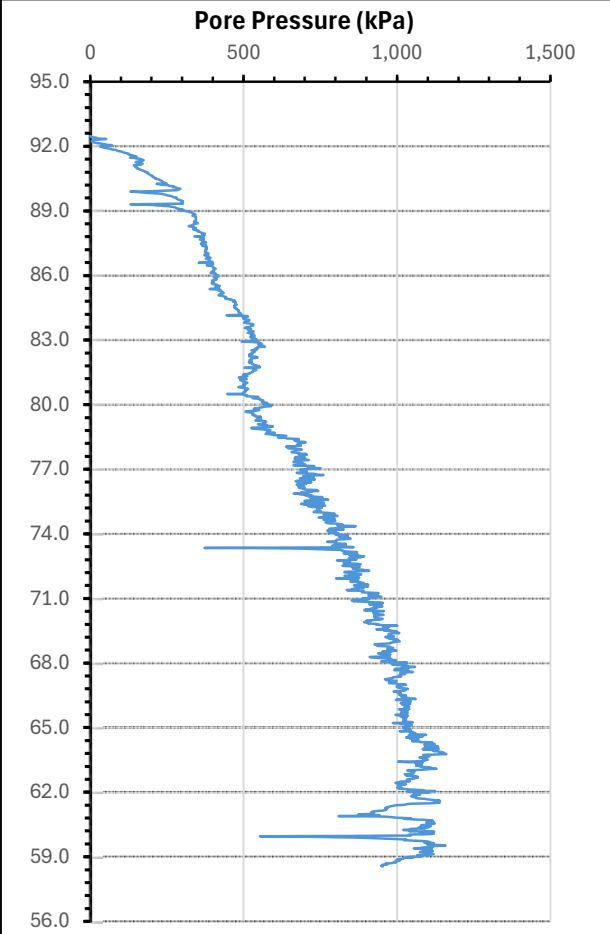
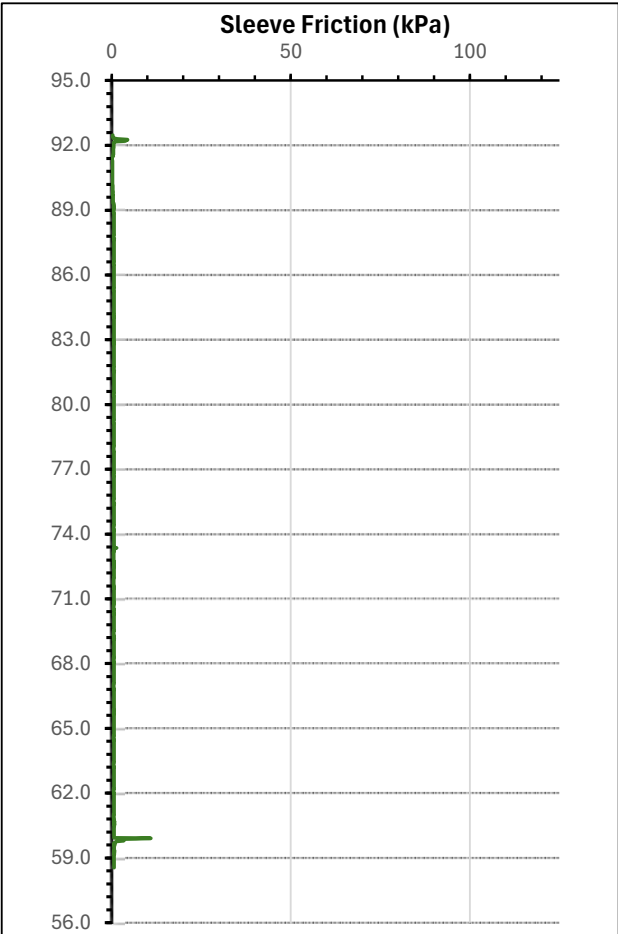
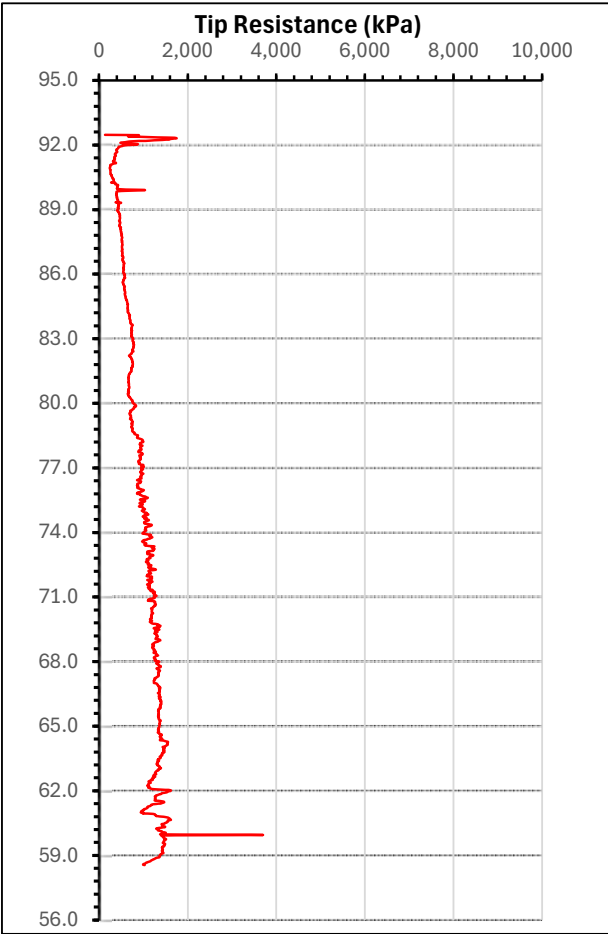


NOTES: TEST HOLE TERMINATED AT DEPTH OF 24.48 m (ELEV. = 69.71 m) BELOW GROUND SURFACE AND AT PRACTICAL REFUSAL TO CPT ADVANCEMENT. THE UPPER 0.94 m WERE AUGERED OUT PRIOR TO ADVANCEMENT OF THE CPT.

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Paterson File: PG7751
Client: FCRI Properties LP
Project: Proposed Commercial Development
Address: 375 Didsbury Road, Ottawa, Ontario

Test Hole ID: CPT 5-26
Ground Surface Elevation (m): 93.37
Investigation Date: 09-Mar-26
Test Hole Depth (m): 34.82

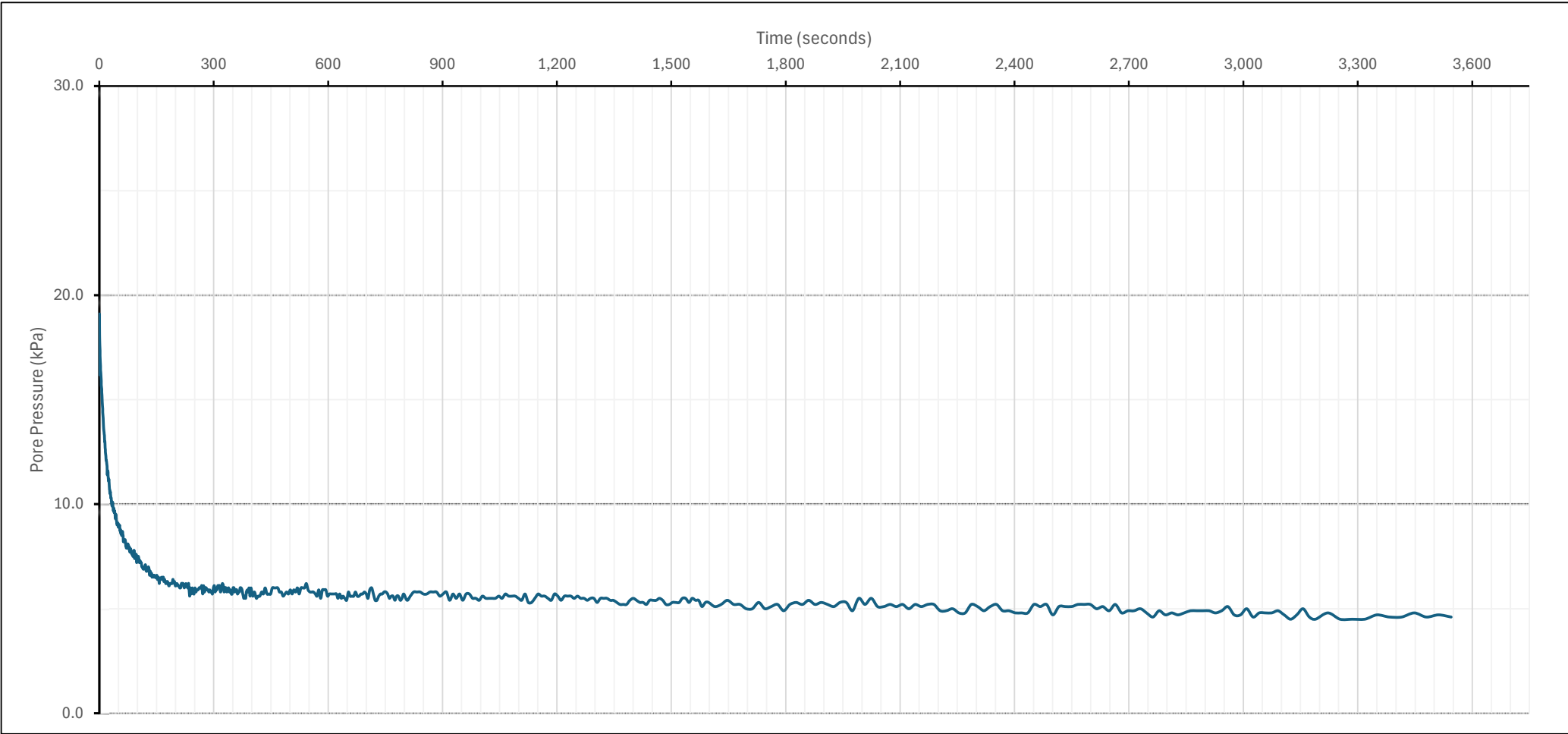


NOTES: TEST HOLE TERMINATED AT DEPTH OF 34.82 m (ELEV. = 58.55 m) BELOW GROUND SURFACE. THE UPPER 0.9 m WERE AUGERED OUT PRIOR TO ADVANCEMENT OF THE CPT.

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Paterson File: PG7751
Client: FCRI Properties LP
Project: Proposed Commercial Development
Address 375 Didsbury Road, Ottawa, Ontario

Test Hole ID: CPT 1-26
Ground Surface Elevation (m): 94.09
Investigation Date: 18-Feb-26
Dissipation Test Depth (m) 2.50

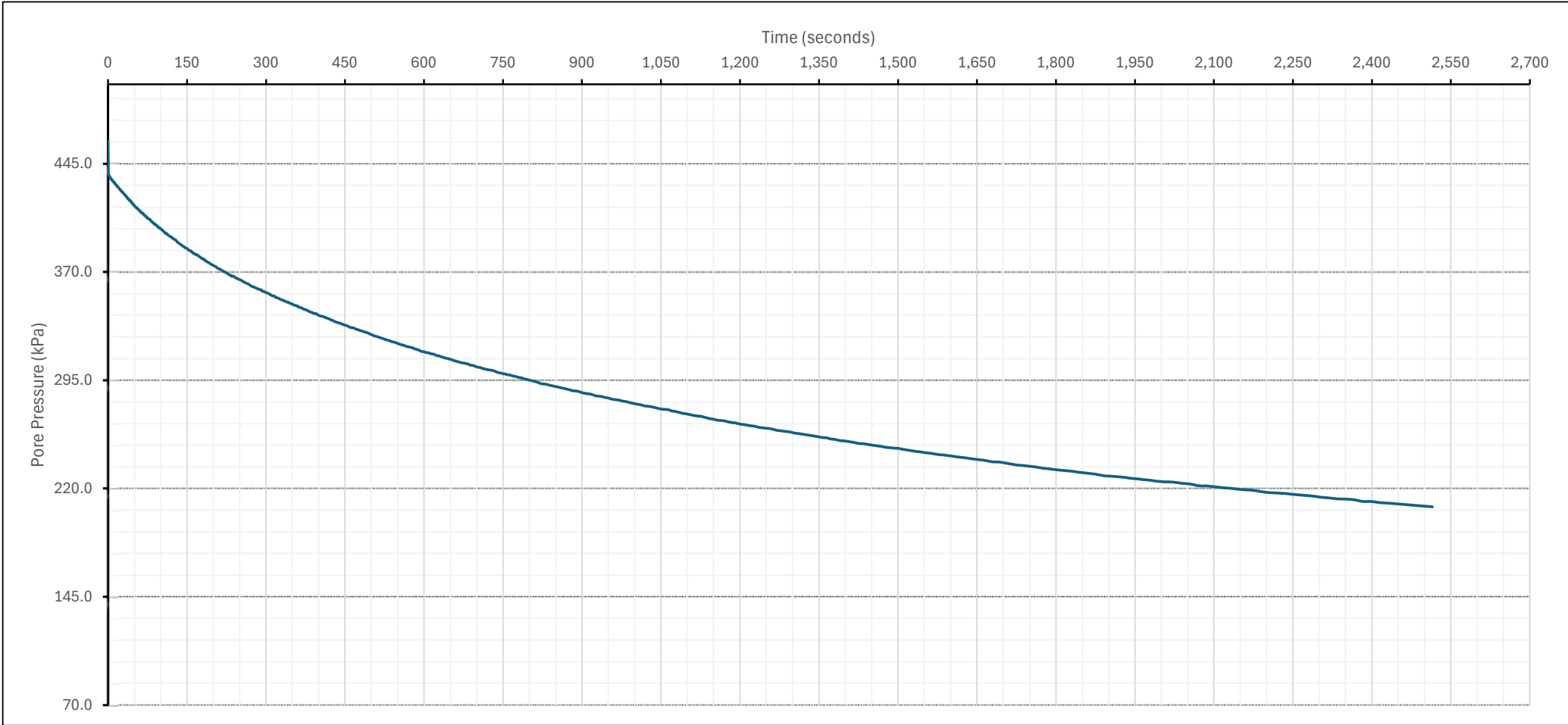


NOTES: DISSIPATION TEST COMPLETE AT 2.5 m (ELEV. = 91.59 m) BELOW GROUND SURFACE. THE UPPER 0.9 m WERE AUGERED OUT PRIOR TO ADVANCEMENT OF THE CPT. T50 WAS MEASURED AS 41.5 SECONDS FROM PEAK PORE PRESSURE MEASUREMENT. PATERSON CONDUCTED THE CPT TEST WITH A 15cm² CONE.

DISCLAIMER: THE DATA PRESENTED IN THIS LOG IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHO IT WAS PRODUCED. THIS LOG SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

Paterson File: PG7751
Client: FCRI Properties LP
Project: Proposed Commercial Development
Address 375 Didsbury Road, Ottawa, Ontario

Test Hole ID: CPT 1-26
Ground Surface Elevation (m): 94.09
Investigation Date: 18-Feb-26
Dissipation Test Depth (m) 10.15

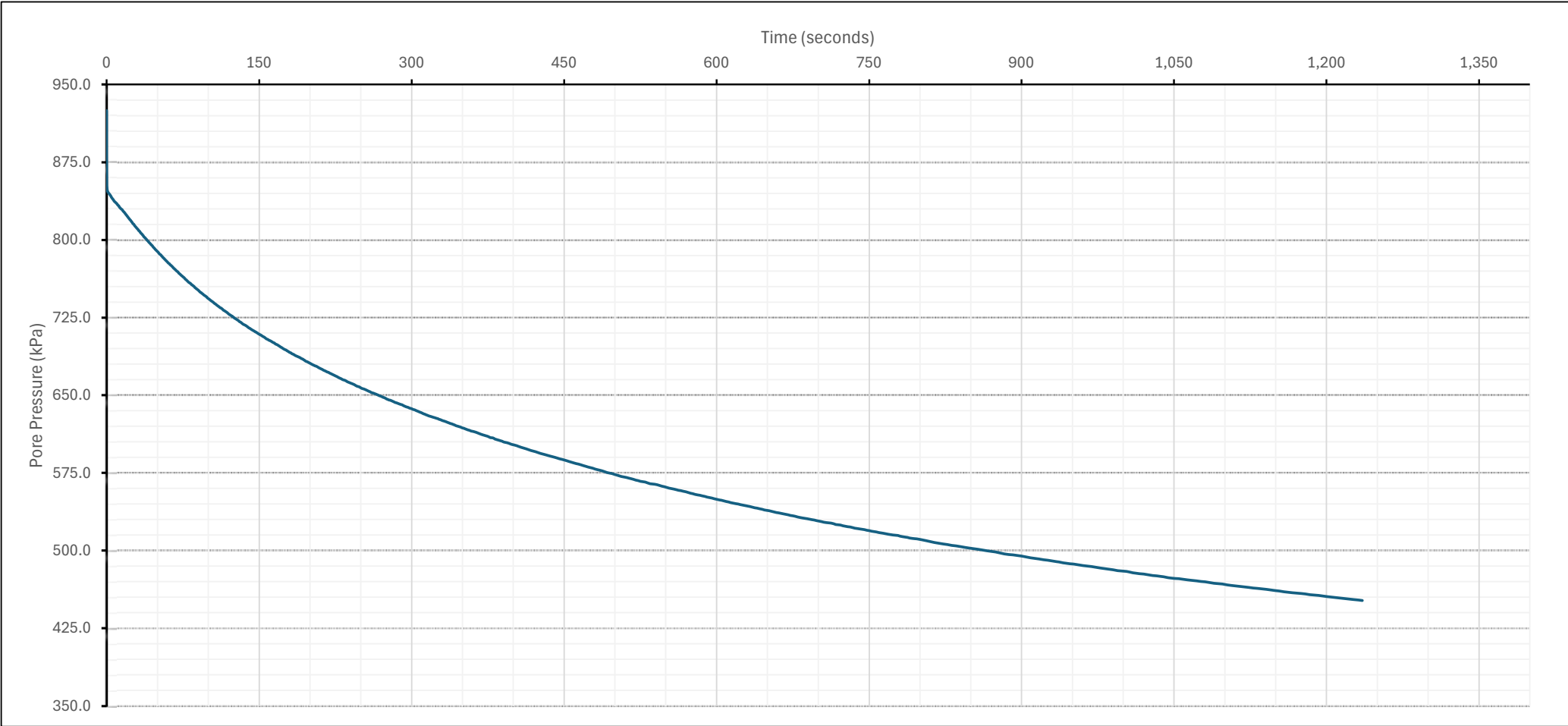


NOTES: DISSIPATION TEST COMPLETE AT 10.15 m (ELEV. = 83.94 m) BELOW GROUND SURFACE. THE UPPER 0.9 m WERE AUGERED OUT PRIOR TO ADVANCEMENT OF THE CPT. T50 WAS MEASURED AS 1874.8 SECONDS FROM PEAK PORE PRESSURE MEASUREMENT. PATERSON CONDUCTED THE CPT TEST WITH A 15cm2 CONE.

DISCLAIMER: THE DATA PRESENTED IN THIS LOG IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHO IT WAS PRODUCED. THIS LOG SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

Paterson File: PG7751
Client: FCRI Properties LP
Project: Proposed Commercial Development
Address 375 Didsbury Road, Ottawa, Ontario

Test Hole ID: CPT 1-26
Ground Surface Elevation (m): 94.04
Investigation Date: 18-Feb-26
Dissipation Test Depth (m) 20.03

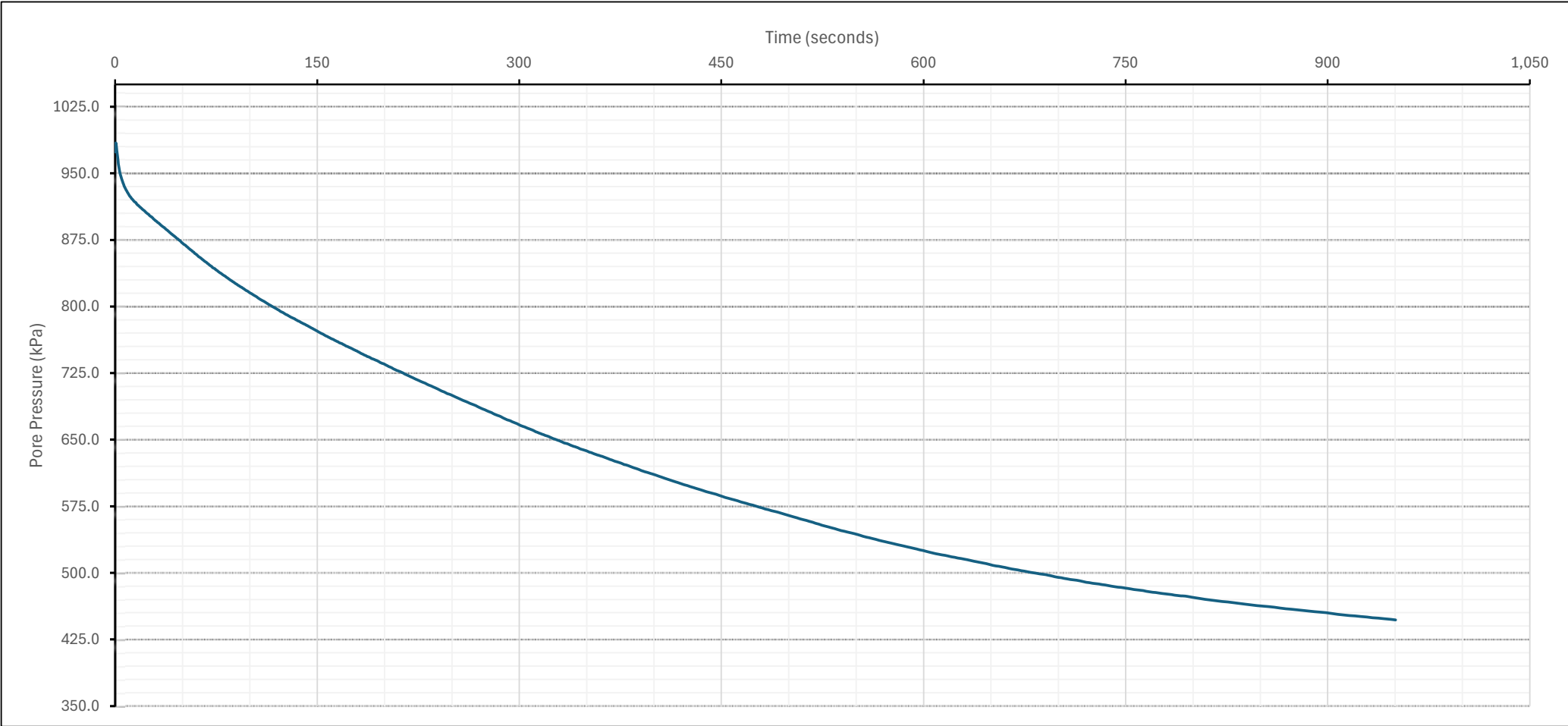


NOTES: DISSIPATION TEST COMPLETE AT 20.03 m (ELEV. = 74.01 m) BELOW GROUND SURFACE. THE UPPER 0.9 m WERE AUGERED OUT PRIOR TO ADVANCEMENT OF THE CPT. T50 WAS MEASURED AS 1140.8 SECONDS FROM PEAK PORE PRESSURE MEASUREMENT. PATERSON CONDUCTED THE CPT TEST WITH A 15cm2 CONE.

DISCLAIMER: THE DATA PRESENTED IN THIS LOG IS THE PROPERTY OF PATERSON GROUP AND THE CLIENT FOR WHO IT WAS PRODUCED. THIS LOG SHOULD BE READ IN CONJUNCTION WITH ITS CORRESPONDING REPORT. PATERSON GROUP IS NOT RESPONSIBLE FOR THE UNAUTHORIZED USE OF THIS DATA.

Paterson File: PG7751
Client: FCRI Properties LP
Project: Proposed Commercial Development
Address 375 Didsbury Road, Ottawa, Ontario

Test Hole ID: CPT 1-26
Ground Surface Elevation (m): 94.09
Investigation Date: 18-Feb-26
Dissipation Test Depth (m) 30.10

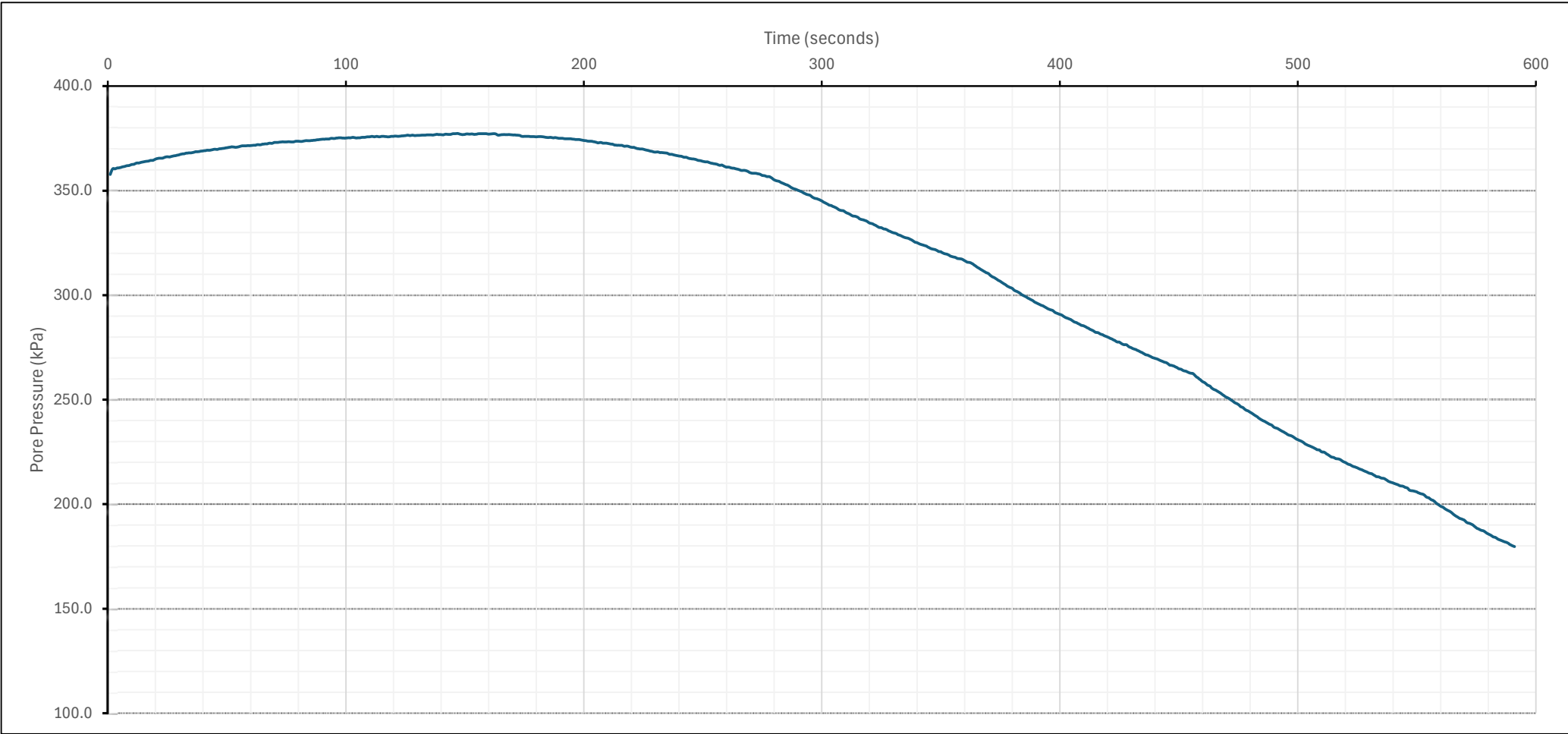


NOTES: DISSIPATION TEST COMPLETE AT 30.1 m (ELEV. = 63.99 m) BELOW GROUND SURFACE. THE UPPER 1.4 m WERE AUGERED OUT PRIOR TO ADVANCEMENT OF THE CPT. T50 WAS MEASURED AS 729.7 SECONDS FROM PEAK PORE PRESSURE MEASUREMENT. PATERSON CONDUCTED THE CPT TEST WITH A 15cm2 CONE.

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Paterson File: PG7751
Client: FCRI Properties LP
Project: Proposed Commercial Development
Address: 375 Didsbury Road, Ottawa, Ontario

Test Hole ID: CPT 2-26
Ground Surface Elevation (m): 93.25
Investigation Date: 05-Mar-26
Dissipation Test Depth (m) 10.02

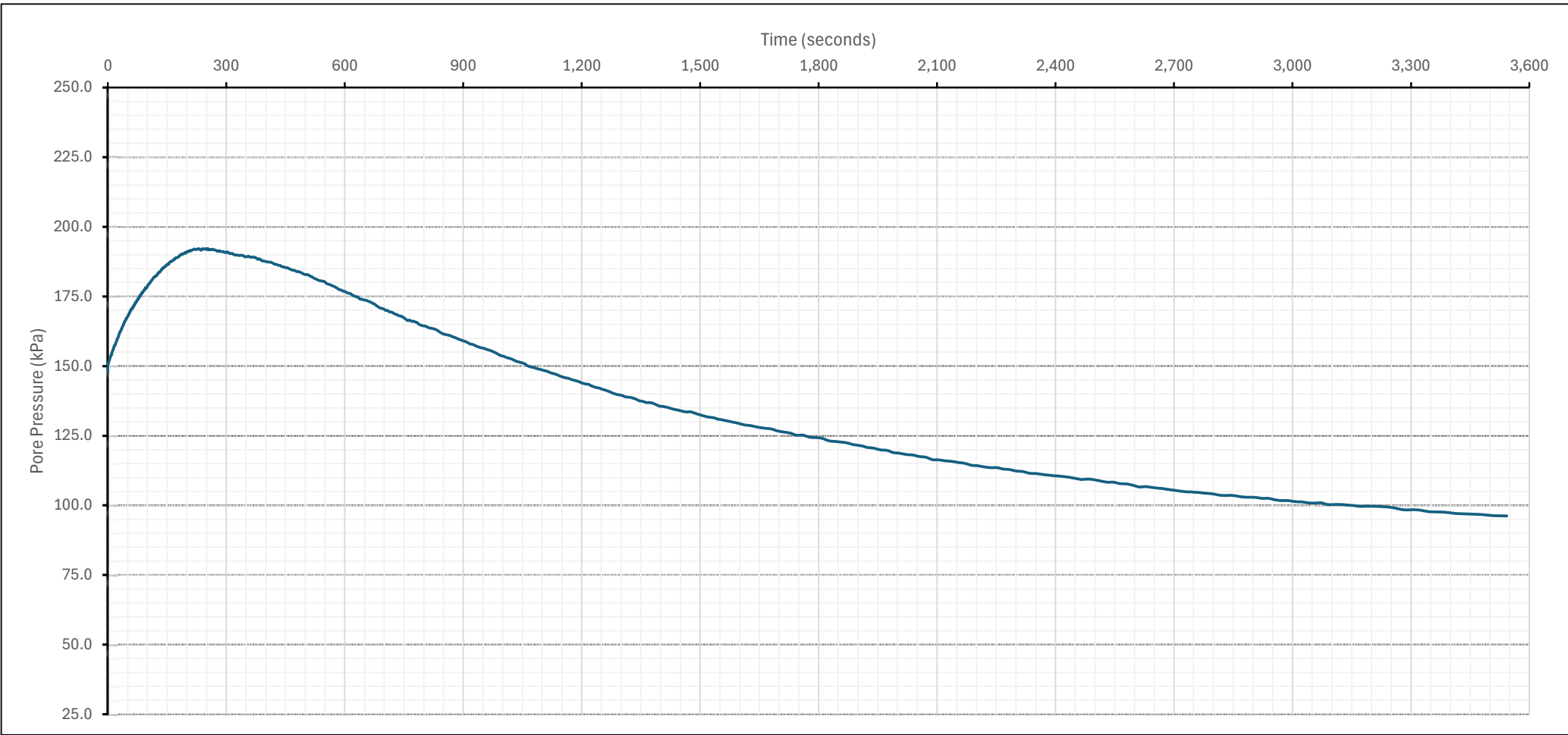


NOTES: DISSIPATION TEST COMPLETE AT 10.015 m (ELEV. = 83.235 m) BELOW GROUND SURFACE. THE UPPER 0.78 m WERE AUGERED OUT PRIOR TO ADVANCEMENT OF THE CPT. T50 WAS MEASURED AS 3770.4 SECONDS FROM PEAK PORE PRESSURE MEASUREMENT. PATERSON CONDUCTED THE CPT TEST WITH A 15cm2 CONE.

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Paterson File: PG7751
Client: FCRI Properties LP
Project: Proposed Commercial Development
Address 375 Didsbury Road, Ottawa, Ontario

Test Hole ID: CPT 3-26
Ground Surface Elevation (m): 93.64
Investigation Date: 06-Mar-26
Dissipation Test Depth (m) 4.51

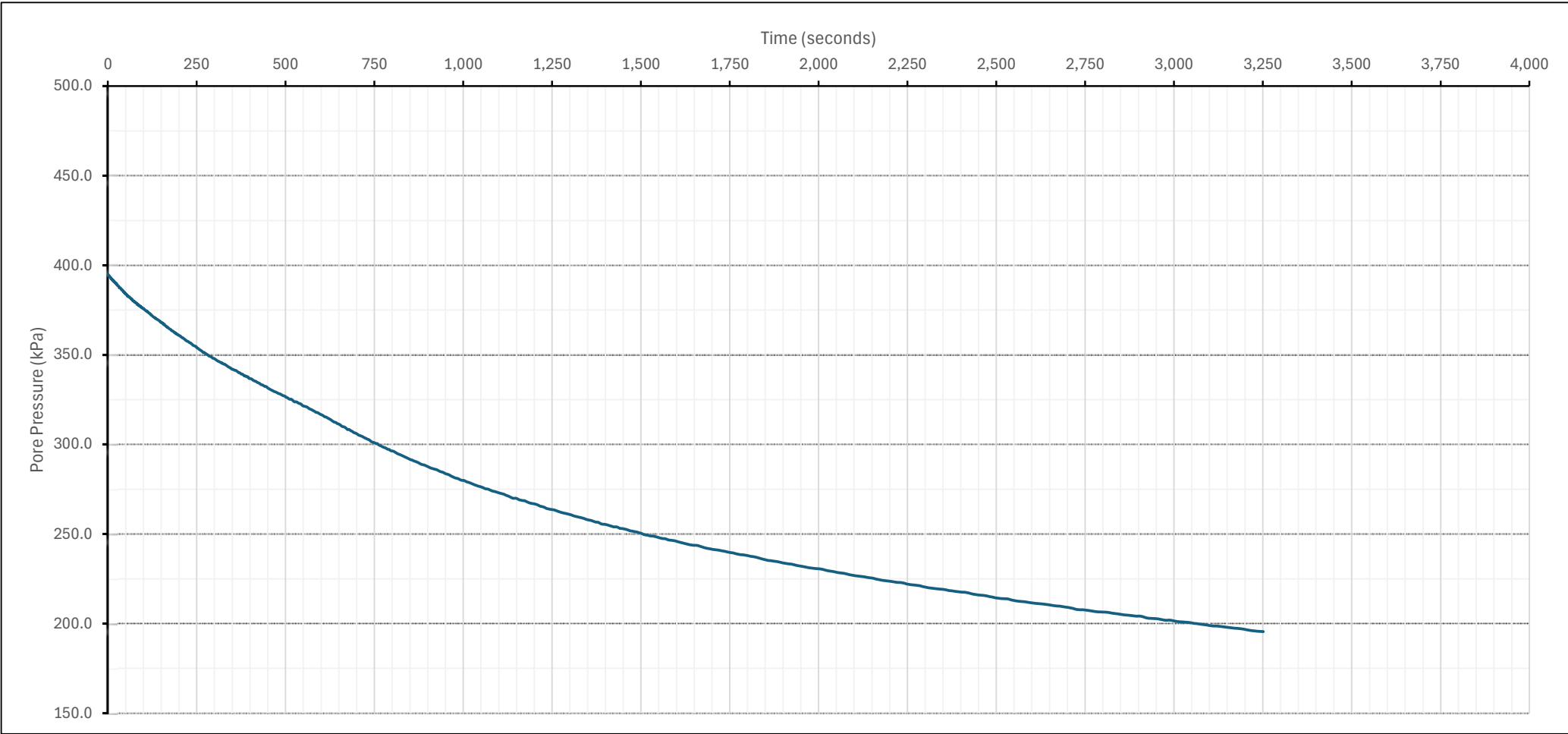


NOTES: DISSIPATION TEST COMPLETE AT 4.51 m (ELEV. = 89.13 m) BELOW GROUND SURFACE. THE UPPER 0.91 m WERE AUGERED OUT PRIOR TO ADVANCEMENT OF THE CPT. T50 WAS MEASURED AS 3277.3 SECONDS FROM PEAK PORE PRESSURE MEASUREMENT. PATERSON CONDUCTED THE CPT TEST WITH A 15cm2 CONE.

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Paterson File: PG7751
Client: FCRI Properties LP
Project: Proposed Commercial Development
Address: 375 Didsbury Road, Ottawa, Ontario

Test Hole ID: CPT 3-26
Ground Surface Elevation (m): 93.64
Investigation Date: 06-Mar-26
Dissipation Test Depth (m) 10.10

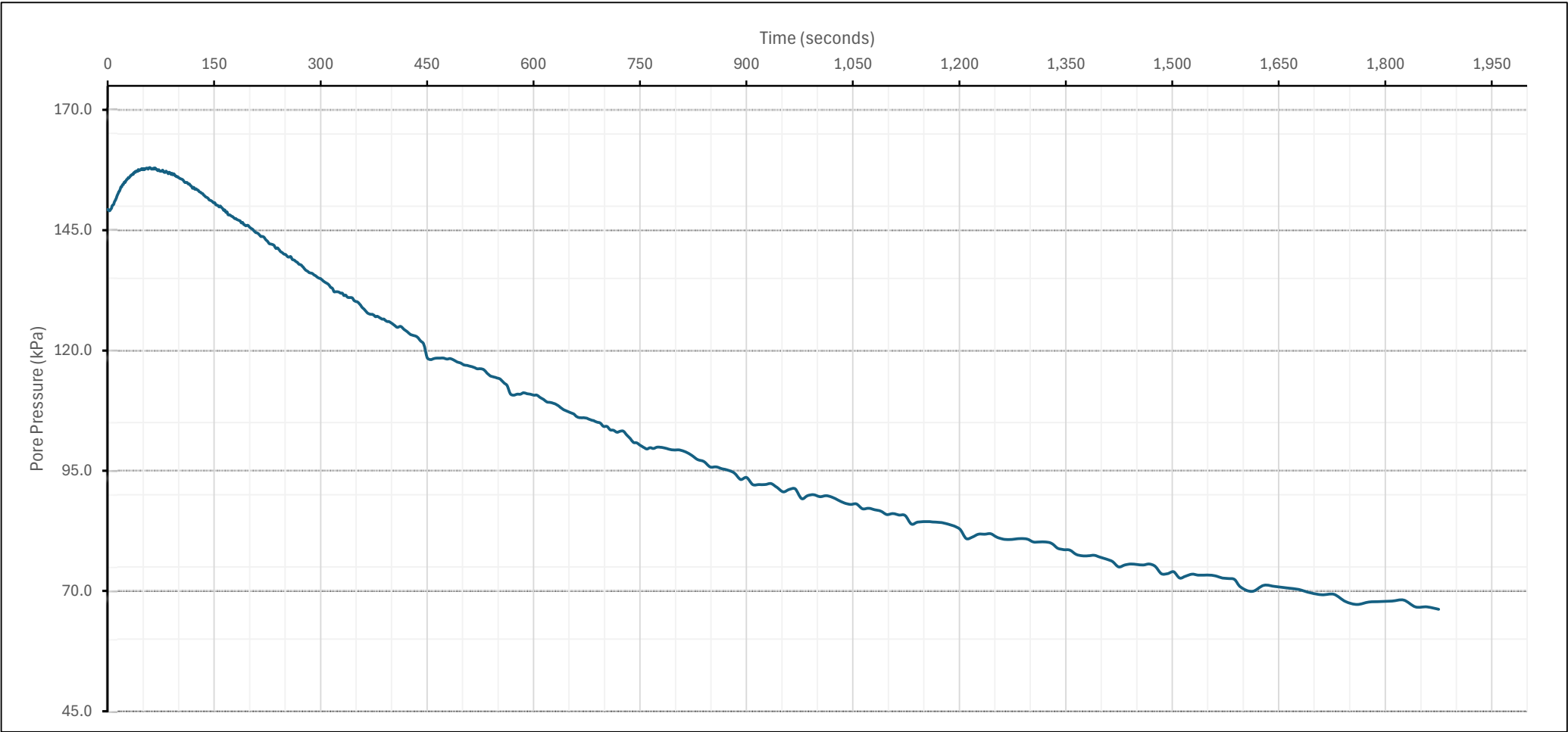


NOTES: DISSIPATION TEST COMPLETE AT 10.1 m (ELEV. = 83.54 m) BELOW GROUND SURFACE. THE UPPER 0.91 m WERE AUGERED OUT PRIOR TO ADVANCEMENT OF THE CPT. T50 WAS MEASURED AS 3186.8 SECONDS FROM PEAK PORE PRESSURE MEASUREMENT. PATERSON CONDUCTED THE CPT TEST WITH A 15cm2 CONE."

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Paterson File: PG7751
Client: FCRI Properties LP
Project: Proposed Commercial Development
Address: 375 Didsbury Road, Ottawa, Ontario

Test Hole ID: CPT 4-26
Ground Surface Elevation (m): 94.19
Investigation Date: 09-Mar-26
Dissipation Test Depth (m) 4.01

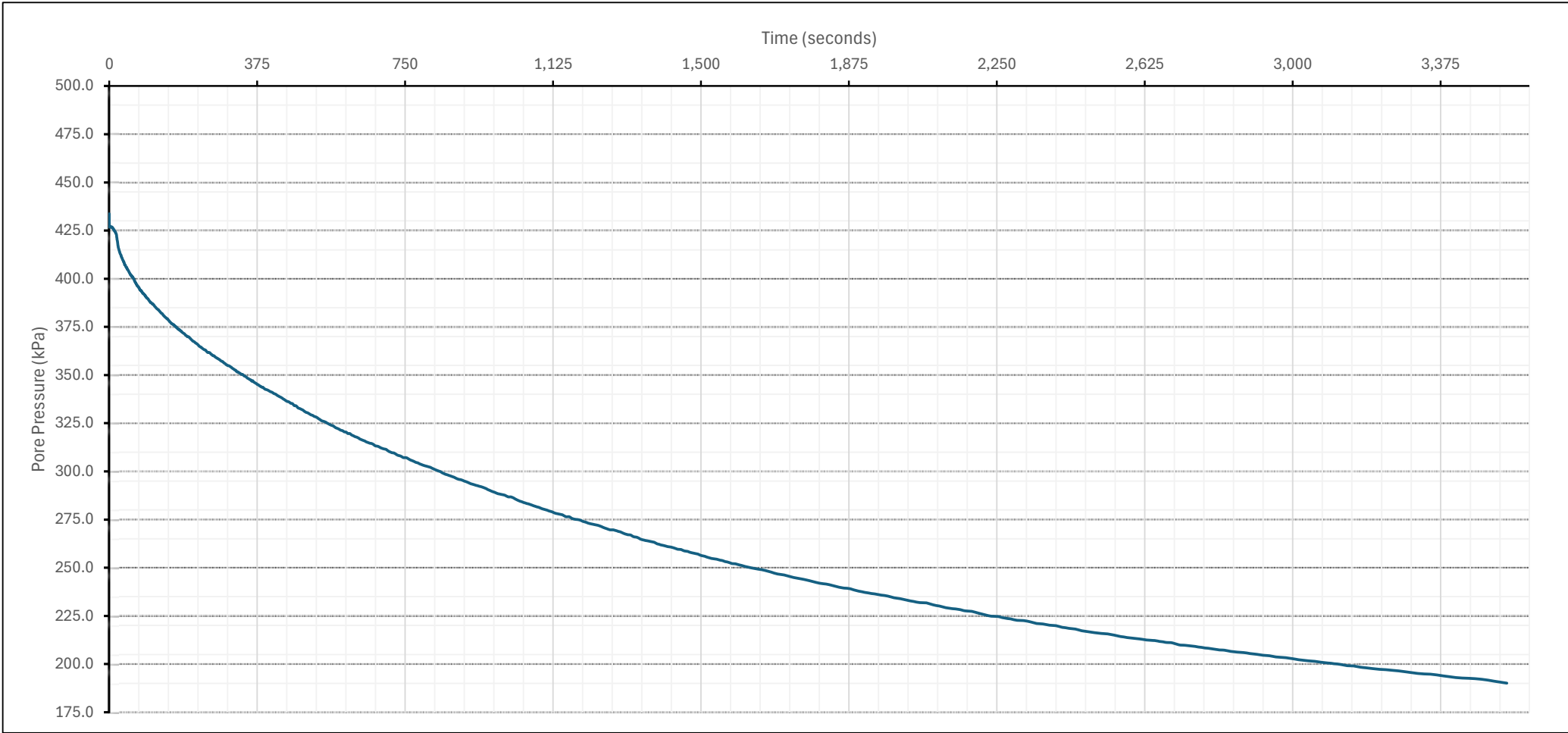


NOTES: DISSIPATION TEST COMPLETE AT 4.01 m (ELEV. = 90.18 m) BELOW GROUND SURFACE. THE UPPER 0.94 m WERE AUGERED OUT PRIOR TO ADVANCEMENT OF THE CPT. T50 WAS MEASURED AS 1264.8 SECONDS FROM PEAK PORE PRESSURE MEASUREMENT. PATERSON CONDUCTED THE CPT TEST WITH A 15cm² CONE.

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Paterson File: PG7751
Client: FCRI Properties LP
Project: Proposed Commercial Development
Address 375 Didsbury Road, Ottawa, Ontario

Test Hole ID: CPT 4-26
Ground Surface Elevation (m): 94.19
Investigation Date: 09-Mar-26
Dissipation Test Depth (m) 10.10

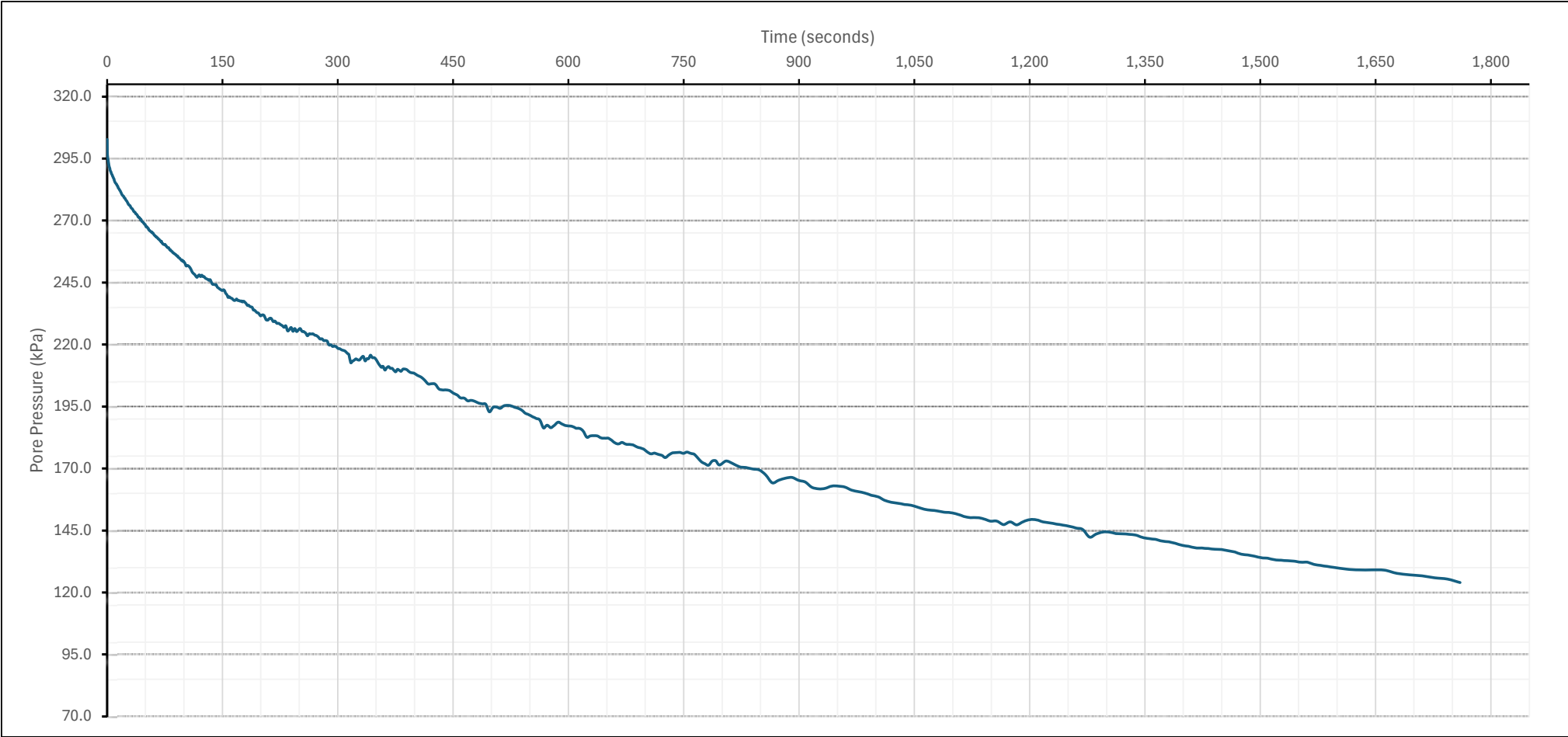


NOTES: DISSIPATION TEST COMPLETE AT 10.1 m (ELEV. = 84.09 m) BELOW GROUND SURFACE. THE UPPER 0.94 m WERE AUGERED OUT PRIOR TO ADVANCEMENT OF THE CPT. T50 WAS MEASURED AS 2514.5 SECONDS FROM PEAK PORE PRESSURE MEASUREMENT. PATERSON CONDUCTED THE CPT TEST WITH A 15cm2 CONE.

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Paterson File: PG7751
Client: FCRI Properties LP
Project: Proposed Commercial Development
Address: 375 Didsbury Road, Ottawa, Ontario

Test Hole ID: CPT 5-26
Ground Surface Elevation (m): 93.37
Investigation Date: 09-Mar-26
Dissipation Test Depth (m) 4.05

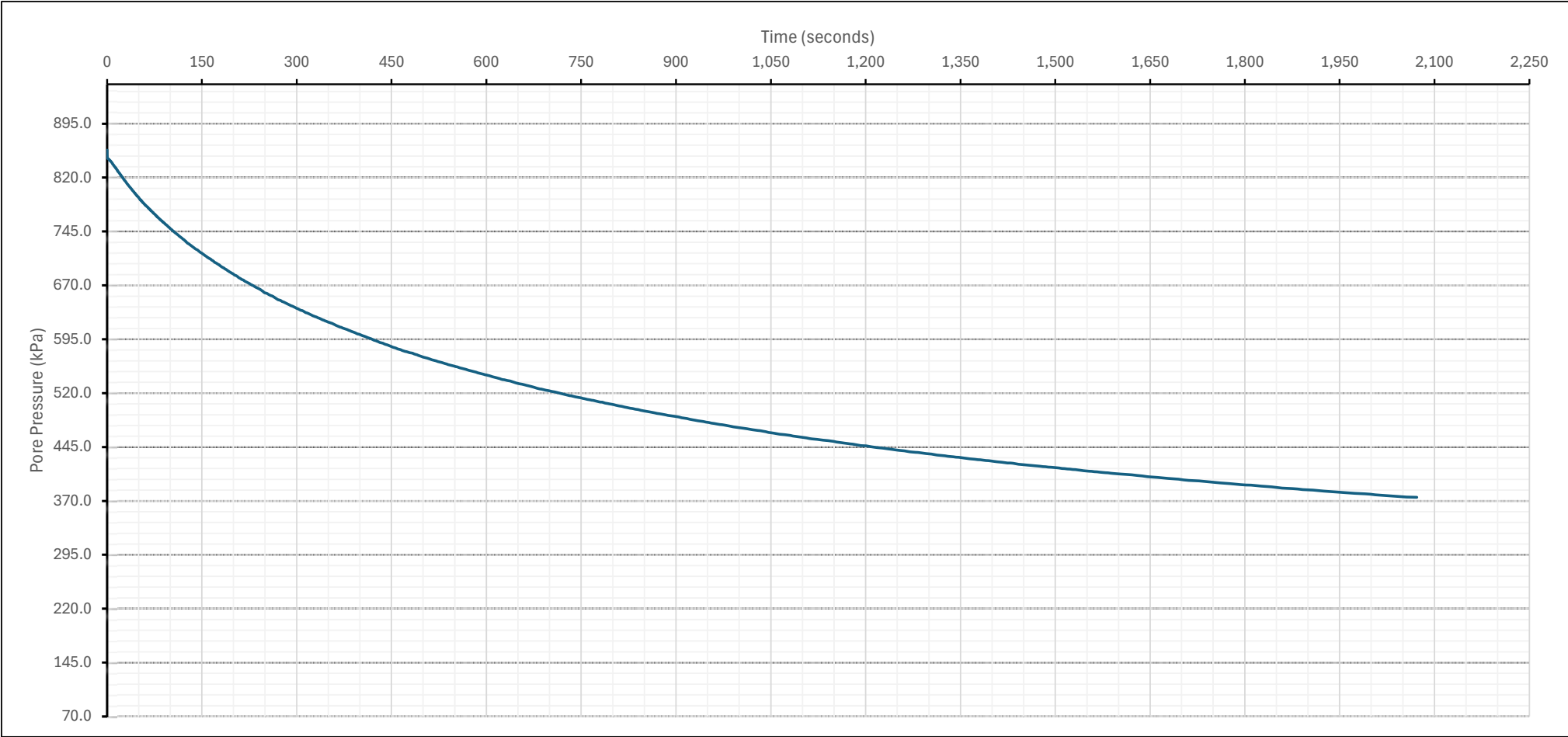


NOTES: DISSIPATION TEST COMPLETE AT 4.05 m (ELEV. = 89.32 m) BELOW GROUND SURFACE. THE UPPER 0.9 m WERE AUGERED OUT PRIOR TO ADVANCEMENT OF THE CPT. T50 WAS MEASURED AS 1114.5 SECONDS FROM PEAK PORE PRESSURE MEASUREMENT. PATERSON CONDUCTED THE CPT TEST WITH A 15cm2 CONE.

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Paterson File: PG7751
Client: FCRI Properties LP
Project: Proposed Commercial Development
Address 375 Didsbury Road, Ottawa, Ontario

Test Hole ID: CPT 5-26
Ground Surface Elevation (m): 93.37
Investigation Date: 09-Mar-26
Dissipation Test Depth (m) 20.10

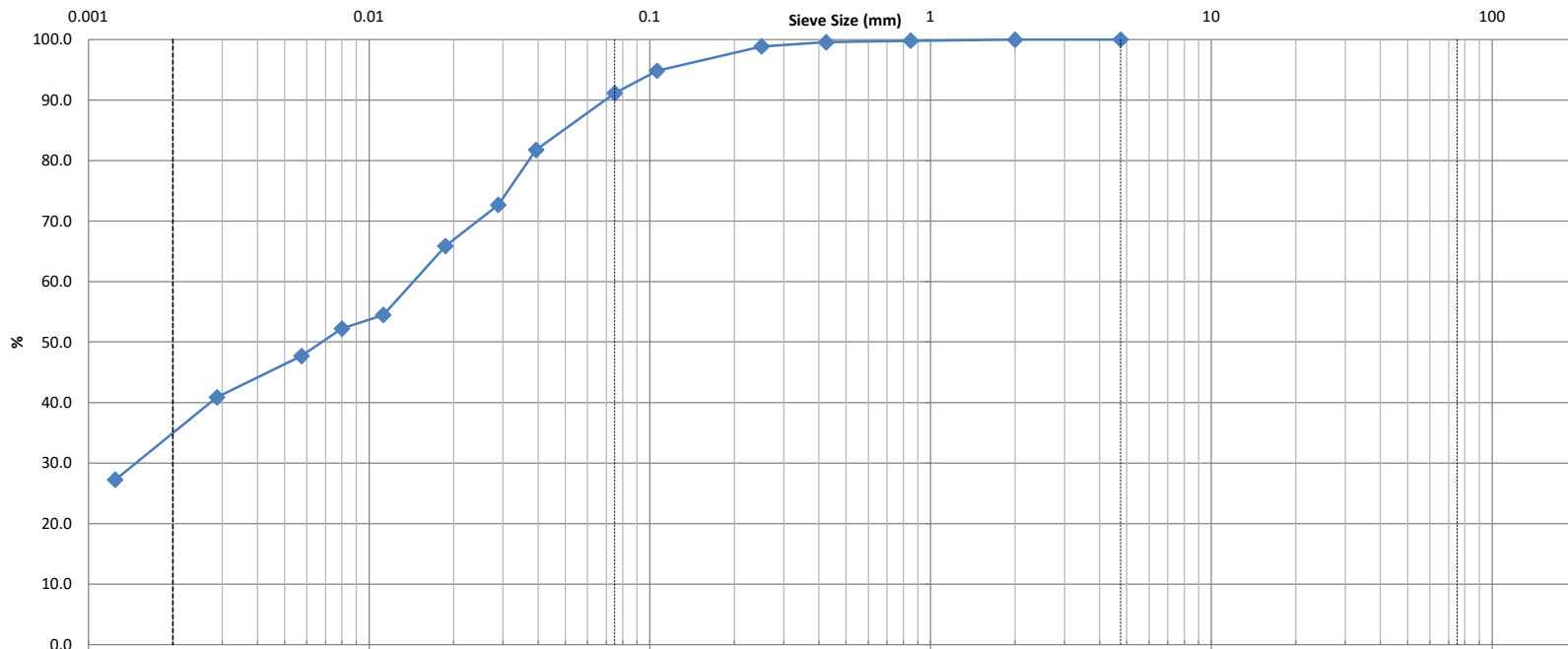


NOTES: DISSIPATION TEST COMPLETE AT 20.1 m (ELEV. = 73.27 m) BELOW GROUND SURFACE. THE UPPER 0.9 m WERE AUGERED OUT PRIOR TO ADVANCEMENT OF THE CPT. T50 WAS MEASURED AS 1347.3 SECONDS FROM PEAK PORE PRESSURE MEASUREMENT. PATERSON CONDUCTED THE CPT TEST WITH A 15cm2 CONE.

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**SIEVE ANALYSIS
ASTM C136**

CLIENT:	First Capital Realty	DEPTH:	7'6" - 9'6"	FILE NO:	PG7751
CONTRACT NO.:		BH OR TP No.:	BH13-25 SS4	LAB NO:	64300
PROJECT:	375 Dilsbury Road			DATE RECEIVED:	6-Nov-25
				DATE TESTED:	6-Nov-25
DATE SAMPLED:	4-Nov-25			DATE REPORTED:	13-Nov-25
SAMPLED BY:	A.E			TESTED BY:	C.M.



Clay	Silt	Sand			Gravel		Cobble
		Fine	Medium	Coarse	Fine	Coarse	

Identification	Soil Classification					MC(%)	LL	PL	PI	Cc	Cu
						41.0%					
	D100	D60	D30	D10	Gravel (%)	Sand (%)		Silt (%)		Clay (%)	
					0.0	8.9		56.1		35.0	

Comments:

REVIEWED BY:

Curtis Beadow

Joe Forsyth, P. Eng.

CLIENT:	First Capital Realty	DEPTH:	7'6" - 9'6"	FILE NO.:	PG7751
PROJECT:	375 Dilsbury Road	BH OR TP No.:	BH13-25 SS4	DATE SAMPLED:	04-Nov-25
LAB No. :	64300	TESTED BY:	C.M.	DATE RECEIVED:	06-Nov-25
SAMPLED BY:	A.E	DATE REPT'D:	13-Nov-25	DATE TESTED:	06-Nov-25

SAMPLE INFORMATION

SAMPLE MASS		SPECIFIC GRAVITY	
106.4		2.700	
INITIAL WEIGHT	50.00	HYGROSCOPIC MOISTURE	
WEIGHT CORRECTED	43.54	TARE WEIGHT	0.00
WT. AFTER WASH BACK SIEVE	4.82	AIR DRY	122.20
SOLUTION CONCENTRATION	40 g/L	OVEN DRY	106.40
		CORRECTED	0.871

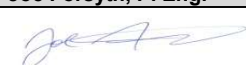
GRAIN SIZE ANALYSIS

SIEVE DIAMETER (mm)	WEIGHT RETAINED (g)	PERCENT RETAINED	PERCENT PASSING
26.5			
19			
13.2			
9.5			
4.75	0.00	0.0	100.0
2.0	0.03	0.0	100.0
Pan	106.37		
0.850	0.09	0.2	99.8
0.425	0.21	0.4	99.6
0.250	0.55	1.1	98.9
0.106	2.56	5.1	94.9
0.075	4.42	8.9	91.1
Pan	4.82		
SIEVE CHECK	0.0	MAX = 0.3%	

HYDROMETER DATA

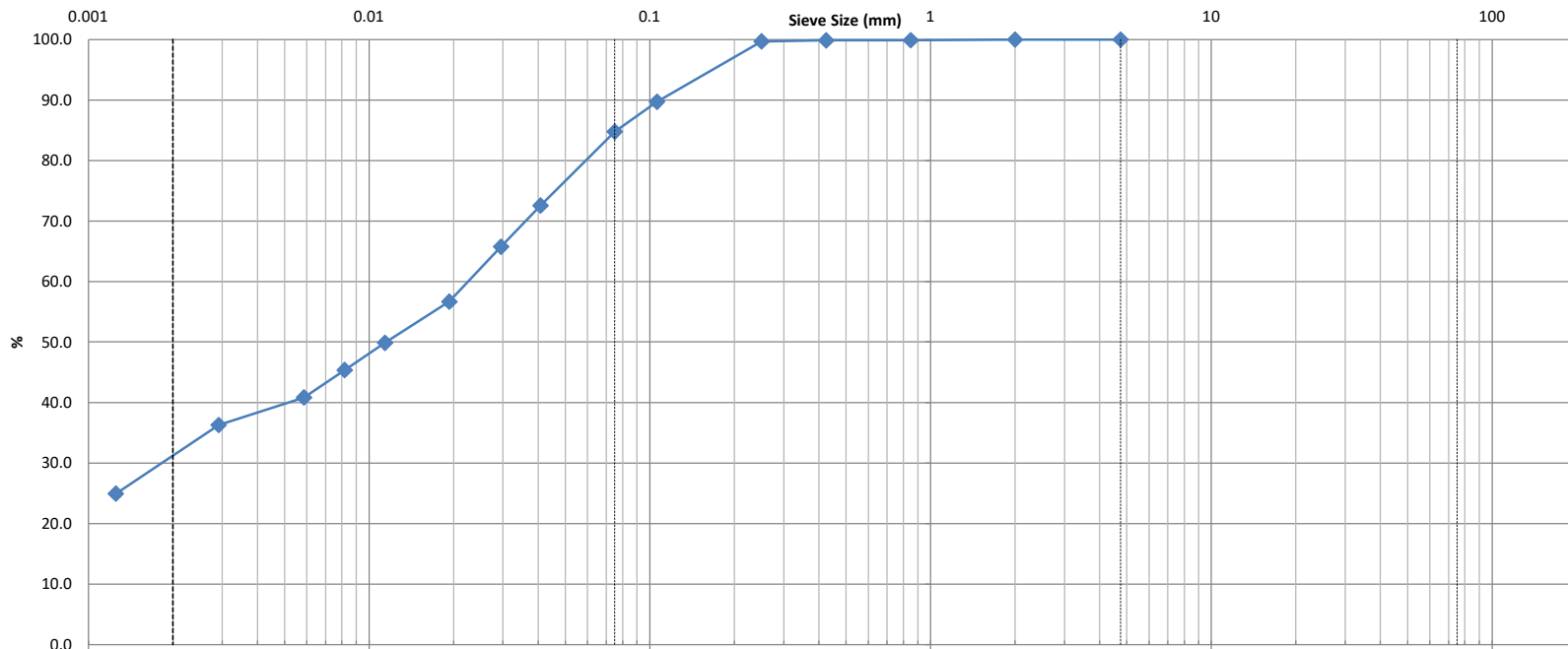
ELAPSED	TIME (24 hours)	Hs	Hc	Temp. (°C)	DIAMETER	(P)	TOTAL PERCENT PASSING
1	7:59	42.0	6.0	23.0	0.0393	81.8	81.7
2	8:00	38.0	6.0	23.0	0.0288	72.7	72.7
5	8:03	35.0	6.0	23.0	0.0187	65.9	65.8
15	8:13	30.0	6.0	23.0	0.0112	54.5	54.5
30	8:28	29.0	6.0	23.0	0.0080	52.2	52.2
60	8:58	27.0	6.0	23.0	0.0057	47.7	47.7
250	12:08	24.0	6.0	23.0	0.0029	40.9	40.9
1440	7:58	18.0	6.0	23.0	0.0012	27.3	27.2

Moisture = 41.0%

REVIEWED BY:	C. Beadow	Joe Forsyth, P. Eng.
		

**SIEVE ANALYSIS
ASTM C136**

CLIENT:	First Capital Realty	DEPTH:	5' - 7'	FILE NO:	PG7751
CONTRACT NO.:		BH OR TP No.:	BH18-25 SS3	LAB NO:	64301
PROJECT:	375 Dilsbury Road			DATE RECEIVED:	6-Nov-25
				DATE TESTED:	6-Nov-25
DATE SAMPLED:	4-Nov-25			DATE REPORTED:	13-Nov-25
SAMPLED BY:	A.E			TESTED BY:	C.M.



Clay	Silt			Sand			Gravel		Cobble
				Fine	Medium	Coarse	Fine	Coarse	

Identification	Soil Classification					MC(%)	LL	PL	PI	Cc	Cu
						41.0%					
	D100	D60	D30	D10	Gravel (%)	Sand (%)		Silt (%)		Clay (%)	
					0.0	15.2		53.3		31.5	

Comments:

REVIEWED BY:

Curtis Beadow

Joe Forsyth, P. Eng.

CLIENT:	First Capital Realty	DEPTH:	5' - 7'	FILE NO.:	PG7751
PROJECT:	375 Dilsbury Road	BH OR TP No.:	BH18-25 SS3	DATE SAMPLED:	04-Nov-25
LAB No. :	64301	TESTED BY:	C.M.	DATE RECEIVED:	06-Nov-25
SAMPLED BY:	A.E	DATE REPT'D:	13-Nov-25	DATE TESTED:	06-Nov-25

SAMPLE INFORMATION

SAMPLE MASS		SPECIFIC GRAVITY	
109.0		2.700	
INITIAL WEIGHT	50.00	HYGROSCOPIC MOISTURE	
WEIGHT CORRECTED	43.60	TARE WEIGHT	0.00
WT. AFTER WASH BACK SIEVE	8.46	AIR DRY	125.00
SOLUTION CONCENTRATION	40 g/L	OVEN DRY	109.00
		CORRECTED	0.872

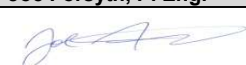
GRAIN SIZE ANALYSIS

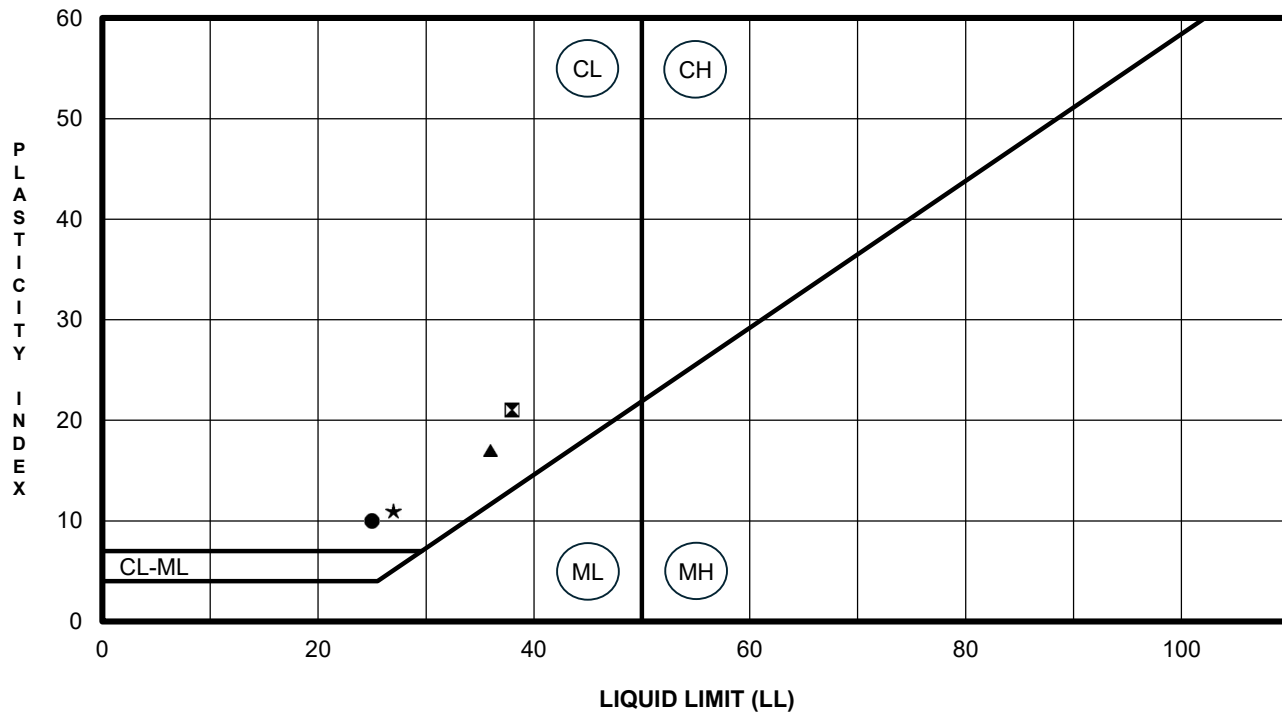
SIEVE DIAMETER (mm)	WEIGHT RETAINED (g)	PERCENT RETAINED	PERCENT PASSING
26.5			
19			
13.2			
9.5			
4.75	0.00	0.0	100.0
2.0	0.00	0.0	100.0
Pan	109.00		
0.850	0.05	0.1	99.9
0.425	0.07	0.1	99.9
0.250	0.16	0.3	99.7
0.106	5.14	10.3	89.7
0.075	7.62	15.2	84.8
Pan	8.46		
SIEVE CHECK	0.0	MAX = 0.3%	

HYDROMETER DATA

ELAPSED	TIME (24 hours)	Hs	Hc	Temp. (°C)	DIAMETER	(P)	TOTAL PERCENT PASSING
1	8:03	38.0	6.0	23.0	0.0408	72.6	72.6
2	8:04	35.0	6.0	23.0	0.0296	65.8	65.8
5	8:07	31.0	6.0	23.0	0.0193	56.7	56.7
15	8:17	28.0	6.0	23.0	0.0114	49.9	49.9
30	8:32	26.0	6.0	23.0	0.0082	45.4	45.4
60	9:02	24.0	6.0	23.0	0.0059	40.8	40.8
250	12:12	22.0	6.0	23.0	0.0029	36.3	36.3
1440	8:02	17.0	6.0	23.0	0.0013	24.9	24.9

Moisture = 41.0%

REVIEWED BY:	C. Beadow	Joe Forsyth, P. Eng.
		

[illegible]

CLIENT First Capital Realty Inc.

FILE NO.

PG7751

PROJECT Geotechnical Investigation - Proposed Commercial

DATE _____

12 Nov 25

Development - 375 Didsbury Road, Ottawa, Ontario



ATTERBERG LIMITS
703/704

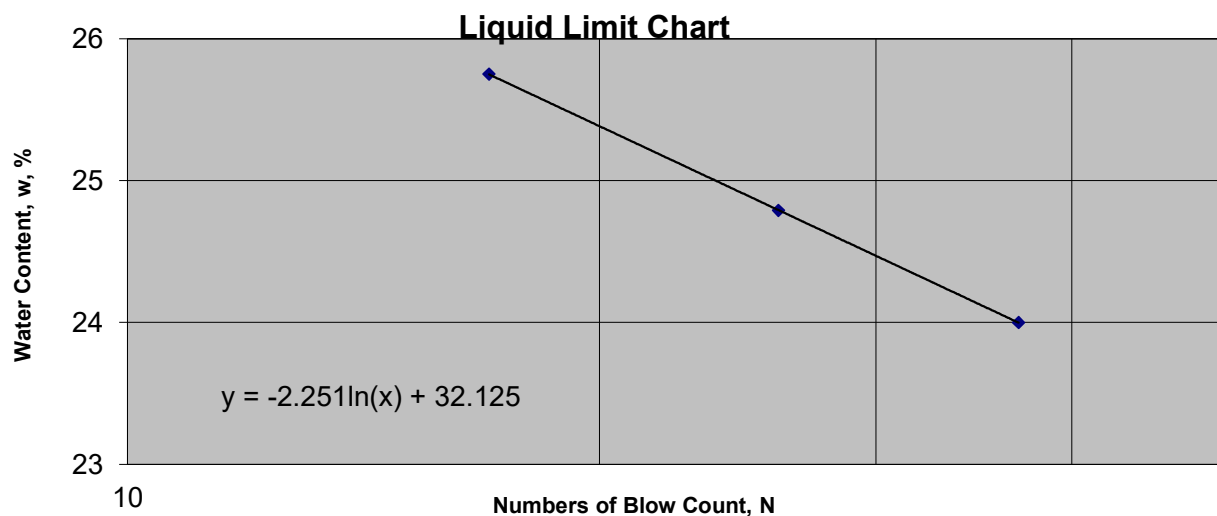
LS-

CLIENT:	First Capital Realty	FILE NO.:	PG7751
PROJECT:	375 Didsbury Road	DATE SAMPLED:	29-Oct
LOCATION:	BH1-25 SS5, 10' - 12'	DATE REPORTED:	12-Nov

CAN NO.	2	3	4				
WT. OF CAN	8.61	8.64	8.64				
WT. OF SOIL & CAN	19.5	18.96	18.25				
WT. OF DRY SOIL & CAN	17.27	16.91	16.39				
WT. OF MOISTURE	2.23	2.05	1.86				
WT. OF DRY SOIL & CAN	8.66	8.27	7.75				
WATER CONTENT, w, %	25.75	24.79	24				
NO. OF BLOWS, N	17	26	37				

CAN NO.	2	4
WT. OF CAN	19.89	19.99
WT. OF SOIL & CAN	28.52	28.24
WT. OF DRY SOIL & CAN	27.43	27.17
WT. OF MOISTURE	1.09	1.07
WT. OF DRY SOIL & CAN	7.54	7.18
WATER CONTENT, w, %	14.46	14.90

RESULTS	
LIQUID LIMIT	25
PLASTIC LIMIT	15
PLASTICITY INDEX	10



TECHNICIAN: CP		C. Beadow	J. Forsyth, P. Eng.
	REVIEWED BY:	<i>[Signature]</i>	<i>[Signature]</i>



ATTERBERG LIMITS
703/704

LS-

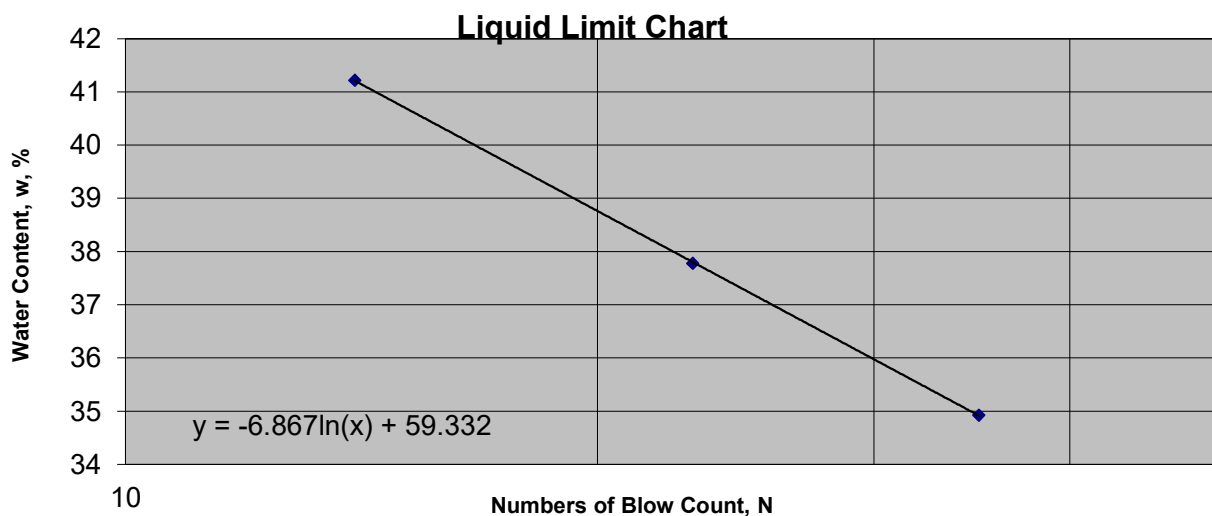
CLIENT:	First Capital Realty	FILE NO.:	PG7751
PROJECT:	375 Didsbury Road	DATE SAMPLED:	03-Nov
LOCATION:	BH9-25 SS3, 5' - 7'	DATE REPORTED:	12-Nov

CAN NO.	0	14	18				
WT. OF CAN	8.64	8.61	8.67				
WT. OF SOIL & CAN	17.24	18.31	17.67				
WT. OF DRY SOIL & CAN	14.73	15.65	15.34				
WT. OF MOISTURE	2.51	2.66	2.33				
WT. OF DRY SOIL & CAN	6.09	7.04	6.67				
WATER CONTENT, w, %	41.22	37.78	34.93				
NO. OF BLOWS, N	14	23	35				

RESULTS

LIQUID LIMIT	38
PLASTIC LIMIT	17
PLASTICITY INDEX	21

CAN NO.	14	18
WT. OF CAN	19.96	20.00
WT. OF SOIL & CAN	28.63	28.70
WT. OF DRY SOIL & CAN	27.36	27.42
WT. OF MOISTURE	1.27	1.28
WT. OF DRY SOIL & CAN	7.4	7.42
WATER CONTENT, w, %	17.16	17.25



TECHNICIAN: CP		C. Beadow	J. Forsyth, P. Eng.
	REVIEWED BY:		



ATTERBERG LIMITS
703/704

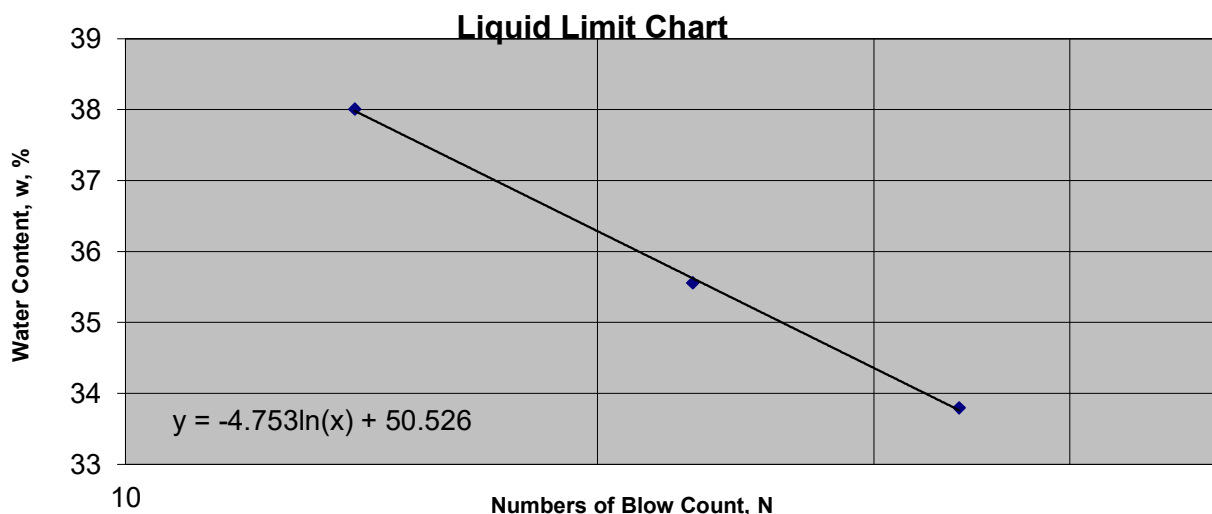
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CLIENT:	First Capital Realty	FILE NO.:	PG7751
PROJECT:	375 Didsbury Road	DATE SAMPLED:	03-Nov
LOCATION:	BH11-25 G4, 15' - 16'	DATE REPORTED:	12-Nov

CAN NO.	67	70	87				
WT. OF CAN	7.17	7.08	7.19				
WT. OF SOIL & CAN	16.72	16.42	16.77				
WT. OF DRY SOIL & CAN	14.09	13.97	14.35				
WT. OF MOISTURE	2.63	2.45	2.42				
WT. OF DRY SOIL & CAN	6.92	6.89	7.16				
WATER CONTENT, w, %	38.01	35.56	33.8				
NO. OF BLOWS, N	14	23	34				

CAN NO.	10	12
WT. OF CAN	19.77	16.71
WT. OF SOIL & CAN	28.39	25.42
WT. OF DRY SOIL & CAN	27.02	24.04
WT. OF MOISTURE	1.37	1.38
WT. OF DRY SOIL & CAN	7.25	7.33
WATER CONTENT, w, %	18.9	18.83

RESULTS	
LIQUID LIMIT	36
PLASTIC LIMIT	19
PLASTICITY INDEX	17



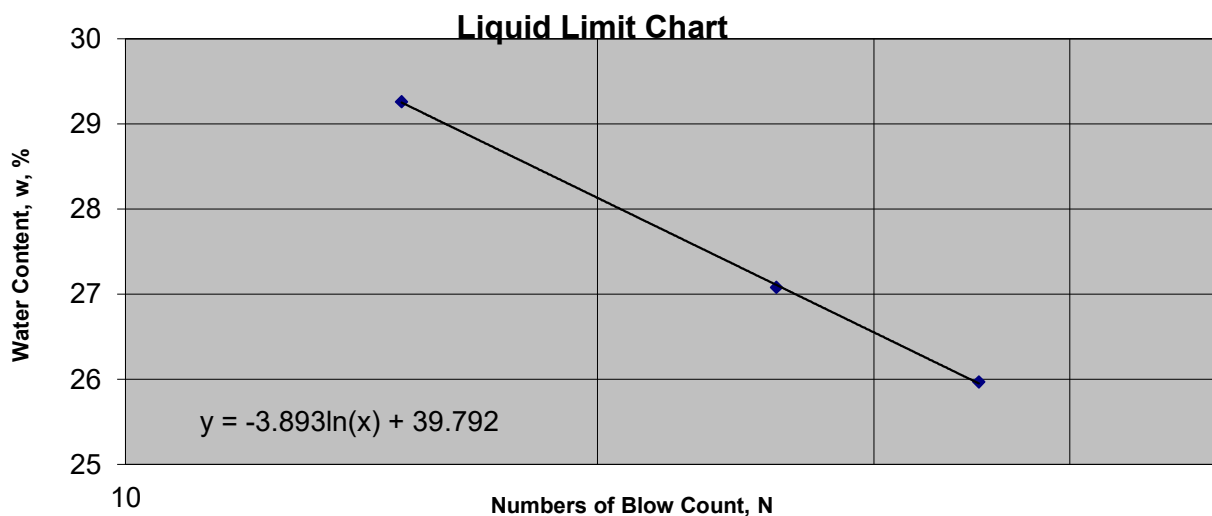
TECHNICIAN: CP		C. Beadow	J. Forsyth, P. Eng.
	REVIEWED BY:		

CLIENT:	First Capital Realty	FILE NO.:	PG7751
PROJECT:	375 Didsbury Road	DATE SAMPLED:	04-Nov
LOCATION:	BH15-25 SS6, 12'6" - 14'6"	DATE REPORTED:	12-Nov

CAN NO.	31	33	34				
WT. OF CAN	4.29	4.29	4.31				
WT. OF SOIL & CAN	14.76	13.77	14.74				
WT. OF DRY SOIL & CAN	12.39	11.75	12.59				
WT. OF MOISTURE	2.37	2.02	2.15				
WT. OF DRY SOIL & CAN	8.1	7.46	8.28				
WATER CONTENT, w, %	29.26	27.08	25.97				
NO. OF BLOWS, N	15	26	35				

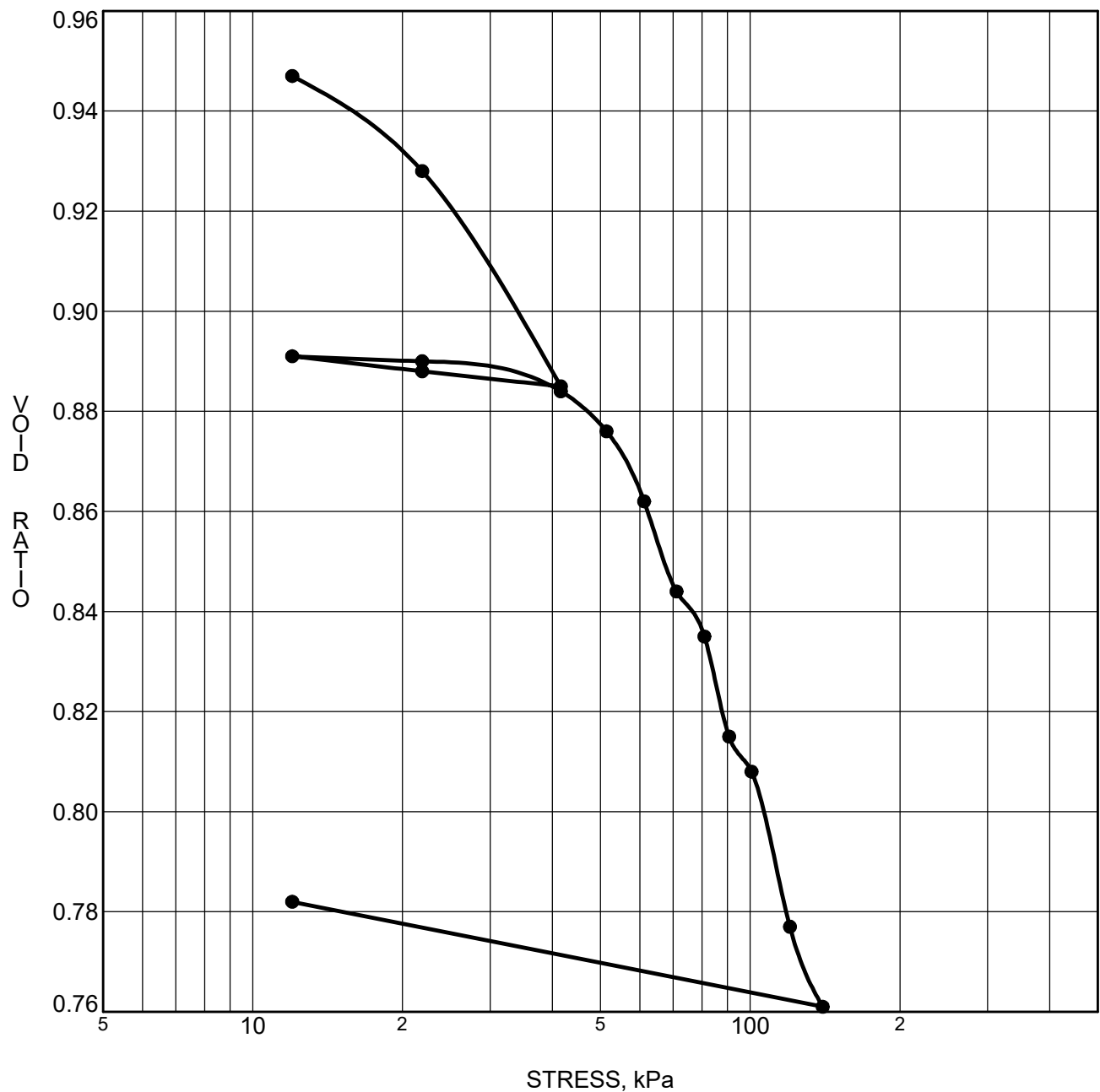
CAN NO.	5	5
WT. OF CAN	19.94	19.35
WT. OF SOIL & CAN	28.87	28.11
WT. OF DRY SOIL & CAN	27.64	26.90
WT. OF MOISTURE	1.23	1.21
WT. OF DRY SOIL & CAN	7.7	7.55
WATER CONTENT, w, %	15.97	16.03

RESULTS	
LIQUID LIMIT	27
PLASTIC LIMIT	16
PLASTICITY INDEX	11



TECHNICIAN: CP		C. Beadow	J. Forsyth, P. Eng.
	REVIEWED BY:		

				Linear Shrinkage ASTM D4943-02					
CLIENT:	First Capital Realty	DEPTH	10' - 12'	FILE NO.:	PG7751				
PROJECT:	375 Didsbudry Road	BH OR TP No:	BH8-25 SS4	DATE SAMPLED	03-Nov				
LAB No:	64302	TESTED BY:	CP	DATE RECEIVED	06-Nov				
SAMPLED BY:	A.E	DATE REPORTED:	12-Nov-25	DATE TESTED	06-Nov				
LABORATORY INFORMATION & TEST RESULTS									
Moisture		No. of Blows(5)	Calibration (Two Trials)		Tin NO.(x24)				
Tare	5.07		Tin	4.75	4.75				
Soil Pat Wet + Tare	79.66		Tin + Grease	5.08	5.08				
Soil Pat Wet	74.59		Glass	43.23	43.22				
Soil Pat Dry + Tare	63.04		Tin + Glass + Water	85.32	85.32				
Soil Pat Dry	57.97		Volume	37.01	37.02				
Moisture	28.67		Average Volume	37.02					
Soil Pat + String Soil Pat + Wax + String in Air Soil Pat + Wax + String in Water Volume Of Pat (Vdx)			<table border="1"> <tr><td>58.30</td></tr> <tr><td>64.06</td></tr> <tr><td>28.45</td></tr> <tr><td>35.61</td></tr> </table>			58.30	64.06	28.45	35.61
58.30									
64.06									
28.45									
35.61									
RESULTS:									
Shrinkage Limit Shrinkage Ratio Volumetric Shrinkage Linear Shrinkage			<table border="1"> <tr><td>15.08</td></tr> <tr><td>1.989</td></tr> <tr><td>27.033</td></tr> <tr><td>7.665</td></tr> </table>			15.08	1.989	27.033	7.665
15.08									
1.989									
27.033									
7.665									
REVIEWED BY:	Curtis Beadow		Joe Forsyth, P. Eng.						
									
Paterson Group Inc., 28 Concourse Gate, Unit 6, Ottawa, Ontario, K2E 7T7									



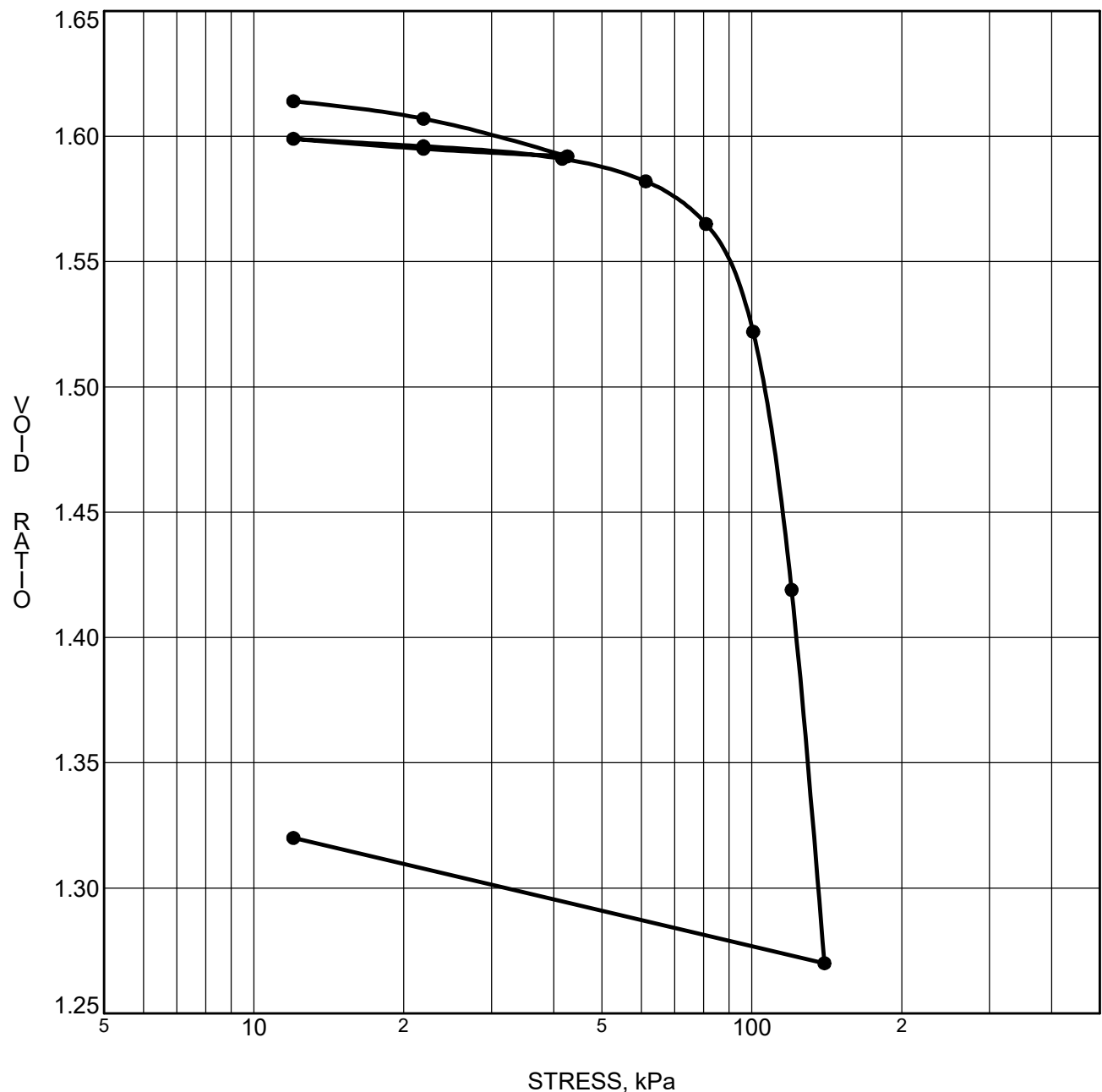
CONSOLIDATION TEST DATA SUMMARY					
Borehole No.	BH 21-25	p'_o	49.9 kPa	C_{cr}	0.013
Sample No.	TW5	p'_c	76.4 kPa	C_c	0.329
Sample Depth	4.57 m	OC Ratio	1.5	W_o	35.5 %
Sample Elev.	88.76 m	Void Ratio	0.977	Unit Wt.	18.5 kN/m³

CLIENT First Capital Realty Inc.
 PROJECT Geotechnical Investigation
375 Didsbury Road, Ottawa, Ontario

FILE NO. PG7751
 DATE 2025/11/18

patersongroup Consulting Engineers
 9 Auriga Drive, Ottawa, Ontario K2E 7T9

**CONSOLIDATION
TEST**



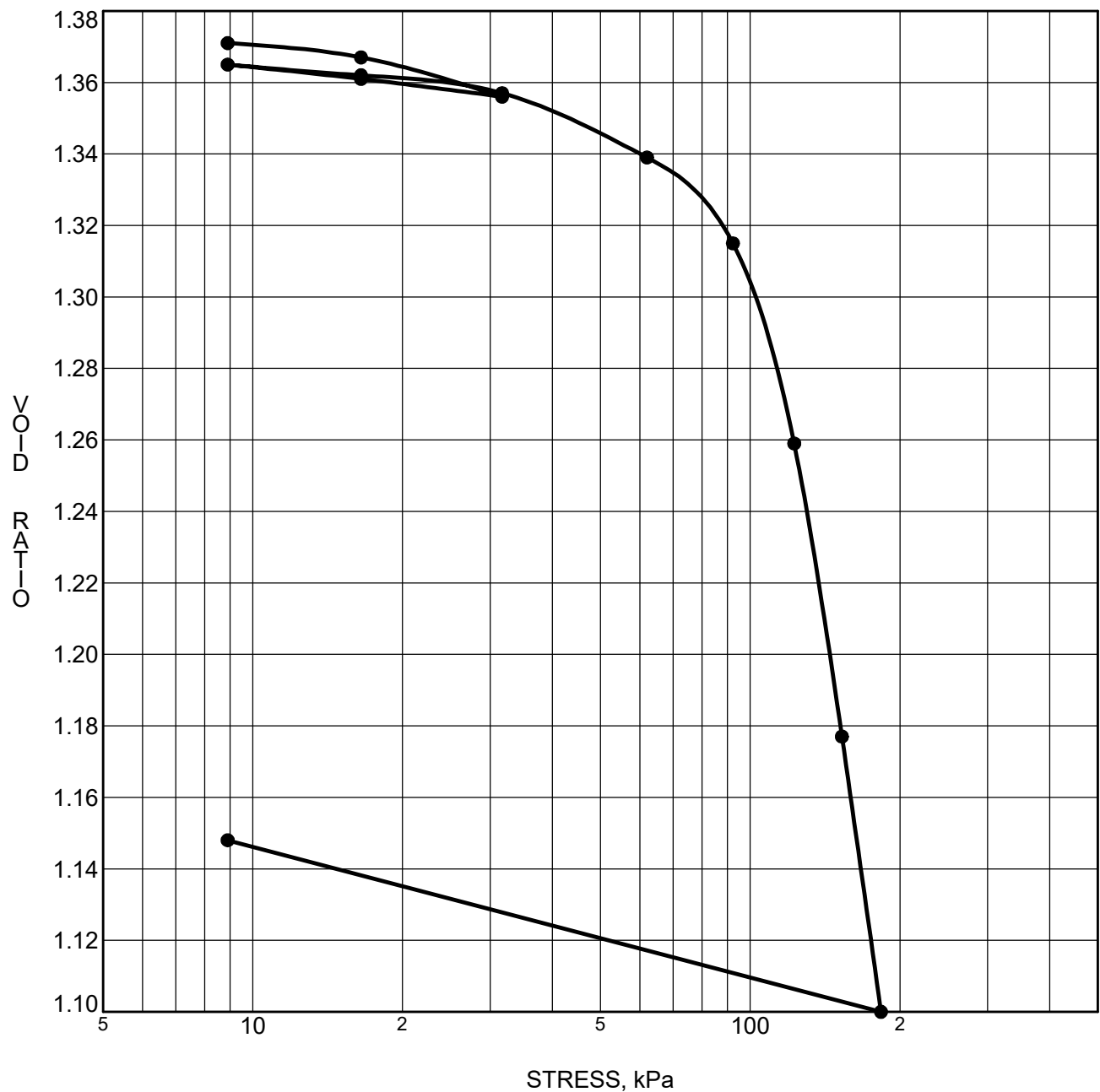
CONSOLIDATION TEST DATA SUMMARY					
Borehole No.	BH 23-25	p'_o	54.19 kPa	C_{cr}	0.014
Sample No.	TW7	p'_c	99.67 kPa	C_c	1.867
Sample Depth	5.33 m	OC Ratio	1.8	W_o	59.1 %
Sample Elev.	87.97 m	Void Ratio	1.625	Unit Wt.	16.4 kN/m ³

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375 Didsbury Road, Ottawa, Ontario

FILE NO. PG7751
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**CONSOLIDATION
TEST**



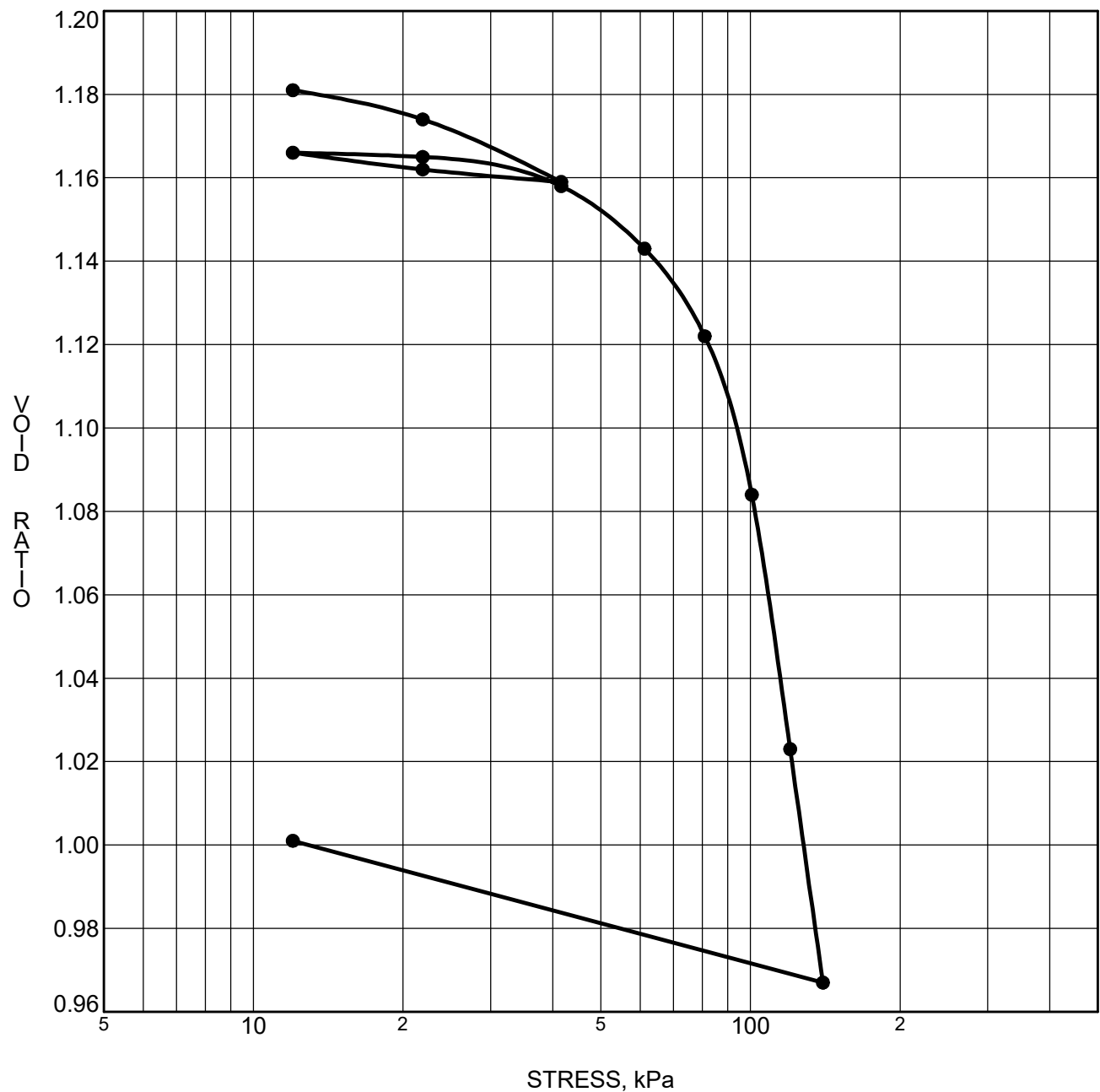
CONSOLIDATION TEST DATA SUMMARY					
Borehole No.	BH 25-25	p'_o	63.39 kPa	C_{cr}	0.015
Sample No.	TW4	p'_c	105.02 kPa	C_c	0.940
Sample Depth	6.86 m	OC Ratio	1.7	W_o	49.9 %
Sample Elev.	86.61 m	Void Ratio	1.373	Unit Wt.	kN/m ³

CLIENT First Capital Realty Inc.
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375 Didsbury Road, Ottawa, Ontario

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**CONSOLIDATION
TEST**



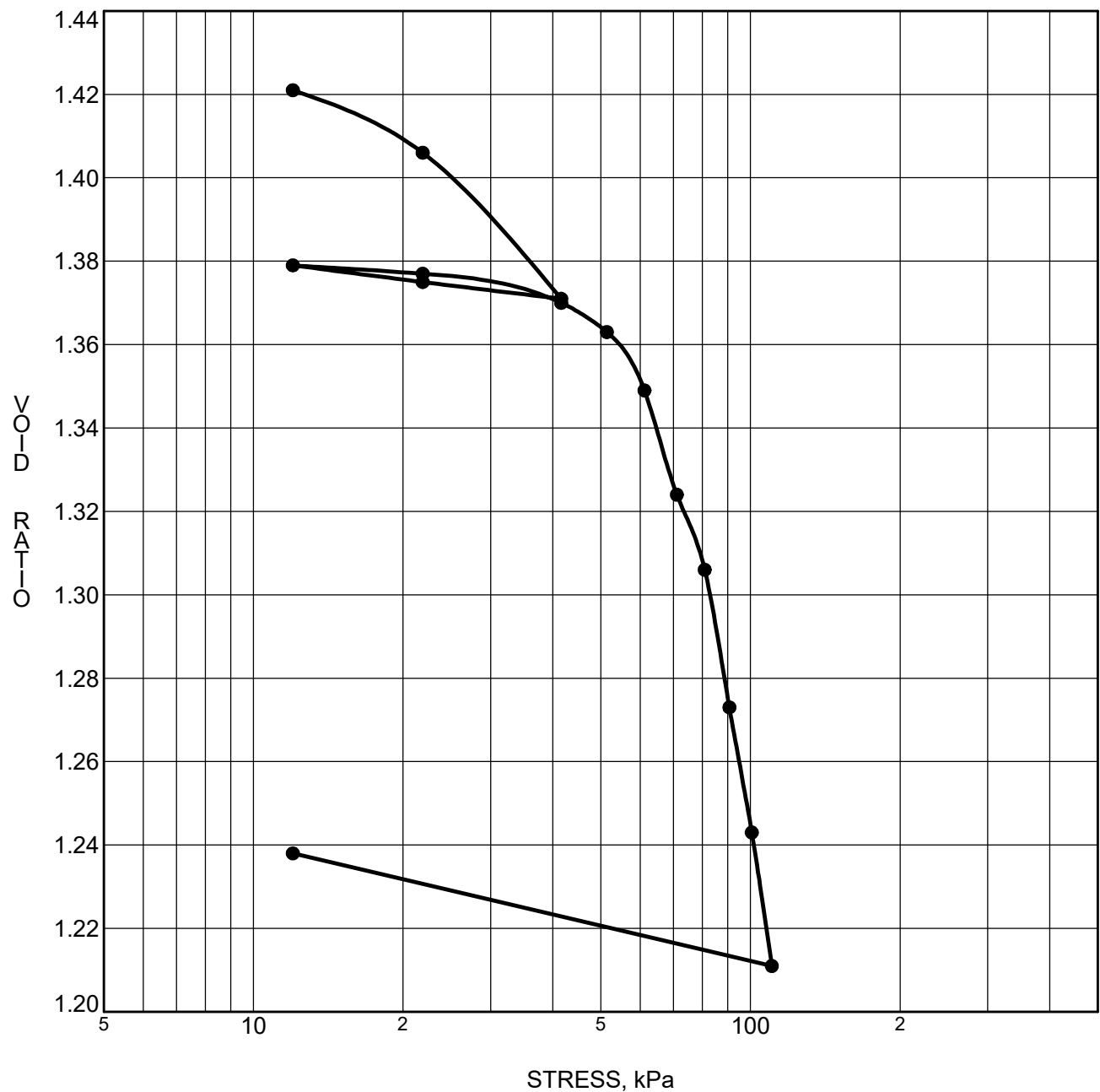
CONSOLIDATION TEST DATA SUMMARY					
Borehole No.	BH 31-25	p'_o	41.77 kPa	C_{cr}	0.015
Sample No.	TW4	p'_c	90 kPa	C_c	0.816
Sample Depth	3.81 m	OC Ratio	2.2	W_o	43.4 %
Sample Elev.	89.77 m	Void Ratio	1.192	Unit Wt.	17.6 kN/m³

CLIENT First Capital Realty Inc.
 PROJECT Geotechnical Investigation
375 Didsbury Road, Ottawa, Ontario

FILE NO. PG7751
 DATE 2025/12/02

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**CONSOLIDATION
TEST**



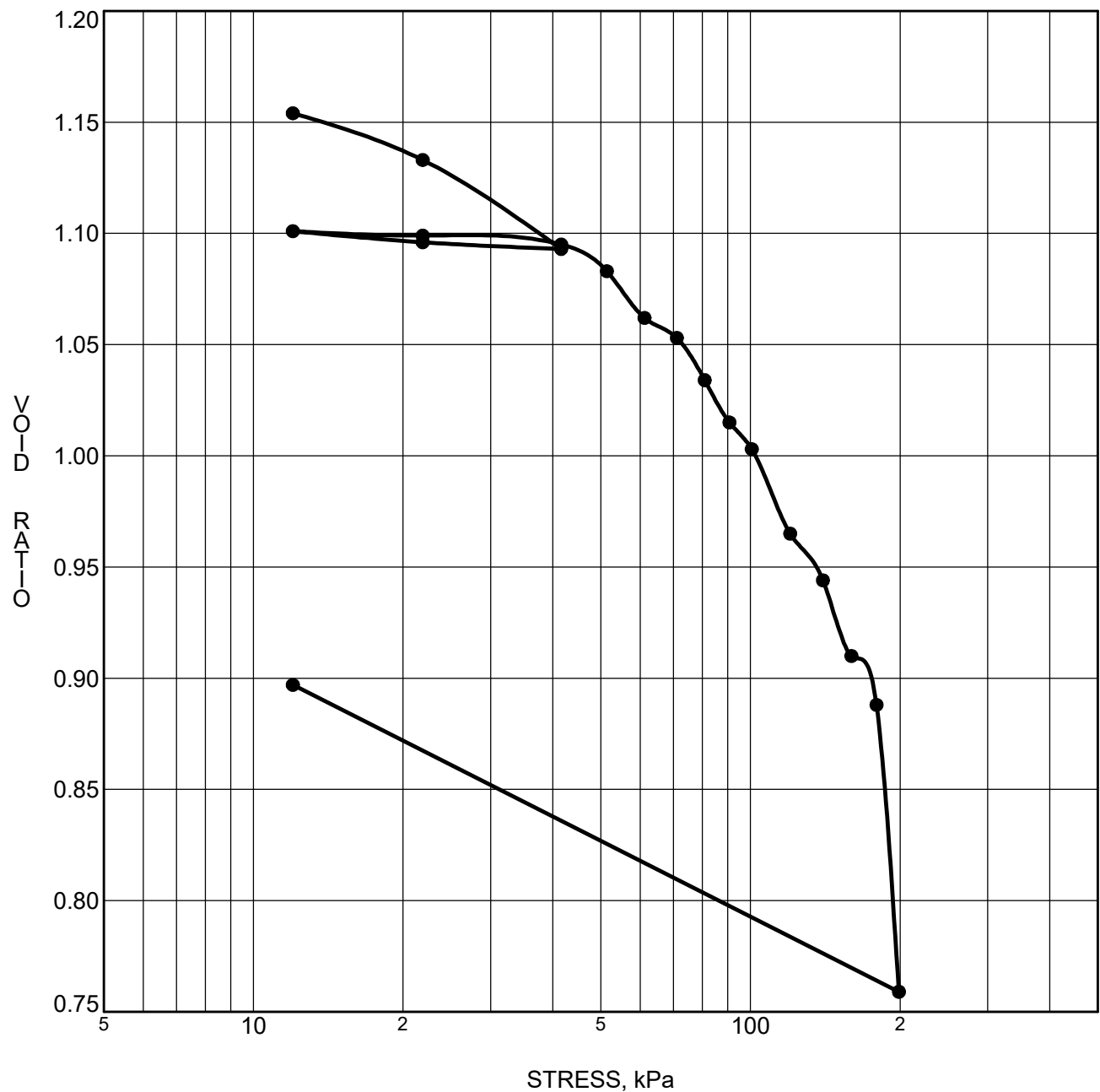
CONSOLIDATION TEST DATA SUMMARY					
Borehole No.	BH 32-25	p' _o	53.12 kPa	C _{cr}	0.018
Sample No.	TW5	p' _c	75.91 kPa	C _c	0.710
Sample Depth	4.57 m	OC Ratio	1.4	W _o	52.4 %
Sample Elev.	89.32 m	Void Ratio	1.441	Unit Wt.	16.8 kN/m ³

CLIENT First Capital Realty Inc.
 PROJECT Geotechnical Investigation
375 Didsbury Road, Ottawa, Ontario

FILE NO. PG7751
 DATE 2026/12/14

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**CONSOLIDATION
TEST**



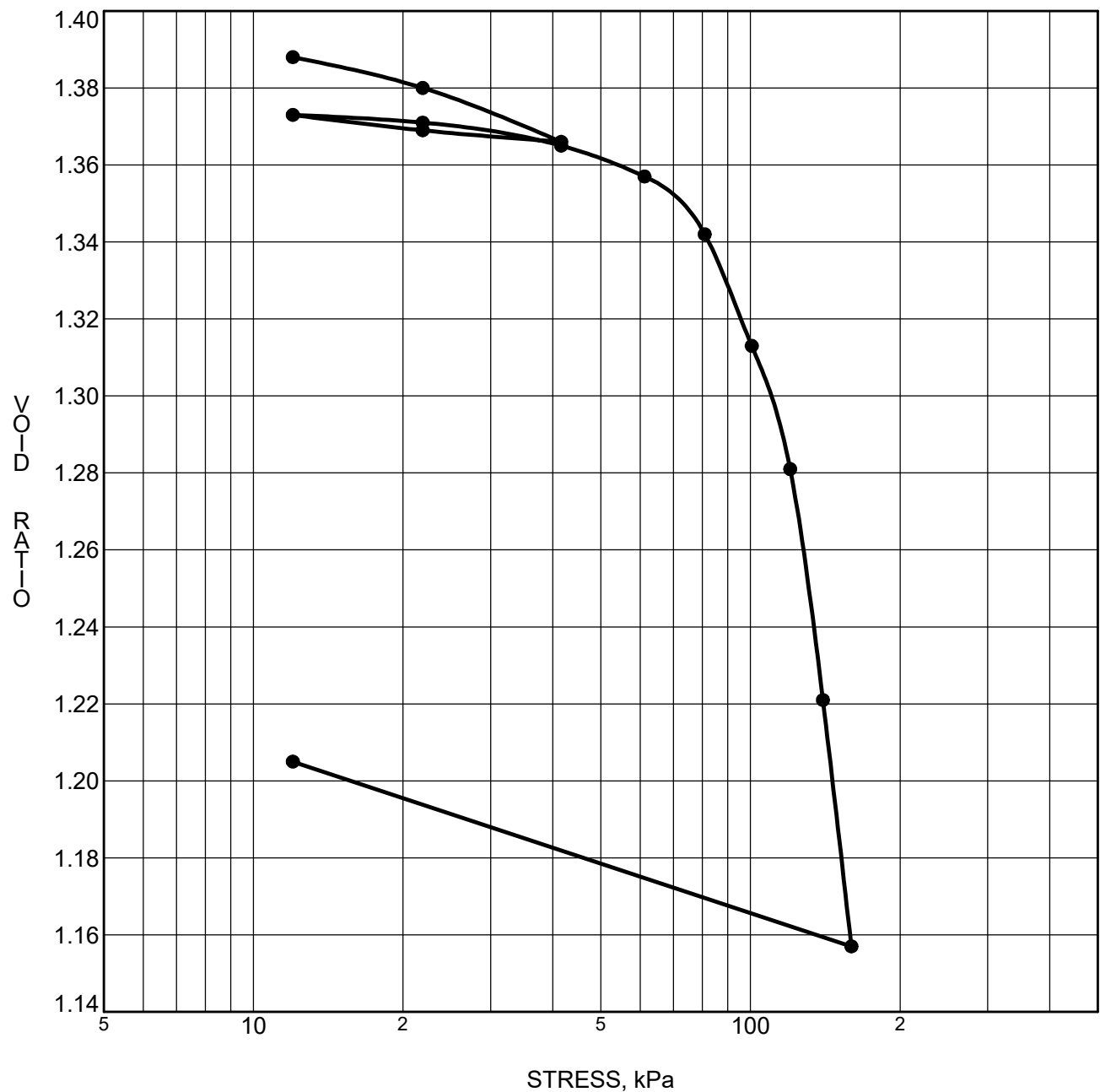
CONSOLIDATION TEST DATA SUMMARY					
Borehole No.	BH 33-25	p'_o	67.28 kPa	C_{cr}	0.015
Sample No.	TW8	p'_c	100 kPa	C_c	0.526
Sample Depth	7.62 m	OC Ratio	1.5	W_o	43.1 %
Sample Elev.	85.92 m	Void Ratio	1.186	Unit Wt.	17.7 kN/m ³

CLIENT First Capital Realty Inc.
 PROJECT Geotechnical Investigation
375 Didsbury Road, Ottawa, Ontario

FILE NO. PG7751
 DATE 2025/12/09

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**CONSOLIDATION
TEST**



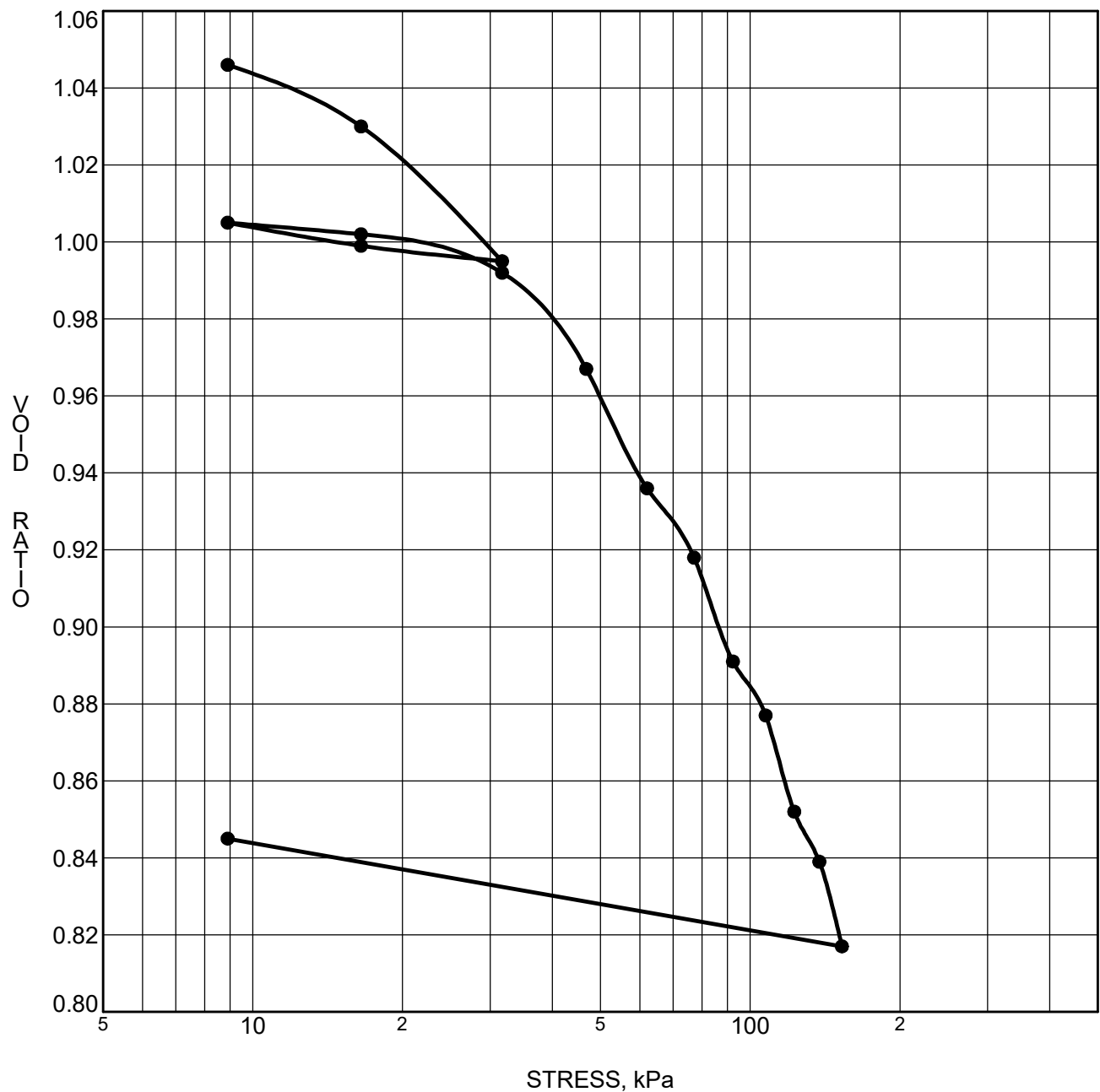
CONSOLIDATION TEST DATA SUMMARY					
Borehole No.	BH 34-25	p'_o	58.89 kPa	C_{cr}	0.016
Sample No.	TW4	p'_c	110.37 kPa	C_c	1.015
Sample Depth	6.10 m	OC Ratio	1.9	W_o	50.9 %
Sample Elev.	86.77 m	Void Ratio	1.4	Unit Wt.	17.0 kN/m ³

CLIENT First Capital Realty Inc.
 PROJECT Geotechnical Investigation
375 Didsbury Road, Ottawa, Ontario

FILE NO. PG7751
 DATE 2025/12/09

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 9 Auriga Drive, Ottawa, Ontario K2E 7T9

**CONSOLIDATION
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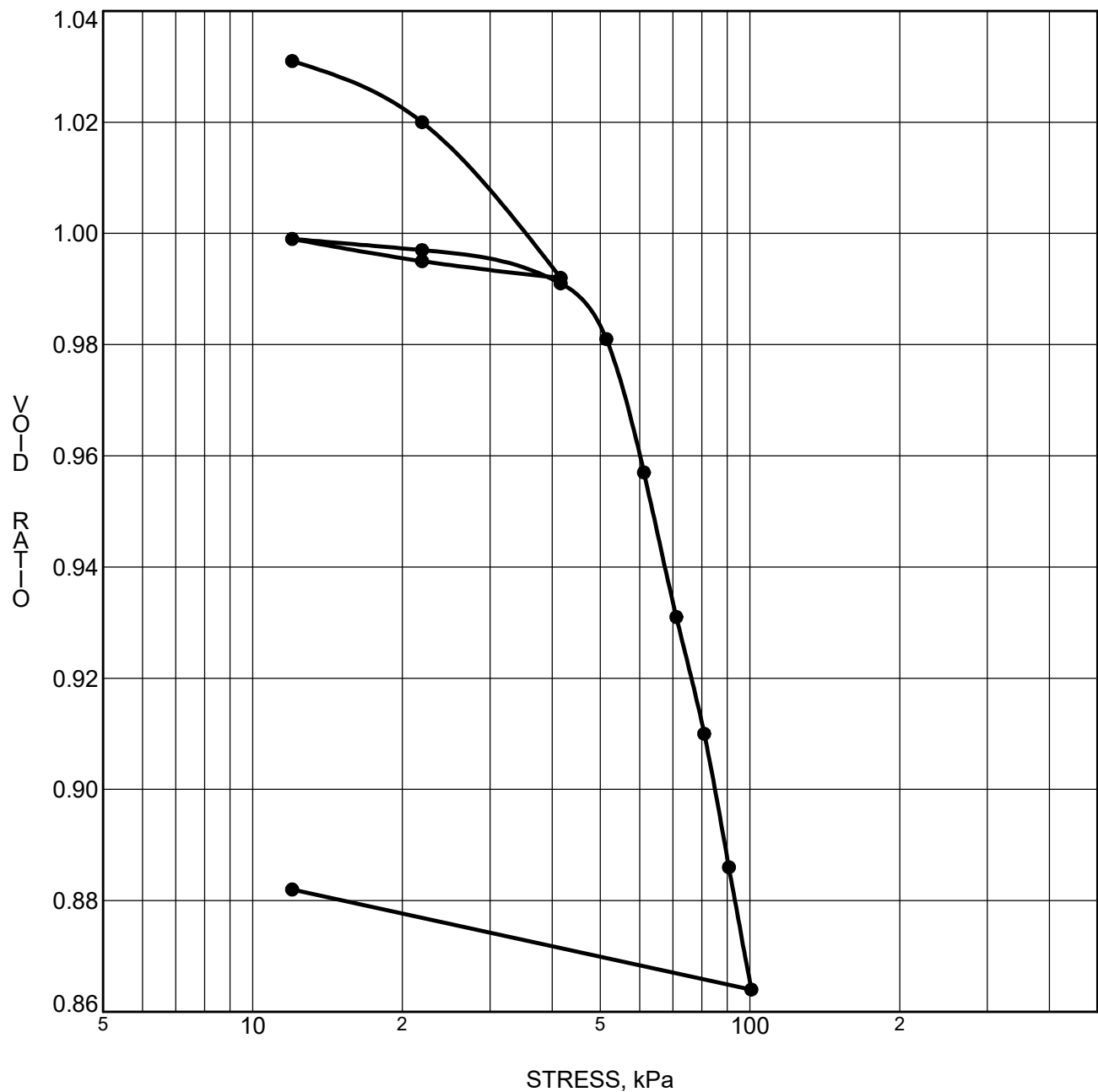
CONSOLIDATION TEST DATA SUMMARY					
Borehole No.	BH 35-25	p' _o	31.83 kPa	C _{cr}	0.025
Sample No.	TW4	p' _c	61.27 kPa	C _c	0.351
Sample Depth	3.05 m	OC Ratio	1.9	W _o	38.7 %
Sample Elev.	89.82 m	Void Ratio	1.065	Unit Wt.	18.1 kN/m ³

CLIENT First Capital Realty Inc.
 PROJECT Geotechnical Investigation
375 Didsbury Road, Ottawa, Ontario

FILE NO. PG7751
 DATE 2025/12/09

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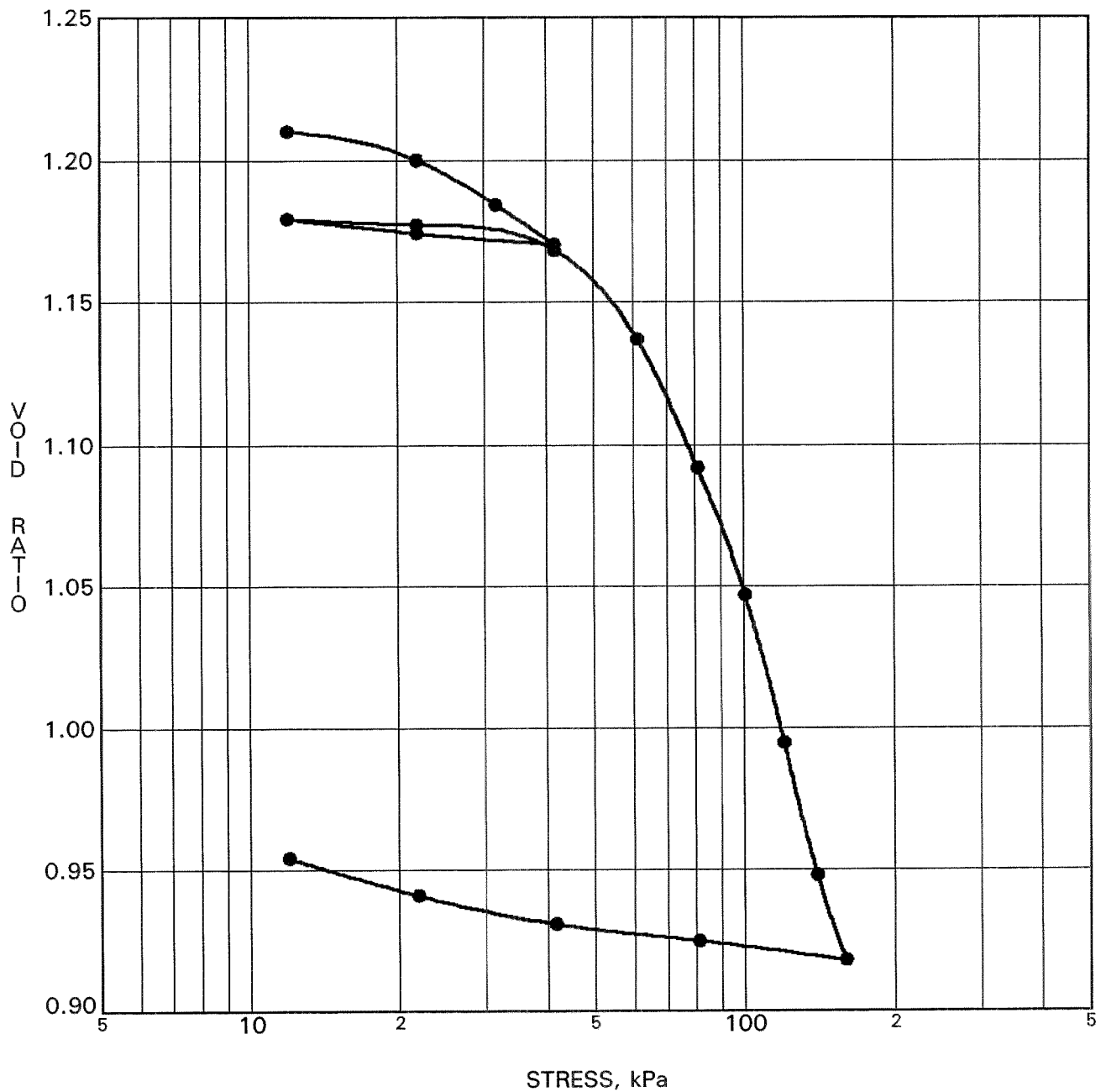
CONSOLIDATION TEST DATA SUMMARY					
Borehole No.	BH 38-25	p'_{o}	62.95 kPa	C_{cr}	0.014
Sample No.	TW7	p'_{c}	64.14 kPa	C_c	0.470
Sample Depth	4.57 m	OC Ratio	1.0	W_o	38.0 %
Sample Elev.	89.72 m	Void Ratio	1.044	Unit Wt.	18.2 kN/m ³

CLIENT First Capital Realty Inc.
 PROJECT Geotechnical Investigation
375 Didsbury Road, Ottawa, Ontario

FILE NO. PG7751
 DATE 2026/01/14

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**CONSOLIDATION
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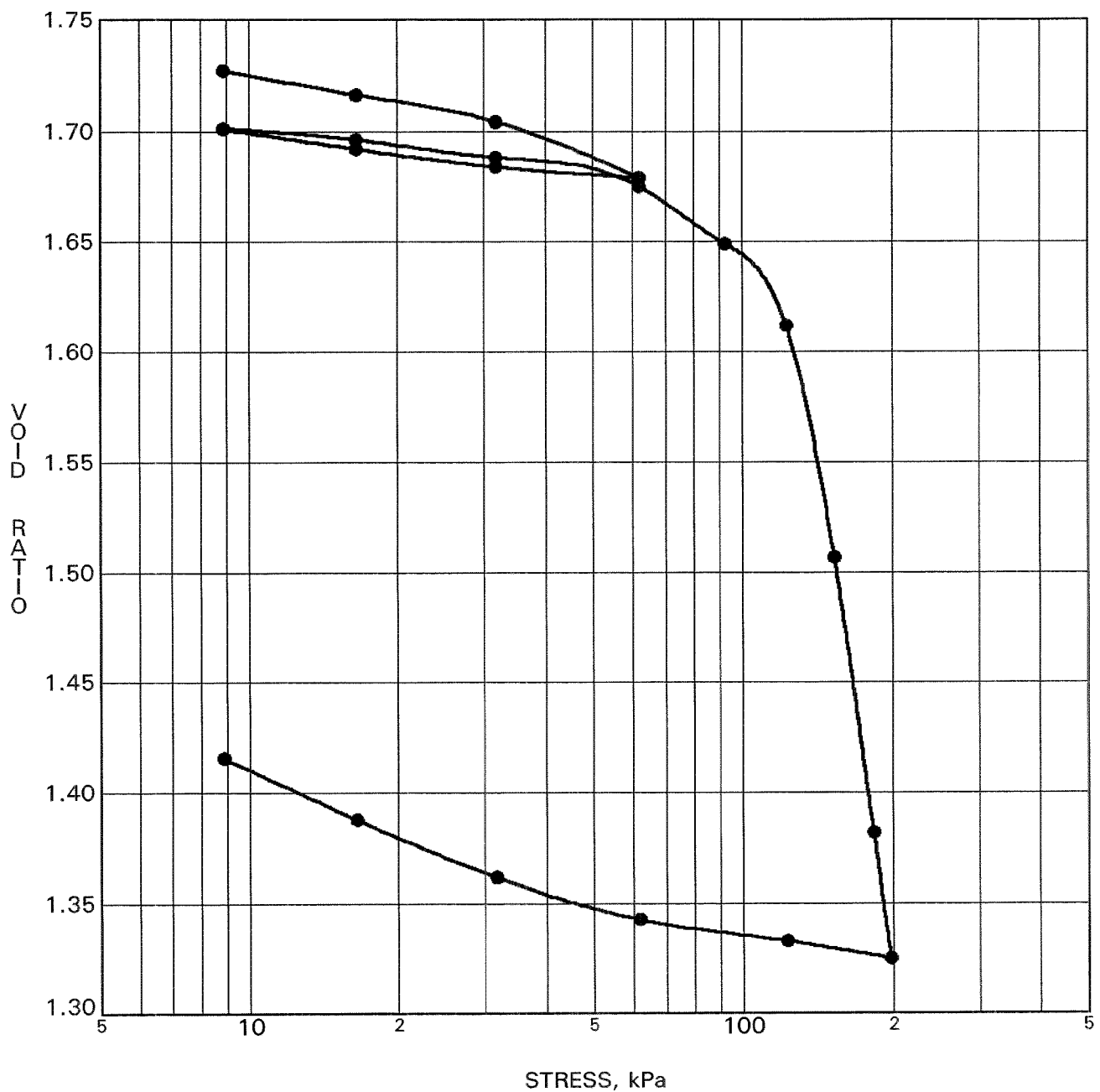
CONSOLIDATION TEST DATA SUMMARY					
Borehole No.	BH 1	p'_o	37 kPa	C_{cr}	0.020
Sample No.	TW 1	p'_c	73 kPa	C_c	0.640
Sample Depth	2.70 m	OC Ratio	2.0	W_o	62.8 %
Sample Elev.	90.30 m	Void Ratio	1.730	Unit Wt.	17.5 kN/m ³

CLIENT Rona Inc. c/o Gross Kaplin Conviensky Architects
 PROJECT Geotechnical Investigation - Proposed
Commercial Development, Didsbury Road

FILE NO. PG0475
 DATE 19/11/04

patersongroup Consulting Engineers
 28 Concourse Gate, Unit 1, Ottawa, Ontario K2E 7T7

CONSOLIDATION TEST



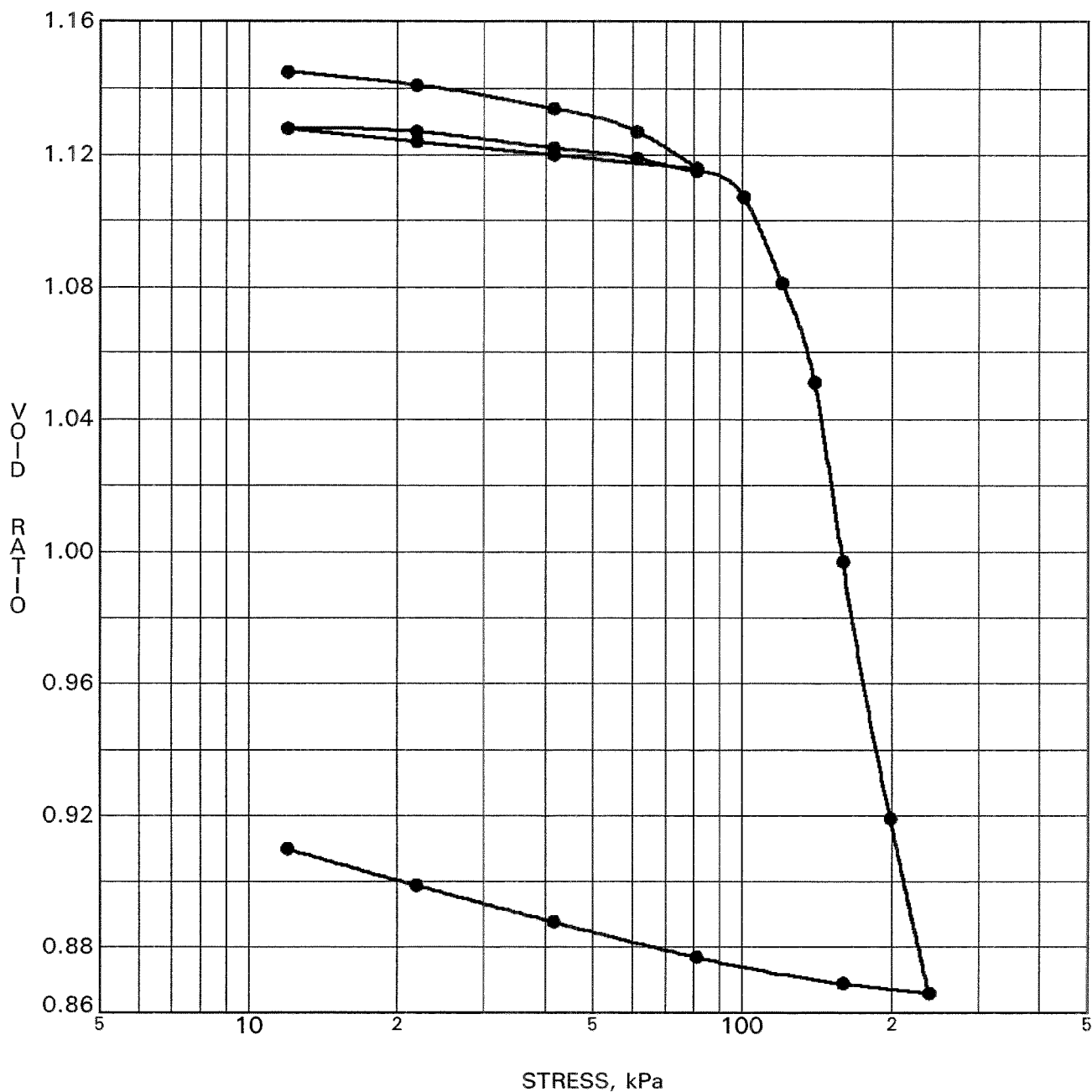
CONSOLIDATION TEST DATA SUMMARY					
Borehole No.	BH 1	p'_o	112 kPa	C_{cr}	0.029
Sample No.	TW 3	p'_c	123 kPa	C_c	1.600
Sample Depth	12.50 m	OC Ratio	1.1	W_o	63.3 %
Sample Elev.	80.50 m	Void Ratio	1.740	Unit Wt.	16.1 kN/m ³

CLIENT Rona Inc. c/o Gross Kaplin Conviensky Architects
 PROJECT Geotechnical Investigation - Proposed
Commercial Development, Didsbury Road

FILE NO. PG0475
 DATE 19/11/04

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 28 Concourse Gate, Unit 1, Ottawa, Ontario K2E 7T7

CONSOLIDATION TEST



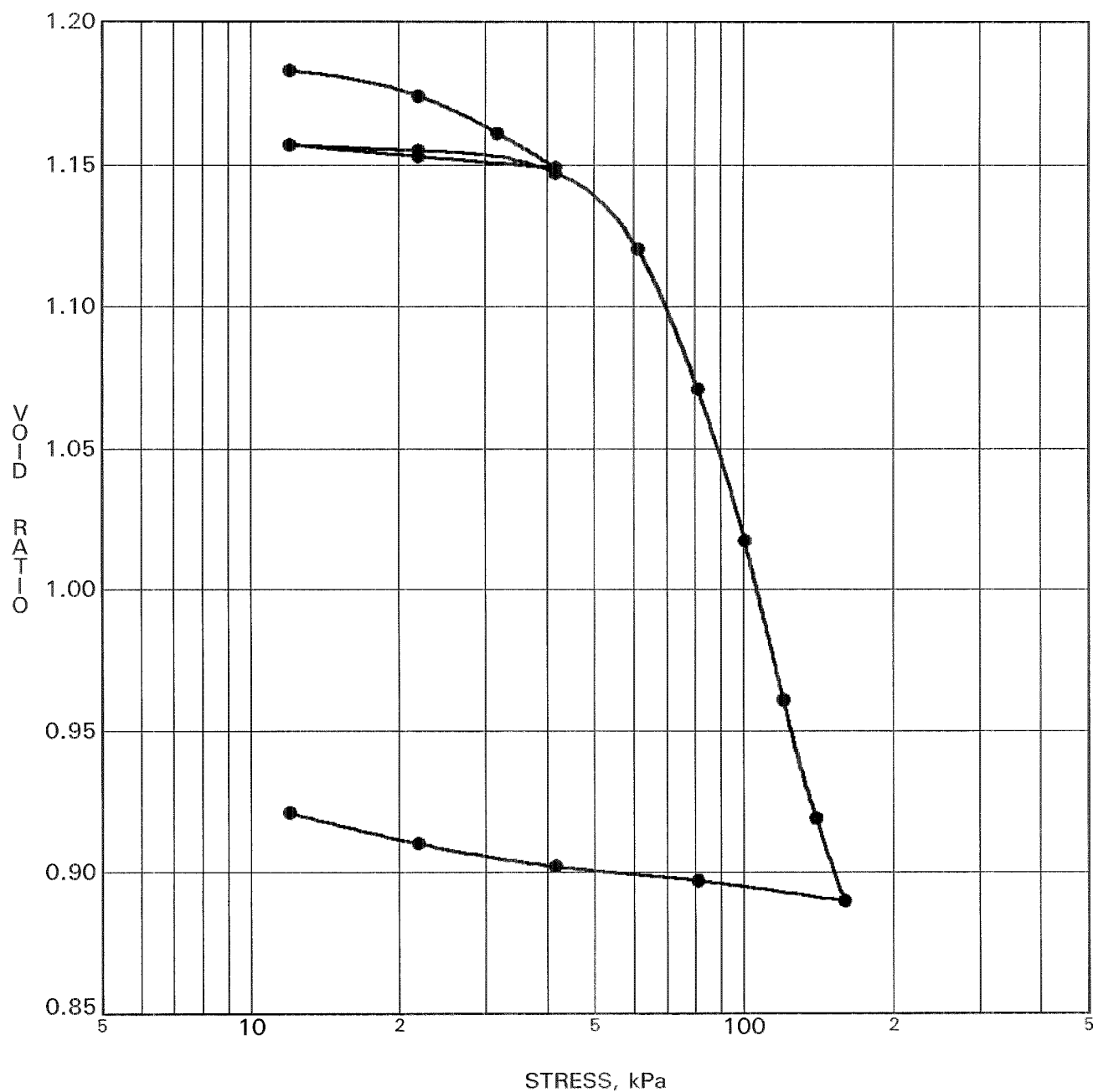
CONSOLIDATION TEST DATA SUMMARY					
Borehole No.	BH 2	p'_o	54 kPa	C_{cr}	0.014
Sample No.	TW 1	p'_c	122 kPa	C_c	0.799
Sample Depth	5.00 m	OC Ratio	2.3	W_o	41.9 %
Sample Elev.	88.04 m	Void Ratio	1.150	Unit Wt.	17.8 kN/m ³

CLIENT Rona Inc. c/o Gross Kaplin Conviensky Architects
 PROJECT Geotechnical Investigation - Proposed
Commercial Development, Didsbury Road

FILE NO. PG0475
 DATE 06/12/04

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 28 Concourse Gate, Unit 1, Ottawa, Ontario K2E 7T7

**CONSOLIDATION
TEST**



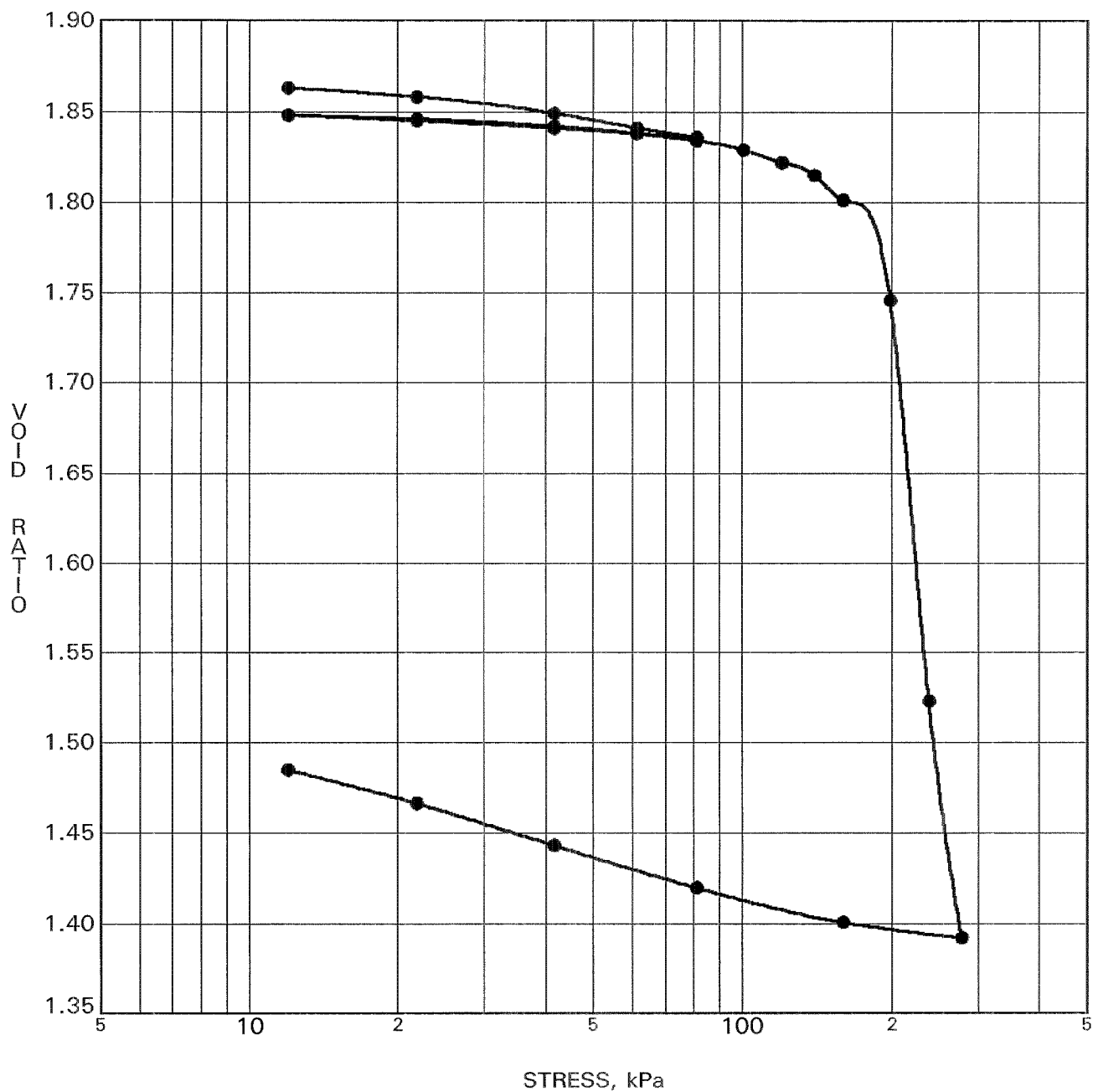
CONSOLIDATION TEST DATA SUMMARY					
Borehole No.	BH 5	p'_o	64 kPa	C_{cr}	0.016
Sample No.	TW 1	p'_c	69 kPa	C_c	0.630
Sample Depth	6.35 m	OC Ratio	1.1	W_o	43.8 %
Sample Elev.	88.01 m	Void Ratio	1.200	Unit Wt.	17.6 kN/m ³

CLIENT Rona Inc. c/o Gross Kaplin Conviensky Architects
 PROJECT Geotechnical Investigation - Proposed
Commercial Development, Didsbury Road

FILE NO. PG0475
 DATE 19/11/04

patersongroup Consulting Engineers
 28 Concourse Gate, Unit 1, Ottawa, Ontario K2E 7T7

CONSOLIDATION TEST



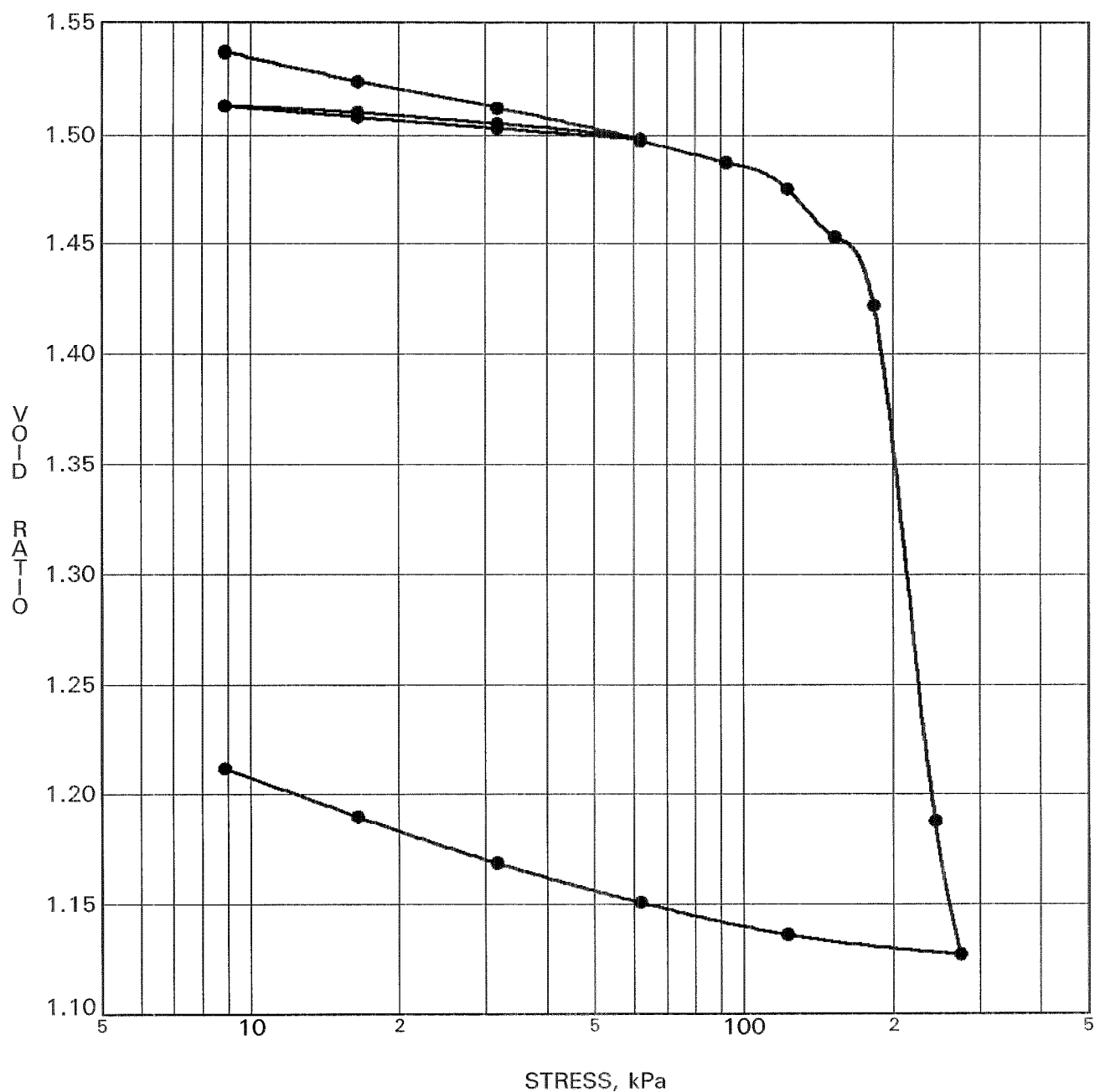
CONSOLIDATION TEST DATA SUMMARY					
Borehole No.	BH 9	p'_o	73 kPa	C_{cr}	0.013
Sample No.	TW 1	p'_c	191 kPa	C_c	2.460
Sample Depth	7.20 m	OC Ratio	2.6	W_o	68.1 %
Sample Elev.	86.72 m	Void Ratio	1.870	Unit Wt.	15.8 kN/m ³

CLIENT Rona Inc. c/o Gross Kaplin Conviensky Architects
 PROJECT Geotechnical Investigation - Proposed
Commercial Development, Didsbury Road

FILE NO. PG0475
 DATE 06/12/04

patersongroup Consulting Engineers
 28 Concourse Gate, Unit 1, Ottawa, Ontario K2E 7T7

**CONSOLIDATION
TEST**



CONSOLIDATION TEST DATA SUMMARY					
Borehole No.	BH 9	p'_o	91 kPa	C_{cr}	0.018
Sample No.	TW 2	p'_c	174 kPa	C_c	1.680
Sample Depth	9.50 m	OC Ratio	1.9	W_o	56.1 %
Sample Elev.	84.42 m	Void Ratio	1.540	Unit Wt.	16.6 kN/m ³

CLIENT Rona Inc. c/o Gross Kaplin Conviensky Architects
 PROJECT Geotechnical Investigation - Proposed
Commercial Development, Didsbury Road

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patersongroup Consulting Engineers
 28 Concourse Gate, Unit 1, Ottawa, Ontario K2E 7T7

CONSOLIDATION TEST



Your Project #: PG 7751
Site Location: 375 DIDSBURY RD
Your C.O.C. #: N/A

Attention: Otilia McLaughlin

Paterson Group
9 Auriga Drive
Ottawa, ON
Canada K2E 7T9

Report Date: 2025/12/16
Report #: R8669566
Version: 1 - Final

CERTIFICATE OF ANALYSIS

BUREAU VERITAS JOB #: C5F0314

Received: 2025/11/26, 13:00

Sample Matrix: Soil
Samples Received: 9

Analyses	Quantity	Date Extracted	Date Analyzed	Laboratory Method	Analytical Method
Chloride (20:1 extract) (1)	9	2025/12/02	2025/12/03	CAM SOP-00463	MOE E3013 m
Conductivity (1)	9	2025/12/02	2025/12/02	CAM SOP-00414	OMOE E3530 v1 m
Acid Extractable Metals by ICPMS (1)	9	2025/12/01	2025/12/01	CAM SOP-00447	EPA 6020B m
Acid Extractable Metals Analysis by ICP (1)	9	2025/12/01	2025/12/02	CAM SOP-00408	EPA 6010D m
Chloride (soluble) (2)	5	2025/12/11	2025/12/11	AB SOP-00033 / AB SOP-00020	SM 24-4500-Cl-E m
Chloride (soluble) (2)	2	2025/12/05	2025/12/05	AB SOP-00033 / AB SOP-00020	SM 24-4500-Cl-E m
Chloride (soluble) (2)	2	2025/12/05	2025/12/07	AB SOP-00033 / AB SOP-00020	SM 24-4500-Cl-E m
Conductivity @25C (Soluble) (2)	5	2025/12/11	2025/12/11	AB SOP-00033 / AB SOP-00004	SM 24 2510 B m
Conductivity @25C (Soluble) (2)	4	2025/12/05	2025/12/06	AB SOP-00033 / AB SOP-00004	SM 24 2510 B m
Loss on Ignition (3, 4)	9	2025/12/01	2025/12/01	BBY6SOP-00040	Carter 2nd ed 28.3
Moisture (Subcontracted) (2, 5)	9	N/A	2025/12/03	AB SOP-00002	CCME PHC-CWS m
Organic Matter - Calculated from LOI (3)	9	2025/11/27	2025/12/01	BBY WI-00033	Auto Calc
pH @ 25C (1:2 Calcium Chloride Extract) (2)	5	2025/12/11	2025/12/11	CAL SOP-00180 / AB SOP-00006	SM 24 4500 H+B m
pH @ 25C (1:2 Calcium Chloride Extract) (2)	4	2025/12/05	2025/12/05	CAL SOP-00180 / AB SOP-00006	SM 24 4500 H+B m
Sodium Adsorption Ratio (SAR) (2)	5	N/A	2025/12/12	AB SOP-00065	Auto Calc
Sodium Adsorption Ratio (SAR) (2)	2	N/A	2025/12/06	AB SOP-00065	Auto Calc
Sodium Adsorption Ratio (SAR) (2)	2	N/A	2025/12/07	AB SOP-00065	Auto Calc
Soluble Ions (2)	5	2025/12/11	2025/12/11	AB SOP-00033 / AB SOP-00042	EPA 6010d R5 m
Soluble Ions (2)	2	2025/12/05	2025/12/06	AB SOP-00033 / AB SOP-00042	EPA 6010d R5 m
Soluble Ions (2)	2	2025/12/05	2025/12/07	AB SOP-00033 / AB SOP-00042	EPA 6010d R5 m
Sulphide in Soil (2)	9	N/A	2025/12/04	AB SOP-00080	EPA9030B/SM4500S2-DF
Soluble Paste (2)	5	2025/12/11	2025/12/11	AB SOP-00033	Carter 2nd ed 15.2 m
Soluble Paste (2)	4	2025/12/05	2025/12/05	AB SOP-00033	Carter 2nd ed 15.2 m



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Sample Matrix: Soil
Samples Received: 9

Analyses	Date		Date Analyzed	Laboratory Method	Analytical Method
	Quantity	Extracted			
Soluble Boron Calculation (2)	5	N/A	2025/12/12		Auto Calc
Soluble Boron Calculation (2)	2	N/A	2025/12/06		Auto Calc
Soluble Boron Calculation (2)	2	N/A	2025/12/07		Auto Calc
Soluble Ions Calculation (2)	9	N/A	2025/12/03		Auto Calc
pH CaCl ₂ EXTRACT (1)	9	2025/12/02	2025/12/02	CAM SOP-00413	EPA 9045 D m
Redox Potential (1, 6)	9	2025/12/03	2025/12/06	CAM SOP-00421	SM 24 2580 B
Resistivity of Soil (1)	9	2025/11/27	2025/12/02	CAM SOP-00414	SM 24 2510 m
Sodium Adsorption Ratio (SAR) (1)	9	N/A	2025/12/16	CAM SOP-00102	EPA 6010C
Sulphate (20:1 Extract) (1)	9	2025/12/02	2025/12/03	CAM SOP-00464	MOE E3013 m

Remarks:

Bureau Veritas is accredited to ISO/IEC 17025 for specific parameters on scopes of accreditation. Unless otherwise noted, procedures used by Bureau Veritas are based upon recognized Provincial, Federal or US method compendia such as CCME, EPA, APHA or the Quebec Ministry of Environment.

All work recorded herein has been done in accordance with procedures and practices ordinarily exercised by professionals in Bureau Veritas' profession using accepted testing methodologies, quality assurance and quality control procedures (except where otherwise agreed by the client and Bureau Veritas in writing). All data is in statistical control and has met quality control and method performance criteria unless otherwise noted. All method blanks are reported; unless indicated otherwise, associated sample data are not blank corrected. Where applicable, unless otherwise noted, Measurement Uncertainty has not been accounted for when stating conformity to the referenced standard.

Bureau Veritas liability is limited to the actual cost of the requested analyses, unless otherwise agreed in writing. There is no other warranty expressed or implied. Bureau Veritas has been retained to provide analysis of samples provided by the Client using the testing methodology referenced in this report. Interpretation and use of test results are the sole responsibility of the Client and are not within the scope of services provided by Bureau Veritas, unless otherwise agreed in writing. Bureau Veritas is not responsible for the accuracy or any data impacts, that result from the information provided by the customer or their agent.

Solid sample results, except biota, are based on dry weight unless otherwise indicated. Organic analyses are not recovery corrected except for isotope dilution methods.

Results relate to samples tested. When sampling is not conducted by Bureau Veritas, results relate to the supplied samples tested.

This Certificate shall not be reproduced except in full, without the written approval of the laboratory.

Reference Method suffix "m" indicates test methods incorporate validated modifications from specific reference methods to improve performance.

* RPDs calculated using raw data. The rounding of final results may result in the apparent difference.

(1) This test was performed by Bureau Veritas Mississauga, 6740 Campobello Rd , Mississauga, ON, L5N 2L8

(2) This test was performed by Bureau Veritas Calgary (19th), 4000 19th Street NE , Calgary, AB, T2E 6P8

(3) This test was performed by Bureau Veritas Burnaby, 4606 Canada Way , Burnaby, BC, V5G 1K5



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- (4) Loss on Ignition was reported on a dry weight basis.
- (5) Offsite analysis requires that subcontracted moisture be reported.
- (6) Oxidation-Reduction Potential (ORP) values are determined using a Ag/AgCl reference electrode. The test is therefore, not SCC accredited for this matrix.

Encryption Key

Please direct all questions regarding this Certificate of Analysis to:

Katherine Szozda, Project Manager
Email: Katherine.Szozda@bureauveritas.com
Phone# (613)274-0573 Ext:7063633

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This report has been generated and distributed using a secure automated process.

Bureau Veritas has procedures in place to guard against improper use of the electronic signature and have the required "signatories", as per ISO/IEC 17025, signing the reports. For Service Group specific validation, please refer to the Validation Signatures page if included, otherwise available by request. For Department specific Analyst/Supervisor validation names, please refer to the Test Summary section if included, otherwise available by request. This report is authorized by Rodney Major, General Manager responsible for Ontario Environmental laboratory operations.

**SOIL CORROSIVITY PACKAGE (SOIL)**

Bureau Veritas ID		AXTU15	AXTU16	AXTU17		
Sampling Date		2025/11/21 10:00	2025/11/21 10:00	2025/11/21 10:00		
COC Number		N/A	N/A	N/A		
	UNITS	TP1-25-G1-150MM	TP1-25-G2-300MM	TP1-25-G3-450MM	RDL	QC Batch
Calculated Parameters						
Resistivity	ohm-cm	750	3200	1800		A063109
CONVENTIONALS						
Redox Potential	mV	230	140	230	N/A	A066391
Inorganics						
Soluble (20:1) Chloride (Cl-)	ug/g	600	91	160	20	A065953
Conductivity	umho/cm	1340	311	546	2	A065600
Available (CaCl2) pH	pH	6.74	7.54	7.58		A065559
Soluble (20:1) Sulphate (SO4)	ug/g	570	95	96	20	A065978
Sulphide	mg/kg	1.28 (1)	<0.50 (1)	0.77 (1)	0.50	A067788
RDL = Reportable Detection Limit						
QC Batch = Quality Control Batch						
N/A = Not Applicable						
(1) Extracted past method specified hold time						
Sample contained greater than 10% headspace at time of extraction.						

Bureau Veritas ID		AXTU17			AXTU18	AXTU19		
Sampling Date		2025/11/21 10:00			2025/11/21 12:00	2025/11/21 12:00		
COC Number		N/A			N/A	N/A		
	UNITS	TP1-25-G3-450MM Lab-Dup	RDL	QC Batch	TP3-25-G1-150MM	TP3-25-G2-300MM	RDL	QC Batch
Calculated Parameters								
Resistivity	ohm-cm				8500	14000		A063109
CONVENTIONALS								
Redox Potential	mV				270	200	N/A	A066391
Inorganics								
Soluble (20:1) Chloride (Cl-)	ug/g	190	20	A065953	<20	<20	20	A065953
Conductivity	umho/cm	552	2	A065600	117	70	2	A065600
Available (CaCl2) pH	pH				6.53	7.21		A065559
Soluble (20:1) Sulphate (SO4)	ug/g	120	20	A065978	90	34	20	A065978
Sulphide	mg/kg				<0.50 (1)	<0.50 (1)	0.50	A067788
RDL = Reportable Detection Limit								
QC Batch = Quality Control Batch								
Lab-Dup = Laboratory Initiated Duplicate								
N/A = Not Applicable								
(1) Extracted past method specified hold time								
Sample contained greater than 10% headspace at time of extraction.								



BUREAU
VERITAS

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Sampler Initials: KS

SOIL CORROSIVITY PACKAGE (SOIL)

Bureau Veritas ID		AXTU19		AXTU20	AXTU21	AXTU22		
Sampling Date		2025/11/21 12:00		2025/11/21 12:00	2025/11/21 16:30	2025/11/21 16:30		
COC Number		N/A		N/A	N/A	N/A		
	UNITS	TP3-25-G2-300MM Lab-Dup	QC Batch	TP3-25-G3-450MM	TP7-25-G1-150MM	TP7-25-G2-300MM	RDL	QC Batch

Calculated Parameters								
Resistivity	ohm-cm			19000	18000	21000		A063109
CONVENTIONALS								
Redox Potential	mV	220	A066391	240	280	200	N/A	A066391
Inorganics								
Soluble (20:1) Chloride (Cl-)	ug/g			<20	<20	<20	20	A065953
Conductivity	umho/cm			53	54	47	2	A065600
Available (CaCl2) pH	pH	7.19	A065559	7.18	6.38	7.01		A065559
Soluble (20:1) Sulphate (SO4)	ug/g			<20	72	<20	20	A065978
Sulphide	mg/kg			<0.50 (1)	<0.50 (1)	0.68 (1)	0.50	A067788

RDL = Reportable Detection Limit

QC Batch = Quality Control Batch

Lab-Dup = Laboratory Initiated Duplicate

N/A = Not Applicable

(1) Extracted past method specified hold time

Sample contained greater than 10% headspace at time of extraction.



SOIL CORROSIVITY PACKAGE (SOIL)

Bureau Veritas ID		AXTU23		
Sampling Date		2025/11/21 16:30		
COC Number		N/A		
	UNITS	TP7-25-G3-450MM	RDL	QC Batch
Calculated Parameters				
Resistivity	ohm-cm	21000		A063109
CONVENTIONALS				
Redox Potential	mV	250	N/A	A066391
Inorganics				
Soluble (20:1) Chloride (Cl-)	ug/g	<20	20	A065953
Conductivity	umho/cm	48	2	A065600
Available (CaCl2) pH	pH	7.02		A065559
Soluble (20:1) Sulphate (SO4)	ug/g	<20	20	A065978
Sulphide	mg/kg	<0.50 (1)	0.50	A067788
RDL = Reportable Detection Limit QC Batch = Quality Control Batch N/A = Not Applicable (1) Extracted past method specified hold time Sample contained greater than 10% headspace at time of extraction.				



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SALINITY IN SOIL (SOIL)

Bureau Veritas ID		AXTU15			AXTU16			AXTU17		
Sampling Date		2025/11/21 10:00			2025/11/21 10:00			2025/11/21 10:00		
COC Number		N/A			N/A			N/A		
	UNITS	TP1-25-G1-150MM	RDL	QC Batch	TP1-25-G2-300MM	RDL	QC Batch	TP1-25-G3-450MM	RDL	QC Batch

ANIONS

Soluble Chloride (Cl-)	mg/L	480	10	A073031	300	10	A073039	370	10	A073031
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Calculated Parameters

Sodium Adsorption Ratio	N/A	3.3	0.10	A073034	7.2	0.10	A073034	3.0	0.10	A073034
Calculated Calcium (Ca)	mg/kg	190	3.5	A073038	18	1.3	A073038	61	1.9	A073038
Calculated Magnesium (Mg)	mg/kg	45	2.4	A073038	5.0	0.86	A073038	20	1.3	A073038
Calculated Sodium (Na)	mg/kg	210	3.5	A073038	88	1.3	A073038	84	1.9	A073038
Calculated Potassium (K)	mg/kg	<2.4	2.4	A073038	1.6	0.86	A073038	3.7	1.3	A073038
Calculated Boron (B)	mg/kg	<0.24	0.24	A073037	<0.086	0.086	A073037	<0.13	0.13	A073037
Calculated Chloride (Cl-)	mg/kg	560	12	A073038	130	4.3	A073038	240	6.3	A073038
Calculated Sulphate (SO4)	mg/kg	380	7.1	A073038	66	2.6	A073038	110	3.8	A073038

Inorganics

Soluble Conductivity	dS/m	2.1	0.020	A073032	1.3	0.020	A073040	1.5	0.020	A073032
Soluble (CaCl2) pH	pH	6.53	N/A	A073033	7.05	N/A	A073041	7.31	N/A	A073033
Soluble Calcium (Ca)	mg/L	160	3.0	A073035	43	3.0	A073042	96	3.0	A073035
Soluble Magnesium (Mg)	mg/L	38	2.0	A073035	12	2.0	A073042	31	2.0	A073035
Soluble Sodium (Na)	mg/L	180	3.0	A073035	200	3.0	A073042	130	3.0	A073035
Soluble Potassium (K)	mg/L	<2.0	2.0	A073035	3.8	2.0	A073042	5.8	2.0	A073035
Saturation %	%	120	N/A	A073036	43	N/A	A073043	63	N/A	A073036
Soluble Sulphate (SO4)	mg/L	320	6.0	A073035	150	6.0	A073042	180	6.0	A073035

RDL = Reportable Detection Limit

QC Batch = Quality Control Batch

N/A = Not Applicable



**BUREAU
VERITAS**

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Client Project #: PG 7751

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Sampler Initials: KS

SALINITY IN SOIL (SOIL)

Bureau Veritas ID		AXTU18			AXTU19			AXTU20		
Sampling Date		2025/11/21 12:00			2025/11/21 12:00			2025/11/21 12:00		
COC Number		N/A			N/A			N/A		
	UNITS	TP3-25-G1-150MM	RDL	QC Batch	TP3-25-G2-300MM	RDL	QC Batch	TP3-25-G3-450MM	RDL	QC Batch

ANIONS

Soluble Chloride (Cl-)	mg/L	22	10	A073031	12	10	A073039	<10	10	A073031
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Calculated Parameters

Sodium Adsorption Ratio	N/A	0.27	0.10	A073034	1.7	0.10	A073034	0.63	0.10	A073034
Calculated Calcium (Ca)	mg/kg	14	1.6	A073038	4.5	1.7	A073038	6.4	1.6	A073038
Calculated Magnesium (Mg)	mg/kg	4.0	1.0	A073038	1.5	1.1	A073038	2.3	1.1	A073038
Calculated Sodium (Na)	mg/kg	3.2	1.6	A073038	13	1.7	A073038	5.3	1.6	A073038
Calculated Potassium (K)	mg/kg	<1.0	1.0	A073038	<1.1	1.1	A073038	<1.1	1.1	A073038
Calculated Boron (B)	mg/kg	<0.10	0.10	A073037	<0.11	0.11	A073037	<0.11	0.11	A073037
Calculated Chloride (Cl-)	mg/kg	11	5.2	A073038	6.8	5.7	A073038	<5.3	5.3	A073038
Calculated Sulphate (SO4)	mg/kg	15	3.1	A073038	8.8	3.4	A073038	7.3	3.2	A073038

Inorganics

Soluble Conductivity	dS/m	0.24	0.020	A073032	0.16	0.020	A073044	0.15	0.020	A073032
Soluble (CaCl2) pH	pH	6.26	N/A	A073033	6.66	N/A	A073041	6.95	N/A	A073033
Soluble Calcium (Ca)	mg/L	27	3.0	A073035	7.9	3.0	A073042	12	3.0	A073035
Soluble Magnesium (Mg)	mg/L	7.7	2.0	A073035	2.7	2.0	A073042	4.2	2.0	A073035
Soluble Sodium (Na)	mg/L	6.2	3.0	A073035	22	3.0	A073042	10	3.0	A073035
Soluble Potassium (K)	mg/L	<2.0	2.0	A073035	<2.0	2.0	A073042	<2.0	2.0	A073035
Saturation %	%	52	N/A	A073036	57	N/A	A073043	53	N/A	A073036
Soluble Sulphate (SO4)	mg/L	28	6.0	A073035	15	6.0	A073042	14	6.0	A073035

RDL = Reportable Detection Limit

QC Batch = Quality Control Batch

N/A = Not Applicable



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Sampler Initials: KS

SALINITY IN SOIL (SOIL)

Bureau Veritas ID		AXTU21			AXTU22		AXTU23		
Sampling Date		2025/11/21 16:30			2025/11/21 16:30		2025/11/21 16:30		
COC Number		N/A			N/A		N/A		
	UNITS	TP7-25-G1-150MM	RDL	QC Batch	TP7-25-G2-300MM	RDL	TP7-25-G3-450MM	RDL	QC Batch
ANIONS									
Soluble Chloride (Cl-)	mg/L	<10	10	A073031	<10	10	<10	10	A073045
Calculated Parameters									
Sodium Adsorption Ratio	N/A	0.20 (1)	0.10	A073034	1.2	0.10	1.9	0.10	A073034
Calculated Calcium (Ca)	mg/kg	7.2	1.1	A073038	8.1	1.5	1.6	1.4	A073038
Calculated Magnesium (Mg)	mg/kg	2.0	0.74	A073038	4.2	1.0	<0.92	0.92	A073038
Calculated Sodium (Na)	mg/kg	1.5	1.1	A073038	12	1.5	5.9	1.4	A073038
Calculated Potassium (K)	mg/kg	1.1	0.74	A073038	1.5	1.0	1.9	0.92	A073038
Calculated Boron (B)	mg/kg	<0.074	0.074	A073037	<0.10	0.10	<0.092	0.092	A073037
Calculated Chloride (Cl-)	mg/kg	<3.7	3.7	A073038	<5.2	5.2	<4.6	4.6	A073038
Calculated Sulphate (SO4)	mg/kg	6.9	2.2	A073038	36	3.1	<2.8	2.8	A073038
Inorganics									
Soluble Conductivity	dS/m	0.16	0.020	A073032	0.27	0.020	0.075	0.020	A073046
Soluble (CaCl2) pH	pH	6.24	N/A	A073033	6.57	N/A	6.65	N/A	A073047
Soluble Calcium (Ca)	mg/L	19	3.0	A073035	16	3.0	3.5	3.0	A073048
Soluble Magnesium (Mg)	mg/L	5.4	2.0	A073035	8.1	2.0	<2.0	2.0	A073048
Soluble Sodium (Na)	mg/L	3.9	3.0	A073035	24	3.0	13	3.0	A073048
Soluble Potassium (K)	mg/L	3.0	2.0	A073035	3.0	2.0	4.1	2.0	A073048
Saturation %	%	37	N/A	A073036	52	N/A	46	N/A	A073049
Soluble Sulphate (SO4)	mg/L	19	6.0	A073035	70	6.0	<6.0	6.0	A073048
RDL = Reportable Detection Limit									
QC Batch = Quality Control Batch									
N/A = Not Applicable									
(1) Sodium was not detected. To report SAR the sodium detection limit was used in the calculation. This value represents a maximum ratio.									



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Sampler Initials: KS

SODIUM ADSORPTION RATIO (SAR)

Bureau Veritas ID		AXTU15	AXTU16	AXTU17	AXTU18	AXTU19	
Sampling Date		2025/11/21 10:00	2025/11/21 10:00	2025/11/21 10:00	2025/11/21 12:00	2025/11/21 12:00	
COC Number		N/A	N/A	N/A	N/A	N/A	
	UNITS	TP1-25-G1-150MM	TP1-25-G2-300MM	TP1-25-G3-450MM	TP3-25-G1-150MM	TP3-25-G2-300MM	QC Batch

Calculated Parameters

Sodium Adsorption Ratio	N/A	3.3	7.2	3.0	0.27	1.7	A063110
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QC Batch = Quality Control Batch

Bureau Veritas ID		AXTU20	AXTU21	AXTU22	AXTU23	
Sampling Date		2025/11/21 12:00	2025/11/21 16:30	2025/11/21 16:30	2025/11/21 16:30	
COC Number		N/A	N/A	N/A	N/A	
	UNITS	TP3-25-G3-450MM	TP7-25-G1-150MM	TP7-25-G2-300MM	TP7-25-G3-450MM	QC Batch

Calculated Parameters

Sodium Adsorption Ratio	N/A	0.63	0.20	1.2	1.9	A063110
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QC Batch = Quality Control Batch



**BUREAU
VERITAS**

Bureau Veritas Job #: C5F0314
Report Date: 2025/12/16

Paterson Group
Client Project #: PG 7751
Site Location: 375 DIDSBURY RD
Sampler Initials: KS

RESULTS OF ANALYSES OF SOIL

Bureau Veritas ID		AXTU15			AXTU15			AXTU16		
Sampling Date		2025/11/21 10:00			2025/11/21 10:00			2025/11/21 10:00		
COC Number		N/A			N/A			N/A		
	UNITS	TP1-25-G1-150MM	RDL	QC Batch	TP1-25-G1-150MM Lab-Dup	RDL	QC Batch	TP1-25-G2-300MM	RDL	QC Batch

Calculated Parameters										
Organic Matter	%	27.1	1.0	A065141				1.8	1.0	A065141
Physical Testing										
Moisture-Subcontracted	%	54	0.30	A067789				18	0.30	A067789
PHYSICAL PROPERTIES										
Loss on Ignition	%w/w	27.1	1.0	A065142	28.8	1.0	A065142	1.8	1.0	A065142
RDL = Reportable Detection Limit										
QC Batch = Quality Control Batch										
Lab-Dup = Laboratory Initiated Duplicate										

Bureau Veritas ID		AXTU17	AXTU18	AXTU19	AXTU20		
Sampling Date		2025/11/21 10:00	2025/11/21 12:00	2025/11/21 12:00	2025/11/21 12:00		
COC Number		N/A	N/A	N/A	N/A		
	UNITS	TP1-25-G3-450MM	TP3-25-G1-150MM	TP3-25-G2-300MM	TP3-25-G3-450MM	RDL	QC Batch

Calculated Parameters							
Organic Matter	%	2.8	7.2	2.9	2.8	1.0	A065141
Physical Testing							
Moisture-Subcontracted	%	27	21	21	22	0.30	A067789
PHYSICAL PROPERTIES							
Loss on Ignition	%w/w	2.8	7.2	2.9	2.8	1.0	A065142
RDL = Reportable Detection Limit							
QC Batch = Quality Control Batch							

Bureau Veritas ID		AXTU20			AXTU21	AXTU22	AXTU23		
Sampling Date		2025/11/21 12:00			2025/11/21 16:30	2025/11/21 16:30	2025/11/21 16:30		
COC Number		N/A			N/A	N/A	N/A		
	UNITS	TP3-25-G3-450MM Lab-Dup	RDL	QC Batch	TP7-25-G1-150MM	TP7-25-G2-300MM	TP7-25-G3-450MM	RDL	QC Batch

Calculated Parameters									
Organic Matter	%				3.0	2.5	2.8	1.0	A065141
Physical Testing									
Moisture-Subcontracted	%	22	0.30	A067789	14	17	20	0.30	A067789
PHYSICAL PROPERTIES									
Loss on Ignition	%w/w				3.0	2.5	2.8	1.0	A065142
RDL = Reportable Detection Limit									
QC Batch = Quality Control Batch									
Lab-Dup = Laboratory Initiated Duplicate									



BUREAU
VERITAS

Bureau Veritas Job #: C5F0314

Report Date: 2025/12/16

Paterson Group

Client Project #: PG 7751

Site Location: 375 DIDSBURY RD

Sampler Initials: KS

ELEMENTS BY ATOMIC SPECTROSCOPY (SOIL)

Bureau Veritas ID		AXTU15	AXTU16	AXTU17	AXTU17		
Sampling Date		2025/11/21 10:00	2025/11/21 10:00	2025/11/21 10:00	2025/11/21 10:00		
COC Number		N/A	N/A	N/A	N/A		
	UNITS	TP1-25-G1-150MM	TP1-25-G2-300MM	TP1-25-G3-450MM	TP1-25-G3-450MM Lab-Dup	RDL	QC Batch

Metals							
Acid Extractable Aluminum (Al)	ug/g	12000	14000	22000	21000	50	A064873
Acid Extractable Antimony (Sb)	ug/g	<0.20	<0.20	<0.20	<0.20	0.20	A064873
Acid Extractable Arsenic (As)	ug/g	1.5	3.1	2.0	1.7	1.0	A064873
Acid Extractable Barium (Ba)	ug/g	97	110	220	210	0.50	A064873
Acid Extractable Beryllium (Be)	ug/g	0.49	0.37	0.64	0.62	0.20	A064873
Acid Extractable Bismuth (Bi)	ug/g	<1.0	<1.0	<1.0	<1.0	1.0	A064873
Acid Extractable Boron (B)	ug/g	7.0	<5.0	5.4	5.4	5.0	A064873
Acid Extractable Cadmium (Cd)	ug/g	0.85	0.12	<0.10	<0.10	0.10	A064873
Acid Extractable Calcium (Ca)	ug/g	14000	5800	14000	13000	50	A064873
Acid Extractable Chromium (Cr)	ug/g	27	38	63	60	1.0	A064873
Acid Extractable Cobalt (Co)	ug/g	5.4	9.7	15	14	0.10	A064873
Acid Extractable Copper (Cu)	ug/g	65	15	25	24	0.50	A064873
Acid Extractable Iron (Fe)	ug/g	12000	21000	34000	32000	50	A064873
Acid Extractable Lead (Pb)	ug/g	8.4	4.2	6.1	5.8	1.0	A064873
Acid Extractable Magnesium (Mg)	ug/g	3900	6400	14000	14000	50	A064873
Acid Extractable Manganese (Mn)	ug/g	190	210	440	420	1.0	A064873
Acid Extractable Sulphur (S)	ug/g	1900	80	110	110	50	A064877
Acid Extractable Molybdenum (Mo)	ug/g	<0.50	<0.50	<0.50	<0.50	0.50	A064873
Acid Extractable Nickel (Ni)	ug/g	17	21	35	33	0.50	A064873
Acid Extractable Phosphorus (P)	ug/g	1100	1100	1200	1100	50	A064873
Acid Extractable Potassium (K)	ug/g	1000	2800	6200	5900	200	A064873
Acid Extractable Selenium (Se)	ug/g	1.5	<0.50	<0.50	<0.50	0.50	A064873
Acid Extractable Silver (Ag)	ug/g	<0.20	<0.20	<0.20	<0.20	0.20	A064873
Acid Extractable Sodium (Na)	ug/g	680	570	980	980	50	A064873
Acid Extractable Strontium (Sr)	ug/g	63	25	41	38	1.0	A064873
Acid Extractable Thallium (Tl)	ug/g	0.077	0.15	0.26	0.25	0.050	A064873
Acid Extractable Tin (Sn)	ug/g	<1.0	<1.0	<1.0	1.0	1.0	A064873
Acid Extractable Uranium (U)	ug/g	2.7	0.62	0.71	0.67	0.050	A064873
Acid Extractable Vanadium (V)	ug/g	57	44	65	62	5.0	A064873
Acid Extractable Zinc (Zn)	ug/g	67	52	81	76	5.0	A064873

RDL = Reportable Detection Limit

QC Batch = Quality Control Batch

Lab-Dup = Laboratory Initiated Duplicate



ELEMENTS BY ATOMIC SPECTROSCOPY (SOIL)

Bureau Veritas ID		AXTU15	AXTU16	AXTU17	AXTU17		
Sampling Date		2025/11/21 10:00	2025/11/21 10:00	2025/11/21 10:00	2025/11/21 10:00		
COC Number		N/A	N/A	N/A	N/A		
	UNITS	TP1-25-G1-150MM	TP1-25-G2-300MM	TP1-25-G3-450MM	TP1-25-G3-450MM Lab-Dup	RDL	QC Batch
Acid Extractable Mercury (Hg)	ug/g	0.12	<0.050	<0.050	<0.050	0.050	A064873
RDL = Reportable Detection Limit QC Batch = Quality Control Batch Lab-Dup = Laboratory Initiated Duplicate							



BUREAU
VERITAS

Bureau Veritas Job #: C5F0314

Report Date: 2025/12/16

Paterson Group

Client Project #: PG 7751

Site Location: 375 DIDSBURY RD

Sampler Initials: KS

ELEMENTS BY ATOMIC SPECTROSCOPY (SOIL)

Bureau Veritas ID		AXTU18	AXTU19	AXTU20	AXTU21		
Sampling Date		2025/11/21 12:00	2025/11/21 12:00	2025/11/21 12:00	2025/11/21 16:30		
COC Number		N/A	N/A	N/A	N/A		
	UNITS	TP3-25-G1-150MM	TP3-25-G2-300MM	TP3-25-G3-450MM	TP7-25-G1-150MM	RDL	QC Batch

Metals

Acid Extractable Aluminum (Al)	ug/g	17000	24000	23000	7700	50	A064873
Acid Extractable Antimony (Sb)	ug/g	<0.20	<0.20	<0.20	<0.20	0.20	A064873
Acid Extractable Arsenic (As)	ug/g	2.5	2.2	3.1	1.0	1.0	A064873
Acid Extractable Barium (Ba)	ug/g	180	300	280	68	0.50	A064873
Acid Extractable Beryllium (Be)	ug/g	0.50	0.69	0.64	0.23	0.20	A064873
Acid Extractable Bismuth (Bi)	ug/g	<1.0	<1.0	<1.0	<1.0	1.0	A064873
Acid Extractable Boron (B)	ug/g	5.6	5.9	5.7	<5.0	5.0	A064873
Acid Extractable Cadmium (Cd)	ug/g	0.33	0.14	<0.10	<0.10	0.10	A064873
Acid Extractable Calcium (Ca)	ug/g	7400	8900	8200	3900	50	A064873
Acid Extractable Chromium (Cr)	ug/g	46	72	67	18	1.0	A064873
Acid Extractable Cobalt (Co)	ug/g	9.9	19	16	3.6	0.10	A064873
Acid Extractable Copper (Cu)	ug/g	20	21	20	4.6	0.50	A064873
Acid Extractable Iron (Fe)	ug/g	24000	42000	38000	11000	50	A064873
Acid Extractable Lead (Pb)	ug/g	8.3	6.7	5.9	4.2	1.0	A064873
Acid Extractable Magnesium (Mg)	ug/g	6700	12000	12000	2800	50	A064873
Acid Extractable Manganese (Mn)	ug/g	660	660	610	220	1.0	A064873
Acid Extractable Sulphur (S)	ug/g	330	110	55	140	50	A064877
Acid Extractable Molybdenum (Mo)	ug/g	<0.50	<0.50	<0.50	<0.50	0.50	A064873
Acid Extractable Nickel (Ni)	ug/g	23	39	36	8.3	0.50	A064873
Acid Extractable Phosphorus (P)	ug/g	1100	1200	1200	770	50	A064873
Acid Extractable Potassium (K)	ug/g	2400	5700	5800	1200	200	A064873
Acid Extractable Selenium (Se)	ug/g	0.53	<0.50	<0.50	<0.50	0.50	A064873
Acid Extractable Silver (Ag)	ug/g	<0.20	<0.20	<0.20	<0.20	0.20	A064873
Acid Extractable Sodium (Na)	ug/g	390	770	840	160	50	A064873
Acid Extractable Strontium (Sr)	ug/g	32	41	39	17	1.0	A064873
Acid Extractable Thallium (Tl)	ug/g	0.15	0.27	0.27	0.056	0.050	A064873
Acid Extractable Tin (Sn)	ug/g	<1.0	<1.0	1.0	<1.0	1.0	A064873
Acid Extractable Uranium (U)	ug/g	1.2	0.73	0.67	0.67	0.050	A064873
Acid Extractable Vanadium (V)	ug/g	57	77	68	21	5.0	A064873
Acid Extractable Zinc (Zn)	ug/g	68	86	80	27	5.0	A064873
Acid Extractable Mercury (Hg)	ug/g	0.056	<0.050	<0.050	<0.050	0.050	A064873

RDL = Reportable Detection Limit

QC Batch = Quality Control Batch



BUREAU
VERITAS

Bureau Veritas Job #: C5F0314

Report Date: 2025/12/16

Paterson Group

Client Project #: PG 7751

Site Location: 375 DIDSBURY RD

Sampler Initials: KS

ELEMENTS BY ATOMIC SPECTROSCOPY (SOIL)

Bureau Veritas ID		AXTU22	AXTU23		
Sampling Date		2025/11/21 16:30	2025/11/21 16:30		
COC Number		N/A	N/A		
	UNITS	TP7-25-G2-300MM	TP7-25-G3-450MM	RDL	QC Batch
Metals					
Acid Extractable Aluminum (Al)	ug/g	17000	26000	50	A064873
Acid Extractable Antimony (Sb)	ug/g	<0.20	<0.20	0.20	A064873
Acid Extractable Arsenic (As)	ug/g	1.7	2.2	1.0	A064873
Acid Extractable Barium (Ba)	ug/g	180	280	0.50	A064873
Acid Extractable Beryllium (Be)	ug/g	0.47	0.68	0.20	A064873
Acid Extractable Bismuth (Bi)	ug/g	<1.0	<1.0	1.0	A064873
Acid Extractable Boron (B)	ug/g	<5.0	<5.0	5.0	A064873
Acid Extractable Cadmium (Cd)	ug/g	<0.10	0.11	0.10	A064873
Acid Extractable Calcium (Ca)	ug/g	6200	8400	50	A064873
Acid Extractable Chromium (Cr)	ug/g	48	70	1.0	A064873
Acid Extractable Cobalt (Co)	ug/g	8.8	14	0.10	A064873
Acid Extractable Copper (Cu)	ug/g	13	18	0.50	A064873
Acid Extractable Iron (Fe)	ug/g	27000	37000	50	A064873
Acid Extractable Lead (Pb)	ug/g	4.7	6.6	1.0	A064873
Acid Extractable Magnesium (Mg)	ug/g	7500	11000	50	A064873
Acid Extractable Manganese (Mn)	ug/g	440	990	1.0	A064873
Acid Extractable Sulphur (S)	ug/g	57	61	50	A064877
Acid Extractable Molybdenum (Mo)	ug/g	<0.50	<0.50	0.50	A064873
Acid Extractable Nickel (Ni)	ug/g	23	34	0.50	A064873
Acid Extractable Phosphorus (P)	ug/g	1000	1100	50	A064873
Acid Extractable Potassium (K)	ug/g	3200	5400	200	A064873
Acid Extractable Selenium (Se)	ug/g	<0.50	<0.50	0.50	A064873
Acid Extractable Silver (Ag)	ug/g	<0.20	<0.20	0.20	A064873
Acid Extractable Sodium (Na)	ug/g	390	620	50	A064873
Acid Extractable Strontium (Sr)	ug/g	28	38	1.0	A064873
Acid Extractable Thallium (Tl)	ug/g	0.17	0.29	0.050	A064873
Acid Extractable Tin (Sn)	ug/g	<1.0	<1.0	1.0	A064873
Acid Extractable Uranium (U)	ug/g	0.53	0.70	0.050	A064873
Acid Extractable Vanadium (V)	ug/g	52	70	5.0	A064873
Acid Extractable Zinc (Zn)	ug/g	58	82	5.0	A064873
Acid Extractable Mercury (Hg)	ug/g	<0.050	<0.050	0.050	A064873
RDL = Reportable Detection Limit					
QC Batch = Quality Control Batch					



**BUREAU
VERITAS**

Bureau Veritas Job #: C5F0314

Report Date: 2025/12/16

Paterson Group

Client Project #: PG 7751

Site Location: 375 DIDSBURY RD

Sampler Initials: KS

TEST SUMMARY

Bureau Veritas ID: AXTU15
Sample ID: TP1-25-G1-150MM
Matrix: Soil

Collected: 2025/11/21
Shipped:
Received: 2025/11/26

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Chloride (20:1 extract)	SKAL/EC	A065953	2025/12/02	2025/12/03	Massarat Jan
Conductivity	AT	A065600	2025/12/02	2025/12/02	Nachiketa Gohil
Acid Extractable Metals by ICPMS	ICP/MS	A064873	2025/12/01	2025/12/01	Daniel Teclu
Acid Extractable Metals Analysis by ICP	ICP	A064877	2025/12/01	2025/12/02	Lina Nguyen
Chloride (soluble)	KONE	A073031	2025/12/11	2025/12/11	Adam Fishleigh
Conductivity @25C (Soluble)	COND	A073032	2025/12/11	2025/12/11	Zafar Iqbal
Loss on Ignition	BAL/BAL	A065142	2025/12/01	2025/12/01	Rafael Sarabia
Moisture (Subcontracted)	BAL	A067789	N/A	2025/12/03	Simranjeet Batth
Organic Matter - Calculated from LOI	CALC	A065141	2025/12/01	2025/12/01	Automated Statchk
pH @ 25C (1:2 Calcium Chloride Extract)	PH	A073033	2025/12/11	2025/12/11	Jaya Rose MALIHAN
Sodium Adsorption Ratio (SAR)	CALC	A073034	N/A	2025/12/12	Automated Statchk
Soluble Ions	ICP	A073035	2025/12/11	2025/12/11	Vincy Scaria
Sulphide in Soil	SPEC	A067788	N/A	2025/12/04	Dafne Strozake Maximo
Soluble Paste	BAL	A073036	2025/12/11	2025/12/11	Nerissa Schwartz
Soluble Boron Calculation	CALC	A073037	N/A	2025/12/12	Automated Statchk
Soluble Ions Calculation	CALC	A073038	N/A	2025/12/03	Automated Statchk
pH CaCl2 EXTRACT	AT	A065559	2025/12/02	2025/12/02	Surinder Rai
Redox Potential	COND	A066391	2025/12/03	2025/12/06	Nachiketa Gohil
Resistivity of Soil		A063109	2025/12/02	2025/12/02	Automated Statchk
Sodium Adsorption Ratio (SAR)	CALC/MET	A063110	N/A	2025/12/16	Automated Statchk
Sulphate (20:1 Extract)	SKAL/EC	A065978	2025/12/02	2025/12/03	Massarat Jan

Bureau Veritas ID: AXTU15 Dup
Sample ID: TP1-25-G1-150MM
Matrix: Soil

Collected: 2025/11/21
Shipped:
Received: 2025/11/26

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Loss on Ignition	BAL/BAL	A065142	2025/12/01	2025/12/01	Rafael Sarabia

Bureau Veritas ID: AXTU16
Sample ID: TP1-25-G2-300MM
Matrix: Soil

Collected: 2025/11/21
Shipped:
Received: 2025/11/26

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Chloride (20:1 extract)	SKAL/EC	A065953	2025/12/02	2025/12/03	Massarat Jan
Conductivity	AT	A065600	2025/12/02	2025/12/02	Nachiketa Gohil
Acid Extractable Metals by ICPMS	ICP/MS	A064873	2025/12/01	2025/12/01	Daniel Teclu
Acid Extractable Metals Analysis by ICP	ICP	A064877	2025/12/01	2025/12/02	Lina Nguyen
Chloride (soluble)	KONE	A073039	2025/12/05	2025/12/05	Tyler Orr
Conductivity @25C (Soluble)	COND	A073040	2025/12/05	2025/12/06	Zafar Iqbal
Loss on Ignition	BAL/BAL	A065142	2025/12/01	2025/12/01	Rafael Sarabia
Moisture (Subcontracted)	BAL	A067789	N/A	2025/12/03	Simranjeet Batth
Organic Matter - Calculated from LOI	CALC	A065141	2025/12/01	2025/12/01	Automated Statchk
pH @ 25C (1:2 Calcium Chloride Extract)	PH	A073041	2025/12/05	2025/12/05	Jaya Rose MALIHAN
Sodium Adsorption Ratio (SAR)	CALC	A073034	N/A	2025/12/06	Automated Statchk



**BUREAU
VERITAS**

Bureau Veritas Job #: C5F0314
Report Date: 2025/12/16

Paterson Group
Client Project #: PG 7751
Site Location: 375 DIDSBURY RD
Sampler Initials: KS

TEST SUMMARY

Bureau Veritas ID: AXTU16
Sample ID: TP1-25-G2-300MM
Matrix: Soil

Collected: 2025/11/21
Shipped:
Received: 2025/11/26

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Soluble Ions	ICP	A073042	2025/12/05	2025/12/06	Vincy Scaria
Sulphide in Soil	SPEC	A067788	N/A	2025/12/04	Dafne Strozake Maximo
Soluble Paste	BAL	A073043	2025/12/05	2025/12/05	Steven Tram
Soluble Boron Calculation	CALC	A073037	N/A	2025/12/06	Automated Statchk
Soluble Ions Calculation	CALC	A073038	N/A	2025/12/03	Automated Statchk
pH CaCl2 EXTRACT	AT	A065559	2025/12/02	2025/12/02	Surinder Rai
Redox Potential	COND	A066391	2025/12/03	2025/12/06	Nachiketa Gohil
Resistivity of Soil		A063109	2025/12/02	2025/12/02	Automated Statchk
Sodium Adsorption Ratio (SAR)	CALC/MET	A063110	N/A	2025/12/16	Automated Statchk
Sulphate (20:1 Extract)	SKAL/EC	A065978	2025/12/02	2025/12/03	Massarat Jan

Bureau Veritas ID: AXTU17
Sample ID: TP1-25-G3-450MM
Matrix: Soil

Collected: 2025/11/21
Shipped:
Received: 2025/11/26

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Chloride (20:1 extract)	SKAL/EC	A065953	2025/12/02	2025/12/03	Massarat Jan
Conductivity	AT	A065600	2025/12/02	2025/12/02	Nachiketa Gohil
Acid Extractable Metals by ICPMS	ICP/MS	A064873	2025/12/01	2025/12/01	Daniel Teclu
Acid Extractable Metals Analysis by ICP	ICP	A064877	2025/12/01	2025/12/02	Lina Nguyen
Chloride (soluble)	KONE	A073031	2025/12/11	2025/12/11	Adam Fishleigh
Conductivity @25C (Soluble)	COND	A073032	2025/12/11	2025/12/11	Zafar Iqbal
Loss on Ignition	BAL/BAL	A065142	2025/12/01	2025/12/01	Rafael Sarabia
Moisture (Subcontracted)	BAL	A067789	N/A	2025/12/03	Simranjeet Batth
Organic Matter - Calculated from LOI	CALC	A065141	2025/12/01	2025/12/01	Automated Statchk
pH @ 25C (1:2 Calcium Chloride Extract)	PH	A073033	2025/12/11	2025/12/11	Jaya Rose MALIHAN
Sodium Adsorption Ratio (SAR)	CALC	A073034	N/A	2025/12/12	Automated Statchk
Soluble Ions	ICP	A073035	2025/12/11	2025/12/11	Vincy Scaria
Sulphide in Soil	SPEC	A067788	N/A	2025/12/04	Dafne Strozake Maximo
Soluble Paste	BAL	A073036	2025/12/11	2025/12/11	Nerissa Schwartz
Soluble Boron Calculation	CALC	A073037	N/A	2025/12/12	Automated Statchk
Soluble Ions Calculation	CALC	A073038	N/A	2025/12/03	Automated Statchk
pH CaCl2 EXTRACT	AT	A065559	2025/12/02	2025/12/02	Surinder Rai
Redox Potential	COND	A066391	2025/12/03	2025/12/06	Nachiketa Gohil
Resistivity of Soil		A063109	2025/12/02	2025/12/02	Automated Statchk
Sodium Adsorption Ratio (SAR)	CALC/MET	A063110	N/A	2025/12/16	Automated Statchk
Sulphate (20:1 Extract)	SKAL/EC	A065978	2025/12/02	2025/12/03	Massarat Jan

Bureau Veritas ID: AXTU17 Dup
Sample ID: TP1-25-G3-450MM
Matrix: Soil

Collected: 2025/11/21
Shipped:
Received: 2025/11/26

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Chloride (20:1 extract)	SKAL/EC	A065953	2025/12/02	2025/12/03	Massarat Jan
Conductivity	AT	A065600	2025/12/02	2025/12/02	Nachiketa Gohil



**BUREAU
VERITAS**

Bureau Veritas Job #: C5F0314

Report Date: 2025/12/16

Paterson Group

Client Project #: PG 7751

Site Location: 375 DIDSBURY RD

Sampler Initials: KS

TEST SUMMARY

Bureau Veritas ID: AXTU17 Dup
Sample ID: TP1-25-G3-450MM
Matrix: Soil

Collected: 2025/11/21
Shipped:
Received: 2025/11/26

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Acid Extractable Metals by ICPMS	ICP/MS	A064873	2025/12/01	2025/12/01	Daniel Teclu
Acid Extractable Metals Analysis by ICP	ICP	A064877	2025/12/01	2025/12/02	Lina Nguyen
Sulphate (20:1 Extract)	SKAL/EC	A065978	2025/12/02	2025/12/03	Massarat Jan

Bureau Veritas ID: AXTU18
Sample ID: TP3-25-G1-150MM
Matrix: Soil

Collected: 2025/11/21
Shipped:
Received: 2025/11/26

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Chloride (20:1 extract)	SKAL/EC	A065953	2025/12/02	2025/12/03	Massarat Jan
Conductivity	AT	A065600	2025/12/02	2025/12/02	Nachiketa Gohil
Acid Extractable Metals by ICPMS	ICP/MS	A064873	2025/12/01	2025/12/01	Daniel Teclu
Acid Extractable Metals Analysis by ICP	ICP	A064877	2025/12/01	2025/12/02	Lina Nguyen
Chloride (soluble)	KONE	A073031	2025/12/11	2025/12/11	Adam Fishleigh
Conductivity @25C (Soluble)	COND	A073032	2025/12/11	2025/12/11	Zafar Iqbal
Loss on Ignition	BAL/BAL	A065142	2025/12/01	2025/12/01	Rafael Sarabia
Moisture (Subcontracted)	BAL	A067789	N/A	2025/12/03	Simranjeet Batth
Organic Matter - Calculated from LOI	CALC	A065141	2025/12/01	2025/12/01	Automated Statchk
pH @ 25C (1:2 Calcium Chloride Extract)	PH	A073033	2025/12/11	2025/12/11	Jaya Rose MALIHAN
Sodium Adsorption Ratio (SAR)	CALC	A073034	N/A	2025/12/12	Automated Statchk
Soluble Ions	ICP	A073035	2025/12/11	2025/12/11	Vincy Scaria
Sulphide in Soil	SPEC	A067788	N/A	2025/12/04	Dafne Strozake Maximo
Soluble Paste	BAL	A073036	2025/12/11	2025/12/11	Nerissa Schwartz
Soluble Boron Calculation	CALC	A073037	N/A	2025/12/12	Automated Statchk
Soluble Ions Calculation	CALC	A073038	N/A	2025/12/03	Automated Statchk
pH CaCl2 EXTRACT	AT	A065559	2025/12/02	2025/12/02	Surinder Rai
Redox Potential	COND	A066391	2025/12/03	2025/12/06	Nachiketa Gohil
Resistivity of Soil		A063109	2025/12/02	2025/12/02	Automated Statchk
Sodium Adsorption Ratio (SAR)	CALC/MET	A063110	N/A	2025/12/16	Automated Statchk
Sulphate (20:1 Extract)	SKAL/EC	A065978	2025/12/02	2025/12/03	Massarat Jan

Bureau Veritas ID: AXTU19
Sample ID: TP3-25-G2-300MM
Matrix: Soil

Collected: 2025/11/21
Shipped:
Received: 2025/11/26

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Chloride (20:1 extract)	SKAL/EC	A065953	2025/12/02	2025/12/03	Massarat Jan
Conductivity	AT	A065600	2025/12/02	2025/12/02	Nachiketa Gohil
Acid Extractable Metals by ICPMS	ICP/MS	A064873	2025/12/01	2025/12/01	Daniel Teclu
Acid Extractable Metals Analysis by ICP	ICP	A064877	2025/12/01	2025/12/02	Lina Nguyen
Chloride (soluble)	KONE	A073039	2025/12/05	2025/12/05	Tyler Orr
Conductivity @25C (Soluble)	COND	A073044	2025/12/05	2025/12/06	Zafar Iqbal
Loss on Ignition	BAL/BAL	A065142	2025/12/01	2025/12/01	Rafael Sarabia
Moisture (Subcontracted)	BAL	A067789	N/A	2025/12/03	Simranjeet Batth
Organic Matter - Calculated from LOI	CALC	A065141	2025/12/01	2025/12/01	Automated Statchk



BUREAU
VERITAS

Bureau Veritas Job #: C5F0314

Report Date: 2025/12/16

Paterson Group

Client Project #: PG 7751

Site Location: 375 DIDSBURY RD

Sampler Initials: KS

TEST SUMMARY

Bureau Veritas ID: AXTU19
Sample ID: TP3-25-G2-300MM
Matrix: Soil

Collected: 2025/11/21
Shipped:
Received: 2025/11/26

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
pH @ 25C (1:2 Calcium Chloride Extract)	PH	A073041	2025/12/05	2025/12/05	Jaya Rose MALIHAN
Sodium Adsorption Ratio (SAR)	CALC	A073034	N/A	2025/12/06	Automated Statchk
Soluble Ions	ICP	A073042	2025/12/05	2025/12/06	Vincy Scaria
Sulphide in Soil	SPEC	A067788	N/A	2025/12/04	Dafne Strozake Maximo
Soluble Paste	BAL	A073043	2025/12/05	2025/12/05	Steven Tram
Soluble Boron Calculation	CALC	A073037	N/A	2025/12/06	Automated Statchk
Soluble Ions Calculation	CALC	A073038	N/A	2025/12/03	Automated Statchk
pH CaCl2 EXTRACT	AT	A065559	2025/12/02	2025/12/02	Surinder Rai
Redox Potential	COND	A066391	2025/12/03	2025/12/06	Nachiketa Gohil
Resistivity of Soil		A063109	2025/12/02	2025/12/02	Automated Statchk
Sodium Adsorption Ratio (SAR)	CALC/MET	A063110	N/A	2025/12/16	Automated Statchk
Sulphate (20:1 Extract)	SKAL/EC	A065978	2025/12/02	2025/12/03	Massarat Jan

Bureau Veritas ID: AXTU19 Dup
Sample ID: TP3-25-G2-300MM
Matrix: Soil

Collected: 2025/11/21
Shipped:
Received: 2025/11/26

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
pH CaCl2 EXTRACT	AT	A065559	2025/12/02	2025/12/02	Surinder Rai
Redox Potential	COND	A066391	2025/12/03	2025/12/06	Nachiketa Gohil

Bureau Veritas ID: AXTU20
Sample ID: TP3-25-G3-450MM
Matrix: Soil

Collected: 2025/11/21
Shipped:
Received: 2025/11/26

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Chloride (20:1 extract)	SKAL/EC	A065953	2025/12/02	2025/12/03	Massarat Jan
Conductivity	AT	A065600	2025/12/02	2025/12/02	Nachiketa Gohil
Acid Extractable Metals by ICPMS	ICP/MS	A064873	2025/12/01	2025/12/01	Daniel Teclu
Acid Extractable Metals Analysis by ICP	ICP	A064877	2025/12/01	2025/12/02	Lina Nguyen
Chloride (soluble)	KONE	A073031	2025/12/11	2025/12/11	Adam Fishleigh
Conductivity @25C (Soluble)	COND	A073032	2025/12/11	2025/12/11	Zafar Iqbal
Loss on Ignition	BAL/BAL	A065142	2025/12/01	2025/12/01	Rafael Sarabia
Moisture (Subcontracted)	BAL	A067789	N/A	2025/12/03	Simranjeet Batth
Organic Matter - Calculated from LOI	CALC	A065141	2025/12/01	2025/12/01	Automated Statchk
pH @ 25C (1:2 Calcium Chloride Extract)	PH	A073033	2025/12/11	2025/12/11	Jaya Rose MALIHAN
Sodium Adsorption Ratio (SAR)	CALC	A073034	N/A	2025/12/12	Automated Statchk
Soluble Ions	ICP	A073035	2025/12/11	2025/12/11	Vincy Scaria
Sulphide in Soil	SPEC	A067788	N/A	2025/12/04	Dafne Strozake Maximo
Soluble Paste	BAL	A073036	2025/12/11	2025/12/11	Nerissa Schwartz
Soluble Boron Calculation	CALC	A073037	N/A	2025/12/12	Automated Statchk
Soluble Ions Calculation	CALC	A073038	N/A	2025/12/03	Automated Statchk
pH CaCl2 EXTRACT	AT	A065559	2025/12/02	2025/12/02	Surinder Rai
Redox Potential	COND	A066391	2025/12/03	2025/12/06	Nachiketa Gohil
Resistivity of Soil		A063109	2025/12/02	2025/12/02	Automated Statchk



**BUREAU
VERITAS**

Bureau Veritas Job #: C5F0314

Report Date: 2025/12/16

Paterson Group

Client Project #: PG 7751

Site Location: 375 DIDSBURY RD

Sampler Initials: KS

TEST SUMMARY

Bureau Veritas ID: AXTU20
Sample ID: TP3-25-G3-450MM
Matrix: Soil

Collected: 2025/11/21
Shipped:
Received: 2025/11/26

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Sodium Adsorption Ratio (SAR)	CALC/MET	A063110	N/A	2025/12/16	Automated Statchk
Sulphate (20:1 Extract)	SKAL/EC	A065978	2025/12/02	2025/12/03	Massarat Jan

Bureau Veritas ID: AXTU20 Dup
Sample ID: TP3-25-G3-450MM
Matrix: Soil

Collected: 2025/11/21
Shipped:
Received: 2025/11/26

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Moisture (Subcontracted)	BAL	A067789	N/A	2025/12/03	Simranjeet Batth

Bureau Veritas ID: AXTU21
Sample ID: TP7-25-G1-150MM
Matrix: Soil

Collected: 2025/11/21
Shipped:
Received: 2025/11/26

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Chloride (20:1 extract)	SKAL/EC	A065953	2025/12/02	2025/12/03	Massarat Jan
Conductivity	AT	A065600	2025/12/02	2025/12/02	Nachiketa Gohil
Acid Extractable Metals by ICPMS	ICP/MS	A064873	2025/12/01	2025/12/01	Daniel Teclu
Acid Extractable Metals Analysis by ICP	ICP	A064877	2025/12/01	2025/12/02	Lina Nguyen
Chloride (soluble)	KONE	A073031	2025/12/11	2025/12/11	Adam Fishleigh
Conductivity @25C (Soluble)	COND	A073032	2025/12/11	2025/12/11	Zafar Iqbal
Loss on Ignition	BAL/BAL	A065142	2025/12/01	2025/12/01	Rafael Sarabia
Moisture (Subcontracted)	BAL	A067789	N/A	2025/12/03	Simranjeet Batth
Organic Matter - Calculated from LOI	CALC	A065141	2025/12/01	2025/12/01	Automated Statchk
pH @ 25C (1:2 Calcium Chloride Extract)	PH	A073033	2025/12/11	2025/12/11	Jaya Rose MALIHAN
Sodium Adsorption Ratio (SAR)	CALC	A073034	N/A	2025/12/12	Automated Statchk
Soluble Ions	ICP	A073035	2025/12/11	2025/12/11	Vincy Scaria
Sulphide in Soil	SPEC	A067788	N/A	2025/12/04	Dafne Strozake Maximo
Soluble Paste	BAL	A073036	2025/12/11	2025/12/11	Nerissa Schwartz
Soluble Boron Calculation	CALC	A073037	N/A	2025/12/12	Automated Statchk
Soluble Ions Calculation	CALC	A073038	N/A	2025/12/03	Automated Statchk
pH CaCl2 EXTRACT	AT	A065559	2025/12/02	2025/12/02	Surinder Rai
Redox Potential	COND	A066391	2025/12/03	2025/12/06	Nachiketa Gohil
Resistivity of Soil		A063109	2025/12/02	2025/12/02	Automated Statchk
Sodium Adsorption Ratio (SAR)	CALC/MET	A063110	N/A	2025/12/16	Automated Statchk
Sulphate (20:1 Extract)	SKAL/EC	A065978	2025/12/02	2025/12/03	Massarat Jan

Bureau Veritas ID: AXTU22
Sample ID: TP7-25-G2-300MM
Matrix: Soil

Collected: 2025/11/21
Shipped:
Received: 2025/11/26

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Chloride (20:1 extract)	SKAL/EC	A065953	2025/12/02	2025/12/03	Massarat Jan
Conductivity	AT	A065600	2025/12/02	2025/12/02	Nachiketa Gohil
Acid Extractable Metals by ICPMS	ICP/MS	A064873	2025/12/01	2025/12/01	Daniel Teclu

BUREAU
VERITAS

Bureau Veritas Job #: C5F0314

Report Date: 2025/12/16

Paterson Group

Client Project #: PG 7751

Site Location: 375 DIDSBURY RD

Sampler Initials: KS

TEST SUMMARY

Bureau Veritas ID: AXTU22
Sample ID: TP7-25-G2-300MM
Matrix: Soil

Collected: 2025/11/21
Shipped:
Received: 2025/11/26

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Acid Extractable Metals Analysis by ICP	ICP	A064877	2025/12/01	2025/12/02	Lina Nguyen
Chloride (soluble)	KONE	A073045	2025/12/05	2025/12/07	Adam Fishleigh
Conductivity @25C (Soluble)	COND	A073046	2025/12/05	2025/12/06	Zafar Iqbal
Loss on Ignition	BAL/BAL	A065142	2025/12/01	2025/12/01	Rafael Sarabia
Moisture (Subcontracted)	BAL	A067789	N/A	2025/12/03	Simranjeet Batth
Organic Matter - Calculated from LOI	CALC	A065141	2025/12/01	2025/12/01	Automated Statchk
pH @ 25C (1:2 Calcium Chloride Extract)	PH	A073047	2025/12/05	2025/12/05	Jaya Rose MALIHAN
Sodium Adsorption Ratio (SAR)	CALC	A073034	N/A	2025/12/07	Automated Statchk
Soluble Ions	ICP	A073048	2025/12/05	2025/12/07	Kevin Hung
Sulphide in Soil	SPEC	A067788	N/A	2025/12/04	Dafne Strozake Maximo
Soluble Paste	BAL	A073049	2025/12/05	2025/12/05	Steven Tram
Soluble Boron Calculation	CALC	A073037	N/A	2025/12/07	Automated Statchk
Soluble Ions Calculation	CALC	A073038	N/A	2025/12/03	Automated Statchk
pH CaCl2 EXTRACT	AT	A065559	2025/12/02	2025/12/02	Surinder Rai
Redox Potential	COND	A066391	2025/12/03	2025/12/06	Nachiketa Gohil
Resistivity of Soil		A063109	2025/12/02	2025/12/02	Automated Statchk
Sodium Adsorption Ratio (SAR)	CALC/MET	A063110	N/A	2025/12/16	Automated Statchk
Sulphate (20:1 Extract)	SKAL/EC	A065978	2025/12/02	2025/12/03	Massarat Jan

Bureau Veritas ID: AXTU23
Sample ID: TP7-25-G3-450MM
Matrix: Soil

Collected: 2025/11/21
Shipped:
Received: 2025/11/26

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Chloride (20:1 extract)	SKAL/EC	A065953	2025/12/02	2025/12/03	Massarat Jan
Conductivity	AT	A065600	2025/12/02	2025/12/02	Nachiketa Gohil
Acid Extractable Metals by ICPMS	ICP/MS	A064873	2025/12/01	2025/12/01	Daniel Teclu
Acid Extractable Metals Analysis by ICP	ICP	A064877	2025/12/01	2025/12/02	Lina Nguyen
Chloride (soluble)	KONE	A073045	2025/12/05	2025/12/07	Adam Fishleigh
Conductivity @25C (Soluble)	COND	A073046	2025/12/05	2025/12/06	Zafar Iqbal
Loss on Ignition	BAL/BAL	A065142	2025/12/01	2025/12/01	Rafael Sarabia
Moisture (Subcontracted)	BAL	A067789	N/A	2025/12/03	Simranjeet Batth
Organic Matter - Calculated from LOI	CALC	A065141	2025/12/01	2025/12/01	Automated Statchk
pH @ 25C (1:2 Calcium Chloride Extract)	PH	A073047	2025/12/05	2025/12/05	Jaya Rose MALIHAN
Sodium Adsorption Ratio (SAR)	CALC	A073034	N/A	2025/12/07	Automated Statchk
Soluble Ions	ICP	A073048	2025/12/05	2025/12/07	Kevin Hung
Sulphide in Soil	SPEC	A067788	N/A	2025/12/04	Dafne Strozake Maximo
Soluble Paste	BAL	A073049	2025/12/05	2025/12/05	Steven Tram
Soluble Boron Calculation	CALC	A073037	N/A	2025/12/07	Automated Statchk
Soluble Ions Calculation	CALC	A073038	N/A	2025/12/03	Automated Statchk
pH CaCl2 EXTRACT	AT	A065559	2025/12/02	2025/12/02	Surinder Rai
Redox Potential	COND	A066391	2025/12/03	2025/12/06	Nachiketa Gohil
Resistivity of Soil		A063109	2025/12/02	2025/12/02	Automated Statchk
Sodium Adsorption Ratio (SAR)	CALC/MET	A063110	N/A	2025/12/16	Automated Statchk
Sulphate (20:1 Extract)	SKAL/EC	A065978	2025/12/02	2025/12/03	Massarat Jan



GENERAL COMMENTS

Each temperature is the average of up to three cooler temperatures taken at receipt

Package 1	22.0°C
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Samples received above an average of 10 degrees with no cooling media, proceeded with client consent.

Results relate only to the items tested.



BUREAU
VERITAS

Bureau Veritas Job #: C5F0314
Report Date: 2025/12/16

Paterson Group
Client Project #: PG 7751
Site Location: 375 DIDSBUY RD
Sampler Initials: KS

QUALITY ASSURANCE REPORT

QA/QC	Batch	Init	QC Type	Parameter	Date Analyzed	Value	Recovery	UNITS	QC Limits
A064873	DT1	Matrix Spike [AXTU17-01]	Acid Extractable Aluminum (Al)	2025/12/01		NC	%	75 - 125	
			Acid Extractable Antimony (Sb)	2025/12/01		86	%	75 - 125	
			Acid Extractable Arsenic (As)	2025/12/01		100	%	75 - 125	
			Acid Extractable Barium (Ba)	2025/12/01		NC	%	75 - 125	
			Acid Extractable Beryllium (Be)	2025/12/01		98	%	75 - 125	
			Acid Extractable Bismuth (Bi)	2025/12/01		99	%	75 - 125	
			Acid Extractable Boron (B)	2025/12/01		93	%	75 - 125	
			Acid Extractable Cadmium (Cd)	2025/12/01		103	%	75 - 125	
			Acid Extractable Calcium (Ca)	2025/12/01		NC	%	75 - 125	
			Acid Extractable Chromium (Cr)	2025/12/01		NC	%	75 - 125	
			Acid Extractable Cobalt (Co)	2025/12/01		102	%	75 - 125	
			Acid Extractable Copper (Cu)	2025/12/01		NC	%	75 - 125	
			Acid Extractable Iron (Fe)	2025/12/01		NC	%	75 - 125	
			Acid Extractable Lead (Pb)	2025/12/01		98	%	75 - 125	
			Acid Extractable Magnesium (Mg)	2025/12/01		NC	%	75 - 125	
			Acid Extractable Manganese (Mn)	2025/12/01		NC	%	75 - 125	
			Acid Extractable Molybdenum (Mo)	2025/12/01		100	%	75 - 125	
			Acid Extractable Nickel (Ni)	2025/12/01		NC	%	75 - 125	
			Acid Extractable Phosphorus (P)	2025/12/01		NC	%	75 - 125	
			Acid Extractable Potassium (K)	2025/12/01		NC	%	75 - 125	
			Acid Extractable Selenium (Se)	2025/12/01		99	%	75 - 125	
			Acid Extractable Silver (Ag)	2025/12/01		103	%	75 - 125	
			Acid Extractable Sodium (Na)	2025/12/01		NC	%	75 - 125	
			Acid Extractable Strontium (Sr)	2025/12/01		NC	%	75 - 125	
			Acid Extractable Thallium (Tl)	2025/12/01		96	%	75 - 125	
			Acid Extractable Tin (Sn)	2025/12/01		104	%	75 - 125	
			Acid Extractable Uranium (U)	2025/12/01		105	%	75 - 125	
			Acid Extractable Vanadium (V)	2025/12/01		NC	%	75 - 125	
			Acid Extractable Zinc (Zn)	2025/12/01		NC	%	75 - 125	
			Acid Extractable Mercury (Hg)	2025/12/01		98	%	75 - 125	
A064873	DT1	Spiked Blank	Acid Extractable Aluminum (Al)	2025/12/01		107	%	80 - 120	
			Acid Extractable Antimony (Sb)	2025/12/01		105	%	80 - 120	
			Acid Extractable Arsenic (As)	2025/12/01		98	%	80 - 120	
			Acid Extractable Barium (Ba)	2025/12/01		95	%	80 - 120	
			Acid Extractable Beryllium (Be)	2025/12/01		94	%	80 - 120	
			Acid Extractable Bismuth (Bi)	2025/12/01		98	%	80 - 120	
			Acid Extractable Boron (B)	2025/12/01		91	%	80 - 120	
			Acid Extractable Cadmium (Cd)	2025/12/01		98	%	80 - 120	
			Acid Extractable Calcium (Ca)	2025/12/01		112	%	80 - 120	
			Acid Extractable Chromium (Cr)	2025/12/01		101	%	80 - 120	
			Acid Extractable Cobalt (Co)	2025/12/01		101	%	80 - 120	
			Acid Extractable Copper (Cu)	2025/12/01		98	%	80 - 120	
			Acid Extractable Iron (Fe)	2025/12/01		100	%	80 - 120	
			Acid Extractable Lead (Pb)	2025/12/01		97	%	80 - 120	
			Acid Extractable Magnesium (Mg)	2025/12/01		98	%	80 - 120	
			Acid Extractable Manganese (Mn)	2025/12/01		101	%	80 - 120	
			Acid Extractable Molybdenum (Mo)	2025/12/01		96	%	80 - 120	
			Acid Extractable Nickel (Ni)	2025/12/01		101	%	80 - 120	
			Acid Extractable Phosphorus (P)	2025/12/01		103	%	80 - 120	
			Acid Extractable Potassium (K)	2025/12/01		98	%	80 - 120	
			Acid Extractable Selenium (Se)	2025/12/01		101	%	80 - 120	
			Acid Extractable Silver (Ag)	2025/12/01		98	%	80 - 120	
			Acid Extractable Sodium (Na)	2025/12/01		98	%	80 - 120	



BUREAU
VERITAS

Bureau Veritas Job #: C5F0314
Report Date: 2025/12/16

Paterson Group
Client Project #: PG 7751
Site Location: 375 DIDSBURY RD
Sampler Initials: KS

QUALITY ASSURANCE REPORT(CONT'D)

QA/QC Batch	Init	QC Type	Parameter	Date Analyzed	Value	Recovery	UNITS	QC Limits
A064873	DT1	Method Blank	Acid Extractable Strontium (Sr)	2025/12/01		98	%	80 - 120
			Acid Extractable Thallium (Tl)	2025/12/01		95	%	80 - 120
			Acid Extractable Tin (Sn)	2025/12/01		99	%	80 - 120
			Acid Extractable Uranium (U)	2025/12/01		103	%	80 - 120
			Acid Extractable Vanadium (V)	2025/12/01		97	%	80 - 120
			Acid Extractable Zinc (Zn)	2025/12/01		102	%	80 - 120
			Acid Extractable Mercury (Hg)	2025/12/01		100	%	80 - 120
			Acid Extractable Aluminum (Al)	2025/12/01	<50		ug/g	
			Acid Extractable Antimony (Sb)	2025/12/01	<0.20		ug/g	
			Acid Extractable Arsenic (As)	2025/12/01	<1.0		ug/g	
			Acid Extractable Barium (Ba)	2025/12/01	<0.50		ug/g	
			Acid Extractable Beryllium (Be)	2025/12/01	<0.20		ug/g	
			Acid Extractable Bismuth (Bi)	2025/12/01	<1.0		ug/g	
			Acid Extractable Boron (B)	2025/12/01	<5.0		ug/g	
			Acid Extractable Cadmium (Cd)	2025/12/01	<0.10		ug/g	
			Acid Extractable Calcium (Ca)	2025/12/01	<50		ug/g	
			Acid Extractable Chromium (Cr)	2025/12/01	<1.0		ug/g	
			Acid Extractable Cobalt (Co)	2025/12/01	<0.10		ug/g	
			Acid Extractable Copper (Cu)	2025/12/01	<0.50		ug/g	
			Acid Extractable Iron (Fe)	2025/12/01	<50		ug/g	
			Acid Extractable Lead (Pb)	2025/12/01	<1.0		ug/g	
			Acid Extractable Magnesium (Mg)	2025/12/01	<50		ug/g	
			Acid Extractable Manganese (Mn)	2025/12/01	<1.0		ug/g	
			Acid Extractable Molybdenum (Mo)	2025/12/01	<0.50		ug/g	
			Acid Extractable Nickel (Ni)	2025/12/01	<0.50		ug/g	
			Acid Extractable Phosphorus (P)	2025/12/01	<50		ug/g	
			Acid Extractable Potassium (K)	2025/12/01	<200		ug/g	
			Acid Extractable Selenium (Se)	2025/12/01	<0.50		ug/g	
			Acid Extractable Silver (Ag)	2025/12/01	<0.20		ug/g	
			Acid Extractable Sodium (Na)	2025/12/01	<50		ug/g	
			Acid Extractable Strontium (Sr)	2025/12/01	<1.0		ug/g	
			Acid Extractable Thallium (Tl)	2025/12/01	<0.050		ug/g	
			Acid Extractable Tin (Sn)	2025/12/01	<1.0		ug/g	
			Acid Extractable Uranium (U)	2025/12/01	<0.050		ug/g	
			Acid Extractable Vanadium (V)	2025/12/01	<5.0		ug/g	
			Acid Extractable Zinc (Zn)	2025/12/01	<5.0		ug/g	
			Acid Extractable Mercury (Hg)	2025/12/01	<0.050		ug/g	
A064873	DT1	RPD [AXTU17-01]	Acid Extractable Aluminum (Al)	2025/12/01	2.5		%	30
			Acid Extractable Antimony (Sb)	2025/12/01	NC		%	30
			Acid Extractable Arsenic (As)	2025/12/01	12		%	30
			Acid Extractable Barium (Ba)	2025/12/01	4.6		%	30
			Acid Extractable Beryllium (Be)	2025/12/01	3.3		%	30
			Acid Extractable Bismuth (Bi)	2025/12/01	NC		%	30
			Acid Extractable Boron (B)	2025/12/01	0.039		%	30
			Acid Extractable Cadmium (Cd)	2025/12/01	NC		%	30
			Acid Extractable Calcium (Ca)	2025/12/01	1.5		%	30
			Acid Extractable Chromium (Cr)	2025/12/01	4.8		%	30
			Acid Extractable Cobalt (Co)	2025/12/01	4.0		%	30
			Acid Extractable Copper (Cu)	2025/12/01	4.2		%	30
			Acid Extractable Iron (Fe)	2025/12/01	5.1		%	30
			Acid Extractable Lead (Pb)	2025/12/01	5.0		%	30



BUREAU
VERITAS

Bureau Veritas Job #: C5F0314
Report Date: 2025/12/16

Paterson Group
Client Project #: PG 7751
Site Location: 375 DIDSBURY RD
Sampler Initials: KS

QUALITY ASSURANCE REPORT(CONT'D)

QA/QC Batch	Init	QC Type	Parameter	Date Analyzed	Value	Recovery	UNITS	QC Limits
			Acid Extractable Molybdenum (Mo)	2025/12/01	NC		%	30
			Acid Extractable Nickel (Ni)	2025/12/01	5.5		%	30
			Acid Extractable Phosphorus (P)	2025/12/01	5.7		%	30
			Acid Extractable Potassium (K)	2025/12/01	5.3		%	30
			Acid Extractable Selenium (Se)	2025/12/01	NC		%	30
			Acid Extractable Silver (Ag)	2025/12/01	NC		%	30
			Acid Extractable Sodium (Na)	2025/12/01	0.23		%	30
			Acid Extractable Strontium (Sr)	2025/12/01	6.6		%	30
			Acid Extractable Thallium (Tl)	2025/12/01	4.8		%	30
			Acid Extractable Tin (Sn)	2025/12/01	0.24		%	30
			Acid Extractable Uranium (U)	2025/12/01	5.6		%	30
			Acid Extractable Vanadium (V)	2025/12/01	4.3		%	30
			Acid Extractable Zinc (Zn)	2025/12/01	6.2		%	30
			Acid Extractable Mercury (Hg)	2025/12/01	NC		%	30
A064877	TLG	Matrix Spike [AXTU17-01]	Acid Extractable Sulphur (S)	2025/12/02		NC	%	75 - 125
A064877	TLG	Spiked Blank	Acid Extractable Sulphur (S)	2025/12/02		98	%	80 - 120
A064877	TLG	Method Blank	Acid Extractable Sulphur (S)	2025/12/02	<50		ug/g	
A064877	TLG	RPD [AXTU17-01]	Acid Extractable Sulphur (S)	2025/12/02	0.29		%	30
A065142	éQ7	RPD [AXTU15-01]	Loss on Ignition	2025/12/01	6.1		%	35
A065559	SAU	Spiked Blank	Available (CaCl2) pH	2025/12/02		101	%	97 - 103
A065559	SAU	RPD [AXTU19-01]	Available (CaCl2) pH	2025/12/02	0.37		%	N/A
A065600	NGI	Spiked Blank	Conductivity	2025/12/02		105	%	90 - 110
A065600	NGI	Method Blank	Conductivity	2025/12/02	<2		umho/cm	
A065600	NGI	RPD [AXTU17-01]	Conductivity	2025/12/02	1.1		%	10
A065953	MJ1	Matrix Spike [AXTU17-01]	Soluble (20:1) Chloride (Cl-)	2025/12/03		NC	%	70 - 130
A065953	MJ1	Spiked Blank	Soluble (20:1) Chloride (Cl-)	2025/12/03		99	%	70 - 130
A065953	MJ1	Method Blank	Soluble (20:1) Chloride (Cl-)	2025/12/03	<20		ug/g	
A065953	MJ1	RPD [AXTU17-01]	Soluble (20:1) Chloride (Cl-)	2025/12/03	13		%	35
A065978	MJ1	Matrix Spike [AXTU17-01]	Soluble (20:1) Sulphate (SO4)	2025/12/03		NC	%	70 - 130
A065978	MJ1	Spiked Blank	Soluble (20:1) Sulphate (SO4)	2025/12/03		98	%	75 - 125
A065978	MJ1	Method Blank	Soluble (20:1) Sulphate (SO4)	2025/12/03	<20		ug/g	
A065978	MJ1	RPD [AXTU17-01]	Soluble (20:1) Sulphate (SO4)	2025/12/03	21		%	35
A066391	NGI	Spiked Blank	Redox Potential	2025/12/06		98	%	80 - 120
A066391	NGI	RPD [AXTU19-01]	Redox Potential	2025/12/06	13		%	35
A067788	éLS	Matrix Spike	Sulphide	2025/12/04		54 (1)	%	75 - 125
			Sulphide	2025/12/04		54 (1)	%	75 - 125
A067788	éLS	Spiked Blank	Sulphide	2025/12/04		79	%	75 - 125
			Sulphide	2025/12/04		79	%	75 - 125
A067788	éLS	Method Blank	Sulphide	2025/12/04	<0.50		mg/kg	
			Sulphide	2025/12/04	<0.50		mg/kg	
A067789	SIB	Method Blank	Moisture-Subcontracted	2025/12/03	<0.30		%	
			Moisture-Subcontracted	2025/12/03	<0.30		%	
A067789	SIB	RPD [AXTU20-01]	Moisture-Subcontracted	2025/12/03	1.8		%	20
A073031	éKS	Matrix Spike	Soluble Chloride (Cl-)	2025/12/11		105	%	75 - 125
A073031	éKS	QC Standard	Soluble Chloride (Cl-)	2025/12/11		79	%	75 - 125
A073031	éKS	Spiked Blank	Soluble Chloride (Cl-)	2025/12/11		105	%	80 - 120
A073031	éKS	Method Blank	Soluble Chloride (Cl-)	2025/12/11	<10		mg/L	
A073032	ZI	QC Standard	Soluble Conductivity	2025/12/12		93	%	75 - 125
A073032	ZI	Spiked Blank	Soluble Conductivity	2025/12/11		98	%	90 - 110
A073032	ZI	Method Blank	Soluble Conductivity	2025/12/11	<0.020		dS/m	
A073033	éPP	QC Standard	Soluble (CaCl2) pH	2025/12/11		101	%	97 - 103
A073033	éPP	Spiked Blank	Soluble (CaCl2) pH	2025/12/11		100	%	97 - 103
A073035	VSC	Matrix Spike	Soluble Calcium (Ca)	2025/12/11		92	%	75 - 125



BUREAU
VERITAS

Bureau Veritas Job #: C5F0314
Report Date: 2025/12/16

Paterson Group
Client Project #: PG 7751
Site Location: 375 DIDSBURY RD
Sampler Initials: KS

QUALITY ASSURANCE REPORT(CONT'D)

QA/QC Batch	Init	QC Type	Parameter	Date Analyzed	Value	Recovery	UNITS	QC Limits
A073035	VSC	QC Standard	Soluble Magnesium (Mg)	2025/12/11		98	%	75 - 125
			Soluble Sodium (Na)	2025/12/11		98	%	75 - 125
			Soluble Potassium (K)	2025/12/11		100	%	75 - 125
			Soluble Calcium (Ca)	2025/12/11		90	%	75 - 125
			Soluble Magnesium (Mg)	2025/12/11		89	%	75 - 125
			Soluble Sodium (Na)	2025/12/11		96	%	75 - 125
A073035	VSC	Spiked Blank	Soluble Potassium (K)	2025/12/11		109	%	75 - 125
			Soluble Sulphate (SO4)	2025/12/11		91	%	75 - 125
			Soluble Calcium (Ca)	2025/12/11		96	%	80 - 120
			Soluble Magnesium (Mg)	2025/12/11		98	%	80 - 120
			Soluble Sodium (Na)	2025/12/11		98	%	80 - 120
			Soluble Potassium (K)	2025/12/11		99	%	80 - 120
A073035	VSC	Method Blank	Soluble Calcium (Ca)	2025/12/11	<3.0		mg/L	
			Soluble Magnesium (Mg)	2025/12/11	<2.0		mg/L	
			Soluble Sodium (Na)	2025/12/11	<3.0		mg/L	
			Soluble Potassium (K)	2025/12/11	<2.0		mg/L	
			Soluble Sulphate (SO4)	2025/12/11	<6.0		mg/L	
A073036	NSW	QC Standard	Saturation %	2025/12/11		100	%	75 - 125
A073039	éLK	Matrix Spike	Soluble Chloride (Cl-)	2025/12/05		NC	%	75 - 125
A073039	éLK	QC Standard	Soluble Chloride (Cl-)	2025/12/05		94	%	75 - 125
A073039	éLK	Spiked Blank	Soluble Chloride (Cl-)	2025/12/05		102	%	80 - 120
A073039	éLK	Method Blank	Soluble Chloride (Cl-)	2025/12/05	<10		mg/L	
A073040	ZI	QC Standard	Soluble Conductivity	2025/12/06		99	%	75 - 125
A073040	ZI	Spiked Blank	Soluble Conductivity	2025/12/06		98	%	90 - 110
A073040	ZI	Method Blank	Soluble Conductivity	2025/12/06	<0.020		dS/m	
A073041	éPP	QC Standard	Soluble (CaCl2) pH	2025/12/05		101	%	97 - 103
A073041	éPP	Spiked Blank	Soluble (CaCl2) pH	2025/12/05		100	%	97 - 103
A073042	VSC	Matrix Spike	Soluble Calcium (Ca)	2025/12/06		96	%	75 - 125
			Soluble Magnesium (Mg)	2025/12/06		101	%	75 - 125
			Soluble Sodium (Na)	2025/12/06		NC	%	75 - 125
			Soluble Potassium (K)	2025/12/06		103	%	75 - 125
			Soluble Calcium (Ca)	2025/12/06		100	%	75 - 125
			Soluble Magnesium (Mg)	2025/12/06		99	%	75 - 125
A073042	VSC	QC Standard	Soluble Sodium (Na)	2025/12/06		105	%	75 - 125
			Soluble Potassium (K)	2025/12/06		112	%	75 - 125
			Soluble Sulphate (SO4)	2025/12/06		98	%	75 - 125
			Soluble Calcium (Ca)	2025/12/06		99	%	80 - 120
			Soluble Magnesium (Mg)	2025/12/06		101	%	80 - 120
			Soluble Sodium (Na)	2025/12/06		97	%	80 - 120
A073042	VSC	Spiked Blank	Soluble Potassium (K)	2025/12/06		103	%	80 - 120
			Soluble Calcium (Ca)	2025/12/06	<3.0		mg/L	
			Soluble Magnesium (Mg)	2025/12/06	<2.0		mg/L	
			Soluble Sodium (Na)	2025/12/06	<3.0		mg/L	
			Soluble Potassium (K)	2025/12/06	<2.0		mg/L	
			Soluble Sulphate (SO4)	2025/12/06	<6.0		mg/L	
A073043	STB	QC Standard	Saturation %	2025/12/05		98	%	75 - 125
A073044	ZI	QC Standard	Soluble Conductivity	2025/12/06		102	%	75 - 125
A073044	ZI	Spiked Blank	Soluble Conductivity	2025/12/06		98	%	90 - 110
A073044	ZI	Method Blank	Soluble Conductivity	2025/12/06	<0.020		dS/m	
A073045	éKS	Matrix Spike	Soluble Chloride (Cl-)	2025/12/07		103	%	75 - 125
A073045	éKS	QC Standard	Soluble Chloride (Cl-)	2025/12/07		90	%	75 - 125
A073045	éKS	Spiked Blank	Soluble Chloride (Cl-)	2025/12/07		101	%	80 - 120
A073045	éKS	Method Blank	Soluble Chloride (Cl-)	2025/12/07	<10		mg/L	



QUALITY ASSURANCE REPORT(CONT'D)

QA/QC Batch	Init	QC Type	Parameter	Date Analyzed	Value	Recovery	UNITS	QC Limits
A073046	ZI	QC Standard	Soluble Conductivity	2025/12/06		96	%	75 - 125
A073046	ZI	Spiked Blank	Soluble Conductivity	2025/12/06		98	%	90 - 110
A073046	ZI	Method Blank	Soluble Conductivity	2025/12/06	<0.020		dS/m	
A073047	éPP	QC Standard	Soluble (CaCl ₂) pH	2025/12/05		101	%	97 - 103
A073047	éPP	Spiked Blank	Soluble (CaCl ₂) pH	2025/12/05		100	%	97 - 103
A073048	éOY	Matrix Spike	Soluble Calcium (Ca)	2025/12/07		96	%	75 - 125
			Soluble Magnesium (Mg)	2025/12/07		95	%	75 - 125
			Soluble Sodium (Na)	2025/12/07		92	%	75 - 125
			Soluble Potassium (K)	2025/12/07		96	%	75 - 125
A073048	éOY	QC Standard	Soluble Calcium (Ca)	2025/12/07		93	%	75 - 125
			Soluble Magnesium (Mg)	2025/12/07		90	%	75 - 125
			Soluble Sodium (Na)	2025/12/07		96	%	75 - 125
			Soluble Potassium (K)	2025/12/07		102	%	75 - 125
			Soluble Sulphate (SO ₄)	2025/12/07		88	%	75 - 125
A073048	éOY	Spiked Blank	Soluble Calcium (Ca)	2025/12/07		96	%	80 - 120
			Soluble Magnesium (Mg)	2025/12/07		95	%	80 - 120
			Soluble Sodium (Na)	2025/12/07		95	%	80 - 120
			Soluble Potassium (K)	2025/12/07		96	%	80 - 120
A073048	éOY	Method Blank	Soluble Calcium (Ca)	2025/12/07	<3.0		mg/L	
			Soluble Magnesium (Mg)	2025/12/07	<2.0		mg/L	
			Soluble Sodium (Na)	2025/12/07	<3.0		mg/L	
			Soluble Potassium (K)	2025/12/07	<2.0		mg/L	
			Soluble Sulphate (SO ₄)	2025/12/07	<6.0		mg/L	
A073049	STB	QC Standard	Saturation %	2025/12/05		102	%	75 - 125

N/A = Not Applicable

Duplicate: Paired analysis of a separate portion of the same sample. Used to evaluate the variance in the measurement.

Matrix Spike: A sample to which a known amount of the analyte of interest has been added. Used to evaluate sample matrix interference.

QC Standard: A sample of known concentration prepared by an external agency under stringent conditions. Used as an independent check of method accuracy.

Spiked Blank: A blank matrix sample to which a known amount of the analyte, usually from a second source, has been added. Used to evaluate method accuracy.

Method Blank: A blank matrix containing all reagents used in the analytical procedure. Used to identify laboratory contamination.

NC (Matrix Spike): The recovery in the matrix spike was not calculated. The relative difference between the concentration in the parent sample and the spike amount was too small to permit a reliable recovery calculation (matrix spike concentration was less than the native sample concentration)

NC (Duplicate RPD): The duplicate RPD was not calculated. The concentration in the sample and/or duplicate was too low to permit a reliable RPD calculation (absolute difference <= 2x RDL).

(1) Recovery or RPD for this parameter is outside control limits. The overall quality control for this analysis meets acceptability criteria.



BUREAU
VERITAS

Bureau Veritas Job #: C5F0314

Report Date: 2025/12/16

Paterson Group

Client Project #: PG 7751

Site Location: 375 DIDSBURY RD

Sampler Initials: KS

VALIDATION SIGNATURE PAGE

The analytical data and all QC contained in this report were reviewed and validated by:

Cristina Carriere, Senior Scientific Specialist

David Huang, BBY Scientific Specialist

Veronica Falk, B.Sc., P.Chem., QP, Scientific Specialist, Organics

Louise Harding, Scientific Specialist

Suwan (Sze Yeung) Fock, B.Sc., Scientific Specialist

Bureau Veritas has procedures in place to guard against improper use of the electronic signature and have the required "signatories", as per ISO/IEC 17025, signing the reports. For Service Group specific validation, please refer to the Validation Signatures page if included, otherwise available by request. For Department specific Analyst/Supervisor validation names, please refer to the Test Summary section if included, otherwise available by request. This report is authorized by Rodney Major, General Manager responsible for Ontario Environmental laboratory operations.



SERVICE CENTER COOLER TEMPERATURE RECORD

COOLER OBSERVATIONS:

BV Receipt #		CUSTODY SEAL		YES	NO	□ Drinking Water		
1	OTT-2025-11-281	PRESENT	✓			5	5	5
		INTACT	✓					
		ICE PRESENT	✓					
2	285	CUSTODY SEAL	✓			4	3	2
		PRESENT	✓					
		INTACT	✓					
		ICE PRESENT	✓					
3	279	CUSTODY SEAL	✓			3	2	2
		PRESENT	✓					
		INTACT	✓					
		ICE PRESENT	✓					
4	292	CUSTODY SEAL	✓			2	1	2
		PRESENT	✓					
		INTACT	✓					
		ICE PRESENT	✓					
5	287	CUSTODY SEAL	✓			2	0	0
		PRESENT	✓					
		INTACT	✓					
		ICE PRESENT	✓					
6	288	CUSTODY SEAL	✓			-1	-1	-2
		PRESENT	✓					
		INTACT	✓					
		ICE PRESENT	✓					
7	289	CUSTODY SEAL	✓			2	1	2
		PRESENT	✓					
		INTACT	✓					
		ICE PRESENT	✓					
8	293	CUSTODY SEAL	✓			-3	1	1
		PRESENT	✓					
		INTACT	✓					
		ICE PRESENT	✓					
9	280	CUSTODY SEAL	✓			2	2	1
		PRESENT	✓					
		INTACT	✓					
		ICE PRESENT	✓					
10	281	CUSTODY SEAL	✓			3	2	2
		PRESENT	✓					
		INTACT	✓					
		ICE PRESENT	✓					

CHAIN-OF-CUSTODY RECORD

SHIPPED FROM BV SERVICE CENTER:		RECEIVED AT:	
OTTAWA		MISSISSAUGA	
BV Receipt #		CUSTODY SEAL	
11	282	YES	NO
		PRESENT	✓
		INTACT	✓
		ICE PRESENT	✓
12	277	YES	NO
		PRESENT	✓
		INTACT	✓
		ICE PRESENT	✓
13	278	YES	NO
		PRESENT	✓
		INTACT	✓
		ICE PRESENT	✓
14	287	YES	NO
		PRESENT	✓
		INTACT	✓
		ICE PRESENT	✓
15	288	YES	NO
		PRESENT	✓
		INTACT	✓
		ICE PRESENT	✓
16		YES	NO
		PRESENT	
		INTACT	
		ICE PRESENT	
17		YES	NO
		PRESENT	
		INTACT	
		ICE PRESENT	
18		YES	NO
		PRESENT	
		INTACT	
		ICE PRESENT	
19		YES	NO
		PRESENT	
		INTACT	
		ICE PRESENT	
20		YES	NO
		PRESENT	
		INTACT	
		ICE PRESENT	

RECEIVED BY (PRINT & SIGN)		DATE (YYYY/MM/DD)	TIME (HH:MM)
ANMOLPREET SINGH		2025/11/27	06:23

If Custody seal condition and presence of ice is the same for all, use these boxes:	CUSTODY SEAL	YES	NO
	PRESENT	✓	
	INTACT	✓	
	ICE PRESENT	✓	

Received in Ottawa



6740 Campobello Road, Mississauga, Ontario L5N 2L8
Phone: 905-817-5700 Fax: 905-817-5779 Toll Free: 800-563-6266

CHAIN OF CUSTODY RECORD

ENV COC - 00014v6

Page 1 of 1

Invoice Information		Invoice to (requires report)		Report Information (if differs from invoice)		Project Information											
Company: First Capital Management LP		Company: Paterson Group		Quotation #:													
Contact Name: Mona Poon		Contact Name: Otilia McLaughlin		P.O. #/ AFE#:													
Street Address: 85 Hanna St Suite 400		Street Address: 9 Auriga Drive		Project #:		PG 7751											
City: Toronto		City: Ottawa		Site #:													
Prov: ON		Prov: ON		Site Location:		375 Didsbury Rd											
Postal Code: M6K 3S3		Postal Code: K2E 1T9		Site Location Province:		ON											
Phone: 416-504-4114		Phone: 613-226-7381		Sampled By:		KS											
Email: mona.poon@fcr.ca		Email: omclaughlin@patersongroup.ca															
Copies:		Copies:															
Regulatory Criteria																	
☐ Table 1 ☐ Res/Park ☐ Med/Fine ☐ CCME ☐ Reg 406, Table: ☐ Sanitary Sewer Bylaw																	
☐ Table 2 ☐ Ind/Comm ☐ Coarse ☐ *min 3 day TAT ☐ Storm Sewer Bylaw																	
☐ Table 3 ☐ Agri/other ☐ For RSC ☐ MISA ☐ Municipality																	
☐ Table ☐ PWQO ☐ Other:																	
Include Criteria on Certificate of Analysis (check if yes): ☐																	
SAMPLES MUST BE KEPT COOL (<10°C) FROM TIME OF SAMPLING UNTIL DELIVERY TO BUREAU VERITAS																	
Sample Identification (Please print or Type)																	
Date Sampled																	
Time (24hr)																	
Matrix																	
1 TPI-25-G1-150 mm 2025 11 21 10 00 Soil																	
2 TPI-25-G2-300 mm 2025 11 21 10 00 Soil																	
3 TPI-25-G3-450 mm 2025 11 21 10 00 Soil																	
4 TP3-25-G1-150 mm 2025 11 21 12 00 Soil																	
5 TP3-25-G2-300 mm 2025 11 21 12 00 Soil																	
6 TP3-25-G3-450 mm 2025 11 21 12 00 Soil																	
7 TP7-25-G1-150 mm 2025 11 21 16 30 Soil																	
8 TP7-25-G2-300 mm 2025 11 21 16 30 Soil																	
9 TP7-25-G3-450 mm 2025 11 21 16 30 Soil																	
10																	
11																	
12																	
13																	
14																	
15																	
16																	
17																	
18																	
19																	
20																	
21																	
22																	
Regular Turnaround Time (TAT)																	
☒ 5 to 7 Day ☐ 10 Day																	
Rush Turnaround Time (TAT) Surcharges apply																	
☐ Same Day ☐ 1 Day																	
☐ 2 Day ☐ 3 Day																	
☐ 4 Day																	
Date Required: YYYY MM D																	
Comments																	
OTT-2025-11-280																	
*UNLESS OTHERWISE AGREED TO IN WRITING, WORK SUBMITTED ON THIS CHAIN OF CUSTODY IS SUBJECT TO BUREAU VERITAS STANDARD TERMS AND CONDITIONS. SIGNING OF THIS CHAIN OF CUSTODY DOCUMENT IS ACKNOWLEDGMENT AND ACCEPTANCE OF OUR TERMS AND CONDITIONS WHICH ARE AVAILABLE FOR VIEWING AT WWW.BVNA.COM/TERMS-AND-CONDITIONS OR BY CALLING THE LABORATORY LISTED ABOVE TO OBTAIN A COPY																	
LAB USE ONLY		Yes		No		°C		LAB USE ONLY		Yes		No		°C		Temperature reading by	
Seal present								Seal present									
Seal intact								Seal intact									
Cooling media present								Cooling media present									
Relinquished by: (Signature/ Print)		Date		Time		Received by: (Signature/ Print)		Date		Time		Special Instructions					
1		YYYY MM DD		HH MM		1 Pedro da Silva		2025 11 26 13 00									
2						2											



Your Project #: PG7751
Site Location: 375 DIDSBURY RD
Your C.O.C. #: C#1074347-01-01

Attention: Otilia McLaughlin

Paterson Group
9 Auriga Drive
Ottawa, ON
Canada K2E 7T9

Report Date: 2025/12/17
Report #: R8670603
Version: 1 - Final

CERTIFICATE OF ANALYSIS

BUREAU VERITAS JOB #: C5F5762

Received: 2025/12/09, 09:20

Sample Matrix: Water
Samples Received: 4

Analyses	Date		Date Analyzed	Laboratory Method	Analytical Method
	Quantity	Extracted			
Alkalinity (1)	2	N/A	2025/12/13	CAM SOP-00448	SM 24 2320 B m
Chloride by Automated Colourimetry (1)	2	N/A	2025/12/15	CAM SOP-00463	SM 24 4500-Cl E m
Fluoride (1)	2	2025/12/12	2025/12/13	CAM SOP-00449	SM 24 4500-F C m
Hardness (calculated as CaCO ₃) (1)	2	N/A	2025/12/17	CAM SOP 00102/00408/00447	SM 2340 B
Dissolved Metals by ICPMS (1)	1	N/A	2025/12/16	CAM SOP-00447	EPA 6020B m
Nitrate & Nitrite as Nitrogen in Water (1, 2)	2	N/A	2025/12/12	CAM SOP-00440	SM 24 4500-NO3I/NO2B
pH (1, 3)	2	2025/12/12	2025/12/13	CAM SOP-00413	SM 24th - 4500H+ B
Sulphate by Automated Turbidimetry (1)	2	N/A	2025/12/15	CAM SOP-00464	SM 24 4500-SO42- E m
Total Dissolved Solids (1)	1	2025/12/12	2025/12/15	CAM SOP-00428	SM 24 2540C m

Remarks:

Bureau Veritas is accredited to ISO/IEC 17025 for specific parameters on scopes of accreditation. Unless otherwise noted, procedures used by Bureau Veritas are based upon recognized Provincial, Federal or US method compendia such as CCME, EPA, APHA or the Quebec Ministry of Environment.

All work recorded herein has been done in accordance with procedures and practices ordinarily exercised by professionals in Bureau Veritas' profession using accepted testing methodologies, quality assurance and quality control procedures (except where otherwise agreed by the client and Bureau Veritas in writing). All data is in statistical control and has met quality control and method performance criteria unless otherwise noted. All method blanks are reported; unless indicated otherwise, associated sample data are not blank corrected. Where applicable, unless otherwise noted, Measurement Uncertainty has not been accounted for when stating conformity to the referenced standard.

Bureau Veritas liability is limited to the actual cost of the requested analyses, unless otherwise agreed in writing. There is no other warranty expressed or implied. Bureau Veritas has been retained to provide analysis of samples provided by the Client using the testing methodology referenced in this report. Interpretation and use of test results are the sole responsibility of the Client and are not within the scope of services provided by Bureau Veritas, unless otherwise agreed in writing. Bureau Veritas is not responsible for the accuracy or any data impacts, that result from the information provided by the customer or their agent.

Solid sample results, except biota, are based on dry weight unless otherwise indicated. Organic analyses are not recovery corrected except for isotope dilution methods.

Results relate to samples tested. When sampling is not conducted by Bureau Veritas, results relate to the supplied samples tested.

This Certificate shall not be reproduced except in full, without the written approval of the laboratory.

Reference Method suffix "m" indicates test methods incorporate validated modifications from specific reference methods to improve performance.

* RPDs calculated using raw data. The rounding of final results may result in the apparent difference.

(1) This test was performed by Bureau Veritas Mississauga, 6740 Campobello Rd, Mississauga, ON, L5N 2L8

(2) Values for calculated parameters may not appear to add up due to rounding of raw data and significant figures.



Your Project #: PG7751
Site Location: 375 DIDSBURY RD
Your C.O.C. #: C#1074347-01-01

Attention: Otilia McLaughlin

Paterson Group
9 Auriga Drive
Ottawa, ON
Canada K2E 7T9

Report Date: 2025/12/17
Report #: R8670603
Version: 1 - Final

CERTIFICATE OF ANALYSIS

BUREAU VERITAS JOB #: C5F5762

Received: 2025/12/09, 09:20

(3) "The CCME method and Analytical Protocol (O. Reg. 153/04, O. Reg. 406/19) requires pH to be analyzed within 15 minutes of sampling and therefore field analysis is required for compliance. All Laboratory pH analyses in this report are reported past the CCME and Analytical Protocol (O. Reg. 153/04, O. Reg. 406/19) holding time. Bureau Veritas endeavors to analyze samples as soon as possible after receipt."

Encryption Key

Please direct all questions regarding this Certificate of Analysis to:

Katherine Szozda, Project Manager
Email: Katherine.Szozda@bureauveritas.com
Phone# (613)274-0573 Ext:7063633

=====

This report has been generated and distributed using a secure automated process.

Bureau Veritas has procedures in place to guard against improper use of the electronic signature and have the required "signatories", as per ISO/IEC 17025, signing the reports. For Service Group specific validation, please refer to the Validation Signatures page if included, otherwise available by request. For Department specific Analyst/Supervisor validation names, please refer to the Test Summary section if included, otherwise available by request. This report is authorized by Rodney Major, General Manager responsible for Ontario Environmental laboratory operations.



**BUREAU
VERITAS**

Bureau Veritas Job #: C5F5762

Report Date: 2025/12/17

Paterson Group

Client Project #: PG7751

Site Location: 375 DIDSBURY RD

Sampler Initials: DR

RESULTS OF ANALYSES OF WATER

Bureau Veritas ID		AYEX95	AYEX96			AYEX98		
Sampling Date		2025/12/05 12:00	2025/12/05 12:00			2025/12/05 12:00		
COC Number		C#1074347-01-01	C#1074347-01-01			C#1074347-01-01		
	UNITS	16884 BH15-25-GW1-1	16884 BH15-25-GW1-2	RDL	QC Batch	16771 BH15-25-GW1-4	RDL	QC Batch
Calculated Parameters								
Hardness (CaCO ₃)	mg/L	230	230	1.0	A071881			
Inorganics								
Total Dissolved Solids	mg/L					835	10	A072761
Fluoride (F ⁻)	mg/L	0.20	0.20	0.10	A073135			
pH	pH	7.93	7.92		A073140			
Dissolved Sulphate (SO ₄)	mg/L	61	61	1.0	A073391			
Alkalinity (Total as CaCO ₃)	mg/L	350	350	1.0	A073139			
Dissolved Chloride (Cl ⁻)	mg/L	240	240	5.0	A073388			
Nitrate (N)	mg/L	<0.10	<0.10	0.10	A073119			
RDL = Reportable Detection Limit								
QC Batch = Quality Control Batch								



BUREAU
VERITAS

Bureau Veritas Job #: CSF5762

Report Date: 2025/12/17

Paterson Group

Client Project #: PG7751

Site Location: 375 DIDSBURY RD

Sampler Initials: DR

ELEMENTS BY ATOMIC SPECTROSCOPY (WATER)

Bureau Veritas ID		AYIK10	AYIK10		
Sampling Date		2025/12/05 12:00	2025/12/05 12:00		
COC Number		C#1074347-01-01	C#1074347-01-01		
	UNITS	BH15-25-GW1-5	BH15-25-GW1-5 Lab-Dup	RDL	QC Batch
Metals					
Dissolved Aluminum (Al)	ug/L	<4.9	<4.9	4.9	A074380
Dissolved Antimony (Sb)	ug/L	0.65	0.61	0.50	A074380
Dissolved Arsenic (As)	ug/L	1.9	1.8	1.0	A074380
Dissolved Barium (Ba)	ug/L	140	140	2.0	A074380
Dissolved Beryllium (Be)	ug/L	<0.40	<0.40	0.40	A074380
Dissolved Bismuth (Bi)	ug/L	<1.0	<1.0	1.0	A074380
Dissolved Boron (B)	ug/L	340	340	10	A074380
Dissolved Cadmium (Cd)	ug/L	<0.090	<0.090	0.090	A074380
Dissolved Calcium (Ca)	ug/L	49000	48000	200	A074380
Dissolved Chromium (Cr)	ug/L	<5.0	<5.0	5.0	A074380
Dissolved Cobalt (Co)	ug/L	<0.50	<0.50	0.50	A074380
Dissolved Copper (Cu)	ug/L	4.7	4.7	0.90	A074380
Dissolved Iron (Fe)	ug/L	<100	<100	100	A074380
Dissolved Lead (Pb)	ug/L	<0.50	<0.50	0.50	A074380
Dissolved Lithium (Li)	ug/L	<5.0	<5.0	5.0	A074380
Dissolved Magnesium (Mg)	ug/L	29000	28000	50	A074380
Dissolved Manganese (Mn)	ug/L	97	96	2.0	A074380
Dissolved Molybdenum (Mo)	ug/L	11	10	0.50	A074380
Dissolved Nickel (Ni)	ug/L	1.1	1.1	1.0	A074380
Dissolved Phosphorus (P)	ug/L	<100	<100	100	A074380
Dissolved Potassium (K)	ug/L	19000	19000	200	A074380
Dissolved Selenium (Se)	ug/L	<2.0	<2.0	2.0	A074380
Dissolved Silicon (Si)	ug/L	6900	6900	50	A074380
Dissolved Silver (Ag)	ug/L	<0.090	<0.090	0.090	A074380
Dissolved Sodium (Na)	ug/L	220000	220000	100	A074380
Dissolved Strontium (Sr)	ug/L	310	300	1.0	A074380
Dissolved Tellurium (Te)	ug/L	<1.0	<1.0	1.0	A074380
Dissolved Thallium (Tl)	ug/L	0.063	<0.050	0.050	A074380
Dissolved Tin (Sn)	ug/L	<1.0	<1.0	1.0	A074380
Dissolved Titanium (Ti)	ug/L	<5.0	<5.0	5.0	A074380
RDL = Reportable Detection Limit					
QC Batch = Quality Control Batch					
Lab-Dup = Laboratory Initiated Duplicate					



BUREAU
VERITAS

Bureau Veritas Job #: C5F5762

Report Date: 2025/12/17

Paterson Group

Client Project #: PG7751

Site Location: 375 DIDSBURY RD

Sampler Initials: DR

ELEMENTS BY ATOMIC SPECTROSCOPY (WATER)

Bureau Veritas ID		AYIK10	AYIK10		
Sampling Date		2025/12/05 12:00	2025/12/05 12:00		
COC Number		C#1074347-01-01	C#1074347-01-01		
	UNITS	BH15-25-GW1-5	BH15-25-GW1-5 Lab-Dup	RDL	QC Batch
Dissolved Tungsten (W)	ug/L	<1.0	<1.0	1.0	A074380
Dissolved Uranium (U)	ug/L	6.3	6.2	0.10	A074380
Dissolved Vanadium (V)	ug/L	1.5	1.4	0.50	A074380
Dissolved Zinc (Zn)	ug/L	<5.0	<5.0	5.0	A074380
Dissolved Zirconium (Zr)	ug/L	<1.0	<1.0	1.0	A074380
RDL = Reportable Detection Limit QC Batch = Quality Control Batch Lab-Dup = Laboratory Initiated Duplicate					



BUREAU
VERITAS

Bureau Veritas Job #: C5F5762

Report Date: 2025/12/17

Paterson Group

Client Project #: PG7751

Site Location: 375 DIDSBURY RD

Sampler Initials: DR

TEST SUMMARY

Bureau Veritas ID: AYEX95
Sample ID: 16884 BH15-25-GW1-1
Matrix: Water

Collected: 2025/12/05
Shipped:
Received: 2025/12/09

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Alkalinity	AT	A073139	N/A	2025/12/13	Nachiketa Gohil
Chloride by Automated Colourimetry	SKAL	A073388	N/A	2025/12/15	Massarat Jan
Fluoride	ISE	A073135	2025/12/12	2025/12/13	Nachiketa Gohil
Hardness (calculated as CaCO ₃)		A071881	N/A	2025/12/17	Automated Statchk
Nitrate & Nitrite as Nitrogen in Water	LACH	A073119	N/A	2025/12/12	Chandra Nandlal
pH	AT	A073140	2025/12/12	2025/12/13	Nachiketa Gohil
Sulphate by Automated Turbidimetry	SKAL	A073391	N/A	2025/12/15	Massarat Jan

Bureau Veritas ID: AYEX96
Sample ID: 16884 BH15-25-GW1-2
Matrix: Water

Collected: 2025/12/05
Shipped:
Received: 2025/12/09

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Alkalinity	AT	A073139	N/A	2025/12/13	Nachiketa Gohil
Chloride by Automated Colourimetry	SKAL	A073388	N/A	2025/12/15	Massarat Jan
Fluoride	ISE	A073135	2025/12/12	2025/12/13	Nachiketa Gohil
Hardness (calculated as CaCO ₃)		A071881	N/A	2025/12/17	Automated Statchk
Nitrate & Nitrite as Nitrogen in Water	LACH	A073119	N/A	2025/12/12	Chandra Nandlal
pH	AT	A073140	2025/12/12	2025/12/13	Nachiketa Gohil
Sulphate by Automated Turbidimetry	SKAL	A073391	N/A	2025/12/15	Massarat Jan

Bureau Veritas ID: AYEX98
Sample ID: 16771 BH15-25-GW1-4
Matrix: Water

Collected: 2025/12/05
Shipped:
Received: 2025/12/09

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Total Dissolved Solids	BAL	A072761	2025/12/12	2025/12/15	Tina Teng

Bureau Veritas ID: AYIK10
Sample ID: BH15-25-GW1-5
Matrix: Water

Collected: 2025/12/05
Shipped:
Received: 2025/12/09

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Dissolved Metals by ICPMS	ICP/MS	A074380	N/A	2025/12/16	Prempal Bhatti

Bureau Veritas ID: AYIK10 Dup
Sample ID: BH15-25-GW1-5
Matrix: Water

Collected: 2025/12/05
Shipped:
Received: 2025/12/09

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Dissolved Metals by ICPMS	ICP/MS	A074380	N/A	2025/12/16	Prempal Bhatti



GENERAL COMMENTS

Each temperature is the average of up to three cooler temperatures taken at receipt

Package 1	12.7°C
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Results relate only to the items tested.



BUREAU
VERITAS

Bureau Veritas Job #: C5F5762
Report Date: 2025/12/17

Paterson Group
Client Project #: PG7751
Site Location: 375 DIDSBURY RD
Sampler Initials: DR

QUALITY ASSURANCE REPORT

QA/QC Batch	Init	QC Type	Parameter	Date Analyzed	Value	Recovery	UNITS	QC Limits
A072761	TTE	Spiked Blank	Total Dissolved Solids	2025/12/15		95	%	80 - 120
A072761	TTE	Method Blank	Total Dissolved Solids	2025/12/15	<10		mg/L	
A072761	TTE	RPD	Total Dissolved Solids	2025/12/15	0.25		%	20
A073119	C_N	Matrix Spike	Nitrate (N)	2025/12/12		102	%	80 - 120
A073119	C_N	Spiked Blank	Nitrate (N)	2025/12/12		101	%	80 - 120
A073119	C_N	Method Blank	Nitrate (N)	2025/12/12	<0.10		mg/L	
A073119	C_N	RPD	Nitrate (N)	2025/12/12	1.1		%	20
A073135	NGI	Matrix Spike	Fluoride (F-)	2025/12/13		106	%	75 - 125
A073135	NGI	Spiked Blank	Fluoride (F-)	2025/12/13		101	%	75 - 125
A073135	NGI	Method Blank	Fluoride (F-)	2025/12/13	<0.10		mg/L	
A073135	NGI	RPD	Fluoride (F-)	2025/12/13	8.5		%	20
A073139	NGI	Spiked Blank	Alkalinity (Total as CaCO3)	2025/12/13		97	%	85 - 115
A073139	NGI	Method Blank	Alkalinity (Total as CaCO3)	2025/12/13	<1.0		mg/L	
A073139	NGI	RPD	Alkalinity (Total as CaCO3)	2025/12/13	0.79		%	20
			Alkalinity (Total as CaCO3)	2025/12/13	0.51		%	20
A073140	NGI	Spiked Blank	pH	2025/12/13		102	%	98 - 103
A073140	NGI	RPD	pH	2025/12/13	0.49		%	N/A
A073388	MJ1	Matrix Spike	Dissolved Chloride (Cl-)	2025/12/15		NC	%	80 - 120
A073388	MJ1	Spiked Blank	Dissolved Chloride (Cl-)	2025/12/15		96	%	80 - 120
A073388	MJ1	Method Blank	Dissolved Chloride (Cl-)	2025/12/15	<1.0		mg/L	
A073388	MJ1	RPD	Dissolved Chloride (Cl-)	2025/12/15	0.014		%	20
A073391	MJ1	Matrix Spike	Dissolved Sulphate (SO4)	2025/12/15		88	%	75 - 125
A073391	MJ1	Spiked Blank	Dissolved Sulphate (SO4)	2025/12/15		101	%	80 - 120
A073391	MJ1	Method Blank	Dissolved Sulphate (SO4)	2025/12/15	<1.0		mg/L	
A073391	MJ1	RPD	Dissolved Sulphate (SO4)	2025/12/15	1.2		%	20
A074380	PBA	Matrix Spike [AYIK10-01]	Dissolved Aluminum (Al)	2025/12/16		117	%	80 - 120
			Dissolved Antimony (Sb)	2025/12/16		119	%	80 - 120
			Dissolved Arsenic (As)	2025/12/16		111	%	80 - 120
			Dissolved Barium (Ba)	2025/12/16		106	%	80 - 120
			Dissolved Beryllium (Be)	2025/12/16		107	%	80 - 120
			Dissolved Bismuth (Bi)	2025/12/16		102	%	80 - 120
			Dissolved Boron (B)	2025/12/16		101	%	80 - 120
			Dissolved Cadmium (Cd)	2025/12/16		112	%	80 - 120
			Dissolved Calcium (Ca)	2025/12/16		NC	%	80 - 120
			Dissolved Chromium (Cr)	2025/12/16		109	%	80 - 120
			Dissolved Cobalt (Co)	2025/12/16		110	%	80 - 120
			Dissolved Copper (Cu)	2025/12/16		111	%	80 - 120
			Dissolved Iron (Fe)	2025/12/16		108	%	80 - 120
			Dissolved Lead (Pb)	2025/12/16		109	%	80 - 120
			Dissolved Lithium (Li)	2025/12/16		111	%	80 - 120
			Dissolved Magnesium (Mg)	2025/12/16		NC	%	80 - 120
			Dissolved Manganese (Mn)	2025/12/16		111	%	80 - 120
			Dissolved Molybdenum (Mo)	2025/12/16		114	%	80 - 120
			Dissolved Nickel (Ni)	2025/12/16		109	%	80 - 120
			Dissolved Phosphorus (P)	2025/12/16		113	%	80 - 120
			Dissolved Potassium (K)	2025/12/16		108	%	80 - 120
			Dissolved Selenium (Se)	2025/12/16		111	%	80 - 120
			Dissolved Silicon (Si)	2025/12/16		107	%	80 - 120
			Dissolved Silver (Ag)	2025/12/16		76 (1)	%	80 - 120
			Dissolved Sodium (Na)	2025/12/16		NC	%	80 - 120
			Dissolved Strontium (Sr)	2025/12/16		108	%	80 - 120
			Dissolved Tellurium (Te)	2025/12/16		109	%	80 - 120
			Dissolved Thallium (Tl)	2025/12/16		108	%	80 - 120



BUREAU
VERITAS

Bureau Veritas Job #: C5F5762

Report Date: 2025/12/17

Paterson Group

Client Project #: PG7751

Site Location: 375 DIDSBURY RD

Sampler Initials: DR

QUALITY ASSURANCE REPORT(CONT'D)

QA/QC Batch	Init	QC Type	Parameter	Date Analyzed	Value	Recovery	UNITS	QC Limits
A074380	PBA	Spiked Blank	Dissolved Tin (Sn)	2025/12/16		115	%	80 - 120
			Dissolved Titanium (Ti)	2025/12/16		108	%	80 - 120
			Dissolved Tungsten (W)	2025/12/16		112	%	80 - 120
			Dissolved Uranium (U)	2025/12/16		110	%	80 - 120
			Dissolved Vanadium (V)	2025/12/16		113	%	80 - 120
			Dissolved Zinc (Zn)	2025/12/16		111	%	80 - 120
			Dissolved Zirconium (Zr)	2025/12/16		121 (1)	%	80 - 120
			Dissolved Aluminum (Al)	2025/12/16		101	%	80 - 120
			Dissolved Antimony (Sb)	2025/12/16		103	%	80 - 120
			Dissolved Arsenic (As)	2025/12/16		101	%	80 - 120
			Dissolved Barium (Ba)	2025/12/16		96	%	80 - 120
			Dissolved Beryllium (Be)	2025/12/16		97	%	80 - 120
			Dissolved Bismuth (Bi)	2025/12/16		94	%	80 - 120
			Dissolved Boron (B)	2025/12/16		93	%	80 - 120
			Dissolved Cadmium (Cd)	2025/12/16		99	%	80 - 120
			Dissolved Calcium (Ca)	2025/12/16		98	%	80 - 120
			Dissolved Chromium (Cr)	2025/12/16		98	%	80 - 120
			Dissolved Cobalt (Co)	2025/12/16		101	%	80 - 120
			Dissolved Copper (Cu)	2025/12/16		99	%	80 - 120
			Dissolved Iron (Fe)	2025/12/16		98	%	80 - 120
			Dissolved Lead (Pb)	2025/12/16		101	%	80 - 120
			Dissolved Lithium (Li)	2025/12/16		100	%	80 - 120
			Dissolved Magnesium (Mg)	2025/12/16		98	%	80 - 120
			Dissolved Manganese (Mn)	2025/12/16		102	%	80 - 120
			Dissolved Molybdenum (Mo)	2025/12/16		99	%	80 - 120
			Dissolved Nickel (Ni)	2025/12/16		101	%	80 - 120
			Dissolved Phosphorus (P)	2025/12/16		99	%	80 - 120
			Dissolved Potassium (K)	2025/12/16		98	%	80 - 120
			Dissolved Selenium (Se)	2025/12/16		101	%	80 - 120
			Dissolved Silicon (Si)	2025/12/16		97	%	80 - 120
			Dissolved Silver (Ag)	2025/12/16		98	%	80 - 120
			Dissolved Sodium (Na)	2025/12/16		99	%	80 - 120
			Dissolved Strontium (Sr)	2025/12/16		103	%	80 - 120
			Dissolved Tellurium (Te)	2025/12/16		99	%	80 - 120
			Dissolved Thallium (Tl)	2025/12/16		100	%	80 - 120
			Dissolved Tin (Sn)	2025/12/16		100	%	80 - 120
			Dissolved Titanium (Ti)	2025/12/16		96	%	80 - 120
			Dissolved Tungsten (W)	2025/12/16		101	%	80 - 120
			Dissolved Uranium (U)	2025/12/16		100	%	80 - 120
			Dissolved Vanadium (V)	2025/12/16		101	%	80 - 120
			Dissolved Zinc (Zn)	2025/12/16		103	%	80 - 120
			Dissolved Zirconium (Zr)	2025/12/16		104	%	80 - 120
A074380	PBA	Method Blank	Dissolved Aluminum (Al)	2025/12/16	<4.9		ug/L	
			Dissolved Antimony (Sb)	2025/12/16	<0.50		ug/L	
			Dissolved Arsenic (As)	2025/12/16	<1.0		ug/L	
			Dissolved Barium (Ba)	2025/12/16	<2.0		ug/L	
			Dissolved Beryllium (Be)	2025/12/16	<0.40		ug/L	
			Dissolved Bismuth (Bi)	2025/12/16	<1.0		ug/L	
			Dissolved Boron (B)	2025/12/16	<10		ug/L	
			Dissolved Cadmium (Cd)	2025/12/16	<0.090		ug/L	
			Dissolved Calcium (Ca)	2025/12/16	<200		ug/L	
			Dissolved Chromium (Cr)	2025/12/16	<5.0		ug/L	
			Dissolved Cobalt (Co)	2025/12/16	<0.50		ug/L	



BUREAU
VERITAS

Bureau Veritas Job #: C5F5762
Report Date: 2025/12/17

Paterson Group
Client Project #: PG7751
Site Location: 375 DIDSBURY RD
Sampler Initials: DR

QUALITY ASSURANCE REPORT(CONT'D)

QA/QC Batch	Init	QC Type	Parameter	Date Analyzed	Value	Recovery	UNITS	QC Limits
A074380	PBA	RPD [AYIK10-01]	Dissolved Copper (Cu)	2025/12/16	<0.90		ug/L	
			Dissolved Iron (Fe)	2025/12/16	<100		ug/L	
			Dissolved Lead (Pb)	2025/12/16	<0.50		ug/L	
			Dissolved Lithium (Li)	2025/12/16	<5.0		ug/L	
			Dissolved Magnesium (Mg)	2025/12/16	<50		ug/L	
			Dissolved Manganese (Mn)	2025/12/16	<2.0		ug/L	
			Dissolved Molybdenum (Mo)	2025/12/16	<0.50		ug/L	
			Dissolved Nickel (Ni)	2025/12/16	<1.0		ug/L	
			Dissolved Phosphorus (P)	2025/12/16	<100		ug/L	
			Dissolved Potassium (K)	2025/12/16	<200		ug/L	
			Dissolved Selenium (Se)	2025/12/16	<2.0		ug/L	
			Dissolved Silicon (Si)	2025/12/16	<50		ug/L	
			Dissolved Silver (Ag)	2025/12/16	<0.090		ug/L	
			Dissolved Sodium (Na)	2025/12/16	<100		ug/L	
			Dissolved Strontium (Sr)	2025/12/16	<1.0		ug/L	
			Dissolved Tellurium (Te)	2025/12/16	<1.0		ug/L	
			Dissolved Thallium (Tl)	2025/12/16	<0.050		ug/L	
			Dissolved Tin (Sn)	2025/12/16	<1.0		ug/L	
			Dissolved Titanium (Ti)	2025/12/16	<5.0		ug/L	
			Dissolved Tungsten (W)	2025/12/16	<1.0		ug/L	
			Dissolved Uranium (U)	2025/12/16	<0.10		ug/L	
			Dissolved Vanadium (V)	2025/12/16	<0.50		ug/L	
			Dissolved Zinc (Zn)	2025/12/16	<5.0		ug/L	
			Dissolved Zirconium (Zr)	2025/12/16	<1.0		ug/L	
			Dissolved Aluminum (Al)	2025/12/16	NC		%	20
			Dissolved Antimony (Sb)	2025/12/16	7.6		%	20
			Dissolved Arsenic (As)	2025/12/16	2.7		%	20
			Dissolved Barium (Ba)	2025/12/16	1.9		%	20
			Dissolved Beryllium (Be)	2025/12/16	NC		%	20
			Dissolved Bismuth (Bi)	2025/12/16	NC		%	20
			Dissolved Boron (B)	2025/12/16	1.4		%	20
			Dissolved Cadmium (Cd)	2025/12/16	NC		%	20
			Dissolved Calcium (Ca)	2025/12/16	0.79		%	20
			Dissolved Chromium (Cr)	2025/12/16	NC		%	20
			Dissolved Cobalt (Co)	2025/12/16	NC		%	20
			Dissolved Copper (Cu)	2025/12/16	0.49		%	20
			Dissolved Iron (Fe)	2025/12/16	NC		%	20
			Dissolved Lead (Pb)	2025/12/16	NC		%	20
			Dissolved Lithium (Li)	2025/12/16	NC		%	20
			Dissolved Magnesium (Mg)	2025/12/16	1.1		%	20
			Dissolved Manganese (Mn)	2025/12/16	1.1		%	20
			Dissolved Molybdenum (Mo)	2025/12/16	4.9		%	20
			Dissolved Nickel (Ni)	2025/12/16	3.7		%	20
			Dissolved Phosphorus (P)	2025/12/16	NC		%	20
			Dissolved Potassium (K)	2025/12/16	2.2		%	20
			Dissolved Selenium (Se)	2025/12/16	NC		%	20
			Dissolved Silicon (Si)	2025/12/16	0.14		%	20
			Dissolved Silver (Ag)	2025/12/16	NC		%	20
			Dissolved Sodium (Na)	2025/12/16	0.11		%	20
			Dissolved Strontium (Sr)	2025/12/16	2.9		%	20
			Dissolved Tellurium (Te)	2025/12/16	NC		%	20
			Dissolved Thallium (Tl)	2025/12/16	NC		%	20
			Dissolved Tin (Sn)	2025/12/16	NC		%	20



QUALITY ASSURANCE REPORT(CONT'D)

QA/QC Batch	Init	QC Type	Parameter	Date Analyzed	Value	Recovery	UNITS	QC Limits
			Dissolved Titanium (Ti)	2025/12/16	NC		%	20
			Dissolved Tungsten (W)	2025/12/16	NC		%	20
			Dissolved Uranium (U)	2025/12/16	2.7		%	20
			Dissolved Vanadium (V)	2025/12/16	4.2		%	20
			Dissolved Zinc (Zn)	2025/12/16	NC		%	20
			Dissolved Zirconium (Zr)	2025/12/16	NC		%	20
N/A = Not Applicable								
Duplicate: Paired analysis of a separate portion of the same sample. Used to evaluate the variance in the measurement.								
Matrix Spike: A sample to which a known amount of the analyte of interest has been added. Used to evaluate sample matrix interference.								
Spiked Blank: A blank matrix sample to which a known amount of the analyte, usually from a second source, has been added. Used to evaluate method accuracy.								
Method Blank: A blank matrix containing all reagents used in the analytical procedure. Used to identify laboratory contamination.								
NC (Matrix Spike): The recovery in the matrix spike was not calculated. The relative difference between the concentration in the parent sample and the spike amount was too small to permit a reliable recovery calculation (matrix spike concentration was less than the native sample concentration)								
NC (Duplicate RPD): The duplicate RPD was not calculated. The concentration in the sample and/or duplicate was too low to permit a reliable RPD calculation (absolute difference $\leq 2 \times \text{RDL}$).								
(1) Matrix Spike exceeds acceptance limits, probable matrix interference								



BUREAU
VERITAS

Bureau Veritas Job #: C5F5762

Report Date: 2025/12/17

Paterson Group

Client Project #: PG7751

Site Location: 375 DIDSBURY RD

Sampler Initials: DR

VALIDATION SIGNATURE PAGE

The analytical data and all QC contained in this report were reviewed and validated by:

Cristina Carriere, Senior Scientific Specialist

Bureau Veritas has procedures in place to guard against improper use of the electronic signature and have the required "signatories", as per ISO/IEC 17025, signing the reports. For Service Group specific validation, please refer to the Validation Signatures page if included, otherwise available by request. For Department specific Analyst/Supervisor validation names, please refer to the Test Summary section if included, otherwise available by request. This report is authorized by Rodney Major, General Manager responsible for Ontario Environmental laboratory operations.



SERVICE CENTER COOLER TEMPERATURE RECORD

CHAIN-OF-CUSTODY RECORD

BV Receipt #		COOLER OBSERVATIONS:		
1	OTT-268-12-037	CUSTODY SEAL	YES	NO
		PRESENT	☒	
		INTACT	☒	
		ICE PRESENT	☒	
2	036	CUSTODY SEAL	YES	NO
		PRESENT	☒	
		INTACT	☒	
		ICE PRESENT	☒	
3	039	CUSTODY SEAL	YES	NO
		PRESENT	☒	
		INTACT	☒	
		ICE PRESENT	☒	
4	039	CUSTODY SEAL	YES	NO
		PRESENT	☒	
		INTACT	☒	
		ICE PRESENT	☒	
5	035	CUSTODY SEAL	YES	NO
		PRESENT	☒	
		INTACT	☒	
		ICE PRESENT	☒	
6	040	CUSTODY SEAL	YES	NO
		PRESENT	☒	
		INTACT	☒	
		ICE PRESENT	☒	
7	042	CUSTODY SEAL	YES	NO
		PRESENT	☒	
		INTACT	☒	
		ICE PRESENT	☒	
8	043	CUSTODY SEAL	YES	NO
		PRESENT	☒	
		INTACT	☒	
		ICE PRESENT	☒	
9		CUSTODY SEAL	YES	NO
		PRESENT	☒	
		INTACT	☒	
		ICE PRESENT	☒	
10		CUSTODY SEAL	YES	NO
		PRESENT	☒	
		INTACT	☒	
		ICE PRESENT	☒	

BV Receipt #		SHIPPED FROM BV SERVICE CENTER:		
11		OTTAWA		
		CUSTODY SEAL	YES	NO
		PRESENT	☒	
		INTACT	☒	
		ICE PRESENT	☒	
12		CUSTODY SEAL	YES	NO
		PRESENT	☒	
		INTACT	☒	
		ICE PRESENT	☒	
13		CUSTODY SEAL	YES	NO
		PRESENT	☒	
		INTACT	☒	
		ICE PRESENT	☒	
14		CUSTODY SEAL	YES	NO
		PRESENT	☒	
		INTACT	☒	
		ICE PRESENT	☒	
15		CUSTODY SEAL	YES	NO
		PRESENT	☒	
		INTACT	☒	
		ICE PRESENT	☒	
16		CUSTODY SEAL	YES	NO
		PRESENT	☒	
		INTACT	☒	
		ICE PRESENT	☒	
17		CUSTODY SEAL	YES	NO
		PRESENT	☒	
		INTACT	☒	
		ICE PRESENT	☒	
18		CUSTODY SEAL	YES	NO
		PRESENT	☒	
		INTACT	☒	
		ICE PRESENT	☒	
19		CUSTODY SEAL	YES	NO
		PRESENT	☒	
		INTACT	☒	
		ICE PRESENT	☒	
20		CUSTODY SEAL	YES	NO
		PRESENT	☒	
		INTACT	☒	
		ICE PRESENT	☒	

RECEIVED BY (PRINT & SIGN)	DATE (YYYY/MM/DD)	TIME (HH:MM)
ANMOLORETT SINGH	2025/12/16	06:25

If Custody seal condition and presence of ice is the same for all, use these boxes:	CUSTODY SEAL	YES	NO
	PRESENT	☒	
	INTACT	☒	
	ICE PRESENT	☒	

C5F5762

2025/12/09 09:20

Bureau Veritas
36 Antares Dr Unit 100, Nepean, Ontario Canada K2E 7W5 Tel: (613) 274-0573 Toll-free: 800-563-6266 Fax: (613) 274-0574 www.bvna.com

Received in Ottawa

CHAIN OF CUSTODY RECORD

Page of

Invoice To:		Report To:		PROJECT INFORMATION:		Laboratory Use Only:	
Company:	#39638 First Capital Asset Management LP	Company:	#38345 Paterson Group	Quotation #:	C44365	Bureau Veritas Job #:	Bottle Order #:
Attention:	Accounts Payable	Attention:	Otillia McLaughlin	P.O. #:			
Address:	85 Hanna Ave Toronto ON M6K 3S3	Address:	9 Auriga Drive Ottawa ON K2E 7T9	Project:	PG 7751 375 Didsbury		
Tel:	(416) 643-4341	Tel:	(613) 226-7381	Project Name:		COC #:	Project Manager:
Email:		Email:	omclaughlin@patersongroup.ca	Site #:	DR		Katherine Szozda
MOE REGULATED DRINKING WATER OR WATER INTENDED FOR HUMAN CONSUMPTION MUST BE SUBMITTED ON THE BUREAU VERITAS DRINKING WATER CHAIN OF CUSTODY				ANALYSIS REQUESTED (PLEASE BE SPECIFIC)			
Regulation 153 (2011) ☐ Table 1 ☐ Res/Park ☐ Medium/Fine ☐ Table 2 ☐ Ind/Comm ☐ Coarse ☐ Table 3 ☐ Agri/Other ☐ For RSC ☐ Table _____		Other Regulations ☐ CCME ☐ Sanitary Sewer Bylaw ☐ Reg 558 ☐ Storm Sewer Bylaw ☐ MISA ☐ Municipality _____ ☐ PWQO ☐ Reg 406 Table _____ ☐ Other _____		Special Instructions 		Turnaround Time (TAT) Required: Please provide advance notice for all projects. Regul. (Standard) TAT: (will be applied if Rush TAT is not specified): Standard TAT = 5-7 Working days for most tests. Please note: Standard TAT for certain tests such as BOD and Drinking Furans are > 5 days - contact your Project Manager for details. Job Specific Rush TAT (if applies to entire submission): Date Required: _____ Time Required: _____ Rush Confirmation Number: _____ (call for #)	
Include Criteria on Certificate of Analysis (Y/N)? Regulation 153 (2011) ☐ Y ☐ N				Field Filtered (please circle): Metals / Hg / Cr / V			
Sample Barcode Label	Sample (Location) Identification	Date Sampled	Time Sampled	Matrix	Total Dissolved Solids	Alkalinity	Chloride, Sulphate, Fluoride, Nitrate
16884 (General)	BH15-25-GW1-1	Dec 5 2025	12:00	W		X	X
16884 (General)	BH15-25-GW1-2	Dec 5 2025	12:00	W		X	X
16566 (Nutrients)	BH15-25-GW1-3	Dec 5 2025	12:00	W			X
16771 (Solids)	BH15-25-GW1-4	Dec 5 2025	12:00	W	X		
5							
6							
7							
8							
9							
10							
Relinquished By (Print):	Date: (YY/MM/DD)	Time	RECEIVED BY: (Signature/Print)	Date: (YY/MM/DD)	Time	# jars used and not submitted	Laboratory Use Only (See Pack)
Otillia McLaughlin	25/12/19	9:00	Loen Asad	2025/12/09	9:20		Time Sensitive Temperature (°C) on Receipt: 13/13/12 Custody Seal Present: ☒ Intact: ☒
* UNLESS OTHERWISE AGREED TO IN WRITING, WORK SUBMITTED ON THIS CHAIN OF CUSTODY IS SUBJECT TO BUREAU VERITAS'S STANDARD TERMS AND CONDITIONS. SIGNING OF THIS CHAIN OF CUSTODY DOCUMENT IS ACKNOWLEDGMENT AND ACCEPTANCE OF OUR TERMS WHICH ARE AVAILABLE FOR VIEWING AT WWW.BVNA.COM/ENVIRONMENTAL-LABORATORIES/RESOURCES/COC-TERMS-AND-CONDITIONS. * IT IS THE RESPONSIBILITY OF THE RELINQUISHER TO ENSURE THE ACCURACY OF THE CHAIN OF CUSTODY RECORD. AN INCOMPLETE CHAIN OF CUSTODY MAY RESULT IN ANALYTICAL TAT DELAYS. ** SAMPLE CONTAINER, PRESERVATION, HOLD TIME AND PACKAGE INFORMATION CAN BE VIEWED AT WWW.BVNA.COM/ENVIRONMENTAL-LABORATORIES/RESOURCES/CHAIN-CUSTODY-FORMS-COCS.							White: Bureau Veritas Yellow: Client SAMPLES MUST BE KEPT COOL (< 10° C) FROM TIME OF SAMPLING UNTIL DELIVERY TO BUREAU VERITAS

OTT-2025-12-035



★ Please Add to BV Ton C5E5762 ★

APPENDIX 2

FIGURE 1 - KEY PLAN

DRAWINGS PG7751-1 - TEST HOLE LOCATION PLAN

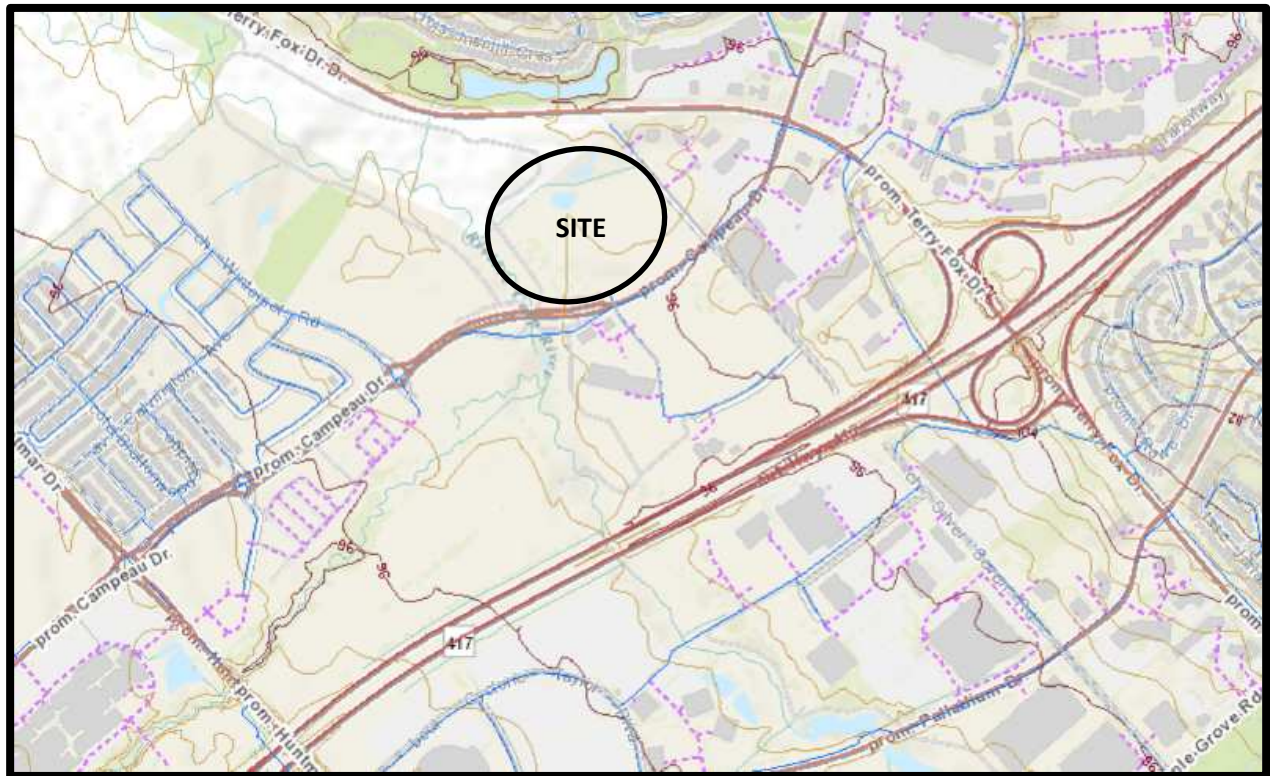
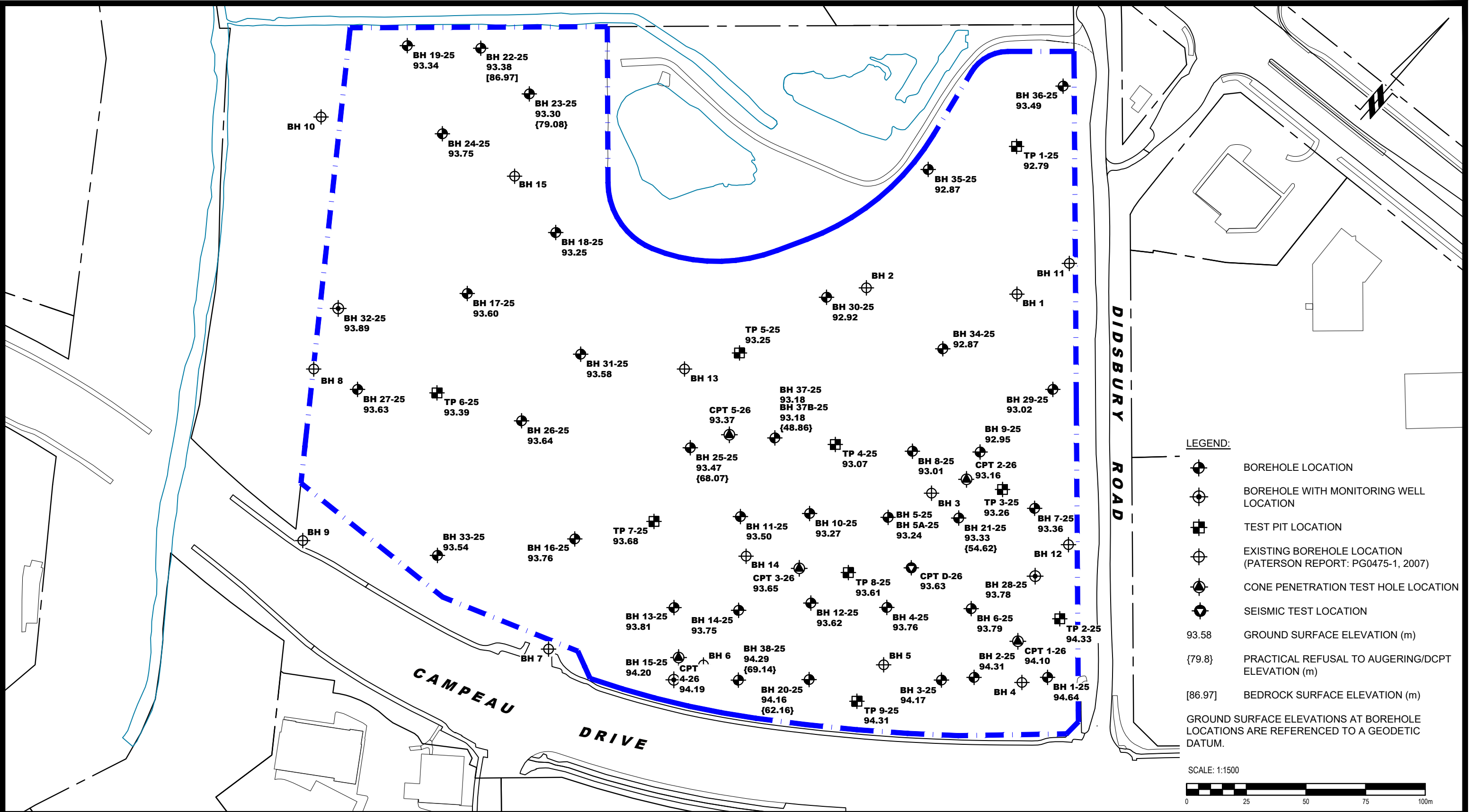


FIGURE 1

KEY PLAN





9 AURIGA DRIVE
OTTAWA, ON
K2E 7T9
TEL: (613) 226-7381

1	ADDED 2026 CONE PENETRATION TEST HOLE CPT 1-26 TO CPT 5-26 AND SEISMIC TEST CPTD-26 TO PLAN	18/03/2026	OM
NO.	REVISIONS	DD/MM/YYYY	INITIAL

FIRST CAPITAL REALTY INC.
GEOTECHNICAL INVESTIGATION
PROPOSED COMMERCIAL DEVELOPMENT
375 DIDSBURY ROAD

ONTARIO

OTTAWA,
Title:

TEST HOLE LOCATION PLAN

Scale:	1:1500	Date:	12/2025
Drawn by:	ZS	Report No.:	PG7751-1
Checked by:	NV	Dwg. No.:	PG7751-1
Approved by:	DP	Revision No.:	1